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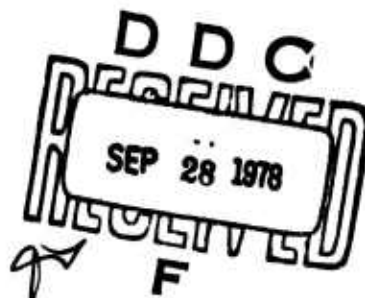


**PRELIMINARY DESIGN STUDY OF A TAIL ROTOR BLADE  
JETTISON CONCEPT**

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Prepared for

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## APPLIED TECHNOLOGY LABORATORY POSITION STATEMENT

This report provides the results of a preliminary concept study which indicates that a tail rotor blade jettison system can be developed for four-bladed tail rotor systems, which will allow the controlled jettison of a damaged blade and its opposing blade and allow continued flight with the remaining two blades. A prototype system was developed that evaluated system performance characteristics throughout the maximum/minimum tail rotor speeds anticipated and determined the resultant effects on structural integrity, tail rotor stability, and handling qualities using both analytical and simulation modeling techniques. The analyses and evaluation tests conducted showed that the prototype blade jettison system developed meets the performance requirements of the UH-60A helicopter.

Results of this contractual effort are still preliminary, and additional effort is required to improve and validate the survivable characteristics of the design.

Mr. Harold W. Holland of the Aeronautical Systems Division served as technical monitor for this effort.

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20 ABSTRACT (Continue on reverse side if necessary and identify by block number) Loss of a significant portion of a tail rotor blade will cause severe imbalance of the tail rotor that can lead to secondary damage to the helicopter and possible injury to the occupants. A system that detects such blade loss and removes the imbalance by jettison of the residual portion of the damaged blade and its opposing blade can overcome the rotor imbalance and allow continued flight. Using the performance characteristics of the UH-60A BLACK HAWK helicopter, a prototype system			

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was developed and its performance evaluated to determine the capability of the system to jettison rotor blades in a manner that would prevent secondary damage. Additionally, analyses were conducted to determine the dynamic stability characteristics of the UH-60A tail rotor in a two-bladed configuration and the ability of the helicopter to accommodate the loads developed during transition from four to two blades. Residual helicopter performance and the capability of the helicopter to be retrimmed following jettison of two opposing tail rotor blades was analyzed using the ~~GENERAL HELICOPTER FLIGHT DYNAMIC MODEL~~ programmed on a PDP-10 Hybrid Computer. Handling qualities to be expected following the loss of opposing tail rotor blades were examined by integrating the computer model and two-blade sub-routine with a flight simulator. The analyses and evaluation tests conducted show that the prototype blade jettison system developed meets the performance requirements of the UH-60A helicopter.

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## INTRODUCTION

Loss of a significant portion of a tail rotor blade will result in severe tail rotor imbalance that can lead to secondary damage to the helicopter and/or injury to the occupants. Continued use of the helicopter in hostile environments is anticipated, and with this the possibility of exposure of the helicopter to increased ballistic threat levels beyond the normally survivable 7.62mm projectile. The 14.5mm, 23mm, 30mm, and 37mm high explosive incendiary rounds are capable of inflicting such severe damage that if a tail rotor blade sustains a hit, blade loss can be expected to occur. The development of tail rotor blades that can tolerate the magnitude of damage that these rounds can cause must therefore be substantially larger and will, in all likelihood, have an undesirable increase in centrifugal force resulting in significant weight penalties in the rotor hub, drive shaft, and supporting structure as well as increasing power requirements. This escalation of component size is particularly unsuitable for the small, reconnaissance-type helicopters.

As an alternative to the development of ballistically tolerant blades to prevent rotor imbalance of four-bladed tail rotor systems, the imbalance forces caused by the loss of a part or all of a blade can be overcome by the controlled jettison of the residual portion of the damaged blade and its opposing blade, to allow continued flight with the remaining two blades. The intent of this effort was to develop a working prototype system to evaluate system performance characteristics throughout the maximum/minimum tail rotor speeds anticipated and to determine the resultant effects on structural integrity, tail rotor stability, and handling qualities using both analytical and simulation modeling techniques.

The prototype system relates closely to a concept defined in a study program previously conducted by Sikorsky Aircraft under U. S. Army Contract DAAD05-73-C-0523, where the feasibility of applying the opposing blade jettison concept to the main rotor system of a four-bladed helicopter was determined. The results of the program are included in a report (Reference 1) distributed by USA Ballistic Research Laboratories, Aberdeen Proving Ground, Maryland. In accordance with the requirements of that program, a conceptual design was established for damage detection and controlled rotor blade jettison that is the basis for the prototype design of this present contract. Although the basic concept is essentially the same, many circuitry improvements and refinements have been incorporated.

The prototype development and associated analyses were based on the physical and performance characteristics of the UH-60A BLACK HAWK helicopter (Figure 1), a candidate for initial application of the system. Additionally, complete performance information and simulation programs were readily available for this effort in accordance with the contract. The system design lends itself to kit-type installation, and the electrical portion of the system can be modified for other four-bladed helicopters with only minor changes. Pyro-

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<sup>1</sup> J. W. Johnson, R. A. Selleck, Rotor Balance Restoration Study, Sikorsky Aircraft, U. S. Army Ballistic Research Laboratories Contract Report #197, December, 1974.

technic blade severing devices, damage detectors, and supporting hardware must be sized for the particular helicopter application.

During the system design portion of this program, emphasis was placed on maximizing system reliability. To this end, the system employs state-of-the-art components, fully encapsulated assemblies, solid-state design, no moving parts in contact, and the latest design techniques and safeguards to prevent inadvertent system initiation. The capability of the prototype system developed under this contract to effect blade jettison within the jettison window established for the UH-60A helicopter was evaluated by installing the system in an Engineering rotary test stand, capable of incremental rotational speed adjustment from well below to well above the UH-60A design rotor speeds.

Concurrent with prototype system development, the dynamic stability characteristics and handling qualities that can be anticipated for the UH-60A helicopter with two opposing tail rotor blades jettisoned were determined. The dynamic analysis included an investigation of the two-bladed stability, vibration, and rotor hub load levels for speeds to 150 knots. Additionally, the ability of the UH-60A helicopter to structurally accommodate the centrifugal loads from loss of a full tail rotor blade until rebalance by opposing blade jettison was examined. The handling qualities were examined through the use of the UH-60A version of General Helicopter Simulation Program and blade transition subroutines to determine trim characteristics. The pilot work load was determined by integration of the Simulation Program with a flight simulator to obtain qualitative pilot-in-the-loop assessment of flight attitude recoverability following transition from the normal four-bladed mode to the emergency two-bladed mode.



Figure 1. UH-60A BLACK HAWK Helicopter Baseline



## PART I CONCEPT ANALYSIS

Loss of a significant portion of tail rotor blade is sensed by the interruption of detector circuits located along the leading and trailing edges of the blade spar. Interruption of both of the detector circuits results in initiation of pyrotechnic linear-shaped charges (LSC) located adjacent to the rotor hub that sever both the residual portion of the damaged blade and its opposing blade. The specific point of rotor rotation at which the separation occurs is controlled to prevent secondary damage to the main rotor blades or the vehicle proper.

Successful operation of the system on the UH-60A helicopter requires the analysis of the effects of the system on the aircraft and its occupants both during and after blade jettison has occurred. It is necessary to define an available window for blade jettison that will avoid secondary damage and to determine the residual performance capability of the helicopter following the jettison of the two rotor blades. Included in the analyses is a determination of the resultant vibration levels and loads to be expected and a discussion of the ability of the UH-60A to structurally accommodate the reaction loads during the period of rotor imbalance. This work is presented in the following subtasks.

### BLADE SEPARATION WINDOW

Following loss of a portion of all of the damaged rotor blade, rebalance of the rotor can be effected by either simultaneous jettison of the residual portion of the damaged blade and its opposing blade or by sequential jettison of the blades. The latter, sequential, approach is selected for the UH-60A for the following reasons: The available window for simultaneous blade jettison is established by the need for adequate clearance with the main rotor blades for a forward jettisoned blade and the horizontal stabilator for an aftward jettisoned blade. The available window must accommodate the variances in the point of blade jettison due to the variations of component function times and the range of rotor speeds considered for the design of the system. Of greater importance, however, is the potential hazard of a vertically jettisoned tail rotor blade to the helicopter in the event of system operation in a hover, or near hover, flight mode. Selection of a sequential blade jettison capability overcomes both of these difficulties. Figure 2 shows the window established for use in the design of the UH-60A blade jettison system.

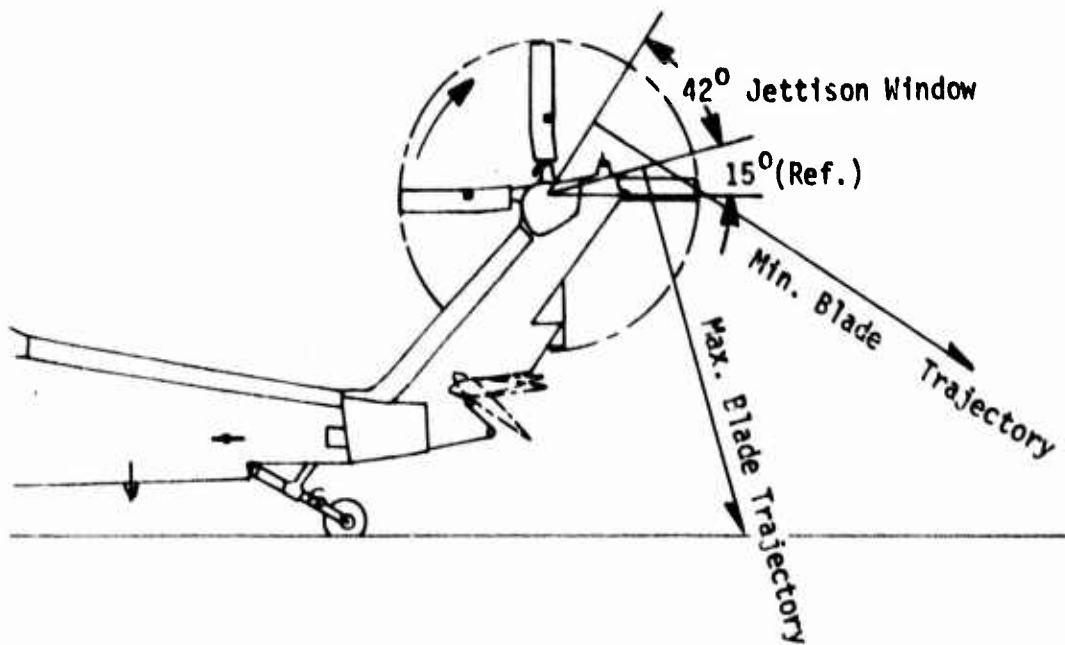


Figure 2. Acceptable Window for Sequential Rotor Blade Jettison

Although the sequential jettison of blades would normally allow a much greater window than that shown in Figure 2, the upper limit has been constrained to minimize any potential hazard that jettisoned blades might present to other aircraft that may be flying formation with the damaged aircraft. Further, the lower window limit is less than that available to reduce the possibility of secondary damage to the remaining rotor blades by a rebounding blade if the system is operated while the aircraft is on, or near the ground. The 42-degree window has been verified by analysis to be adequate for rotor rotations from 70%  $N_R$  (830 RPM) to 150%  $N_R$  (1877 RPM). Additionally, the 42-degree window will accommodate a worst case stack-up of component function times at the 150%  $N_R$  rotor speed.

#### TWO BLADE STABILITY, VIBRATION, AND LOAD LEVEL

Analytical investigations were performed to evaluate the dynamic stability characteristics of the two-bladed UH-60A cross beam tail rotor, and the vibration and load levels in the aircraft in the forward flight regime up to 150 knots. The analytical results indicate that the two-bladed rotor system mounted on the flexible pylon is stable up to the maximum speed investigated of 150 knots.

A normal modes rotor aeroelastic analysis was employed to calculate the steady and 2 and 4/rev vibratory loads at the hub originating from the two-bladed rotor system. These loads were then used in conjunction with the tail rotor pylon modes to evaluate the vibration levels experienced at the hub and gearbox. It was found that the vibration and load levels

increase with forward speed. At 150 knots the highest speed investigated, the maximum 2/rev vibration levels result in a roll moment at the gearbox-pylon attachment of 20 percent of the ultimate value. This level is acceptable to maintain flight and to land within the required one-half hour design criterion established for the UH-60A helicopter.

#### DYNAMIC STABILITY ANALYSIS RESULTS

The dynamic stability characteristics of the two-bladed UH-60A tail rotor system were investigated with a Floquet analysis. The analysis uses blade flapping and lead-lag degrees-of-freedom and up to ten air-frame modes. The stiffness, damping, and mass matrices are evaluated for all the blades from the initial conditions specified for blade flap, lead-lag, and pitch motions at various azimuthal positions and integrated for one rotor revolution. The eigenvalues are then calculated and the system stability determined from an inspection of the real part of the eigenvalues. The UH-60A tail rotor blade characteristics and the pylon modes used in the Floquet analysis are summarized in Tables 1 and 2 respectively. The axes sign convention employed throughout this study is shown in Figure 3. The analysis also includes the effect of rotor inflow, blade pitch and twist, and linear aerodynamic characteristics.

Table 1. UH-60A Tail Rotor Blade Characteristics

Parameter	Units	Quantity
Radius	ft	5.5
Radial Location Where Blade Bending Starts	ft	0.3333
Outboard Blade Chord	ft	0.8125
Number of Blades	-	2.0
Rotor Speed (100% $N_R$ )	rpm	1215.0
Weight of One Blade	lbs	19.0
Blade First Inertia Moment	slug-ft	1.2332
Blade Second Inertia Moment	slug-ft <sup>2</sup>	4.1266
Structural Damping	percent	0.50
Equivalent Linear Twist (from center of rotation to blade tip)	deg	- 20.0
Outboard Blade Airfoil Section	-	SC-1095
Tip Loss Factor	-	0.97
First Flatwise Frequency/Rotor Speed	-	1.152
First Edgewise Frequency/Rotor Speed	-	1.696
Air Density	slug/ft <sup>3</sup>	0.002175
Speed of Sound	ft/sec	1102.0
Pitch-flap Coupling, $\delta_3$	deg	35.0
Airfoil Lift Curve Slope	-	6.30
Airfoil Drag Coefficient	-	0.007

Table 2. Tail Rotor Pylon Modes Without Axial Modal Components

Mode	$M_G$	$\omega_G$	$\zeta_G$	$\phi_x$	$\phi_y$	$\phi_{\theta x}$	$\phi_{\theta y}$
No.	lb sec <sup>2</sup> /in	rad/sec	%	in/in	in/in	1/in	1/in
1.	1.3146	41.15	4.5	1.0	.2105	0.	-.017
2.	1.1255	198.13	3.6	-.285	1.0	-.095	-.068
3.	9.9661	395.42	1.8	1.0	.7714	0.	.0

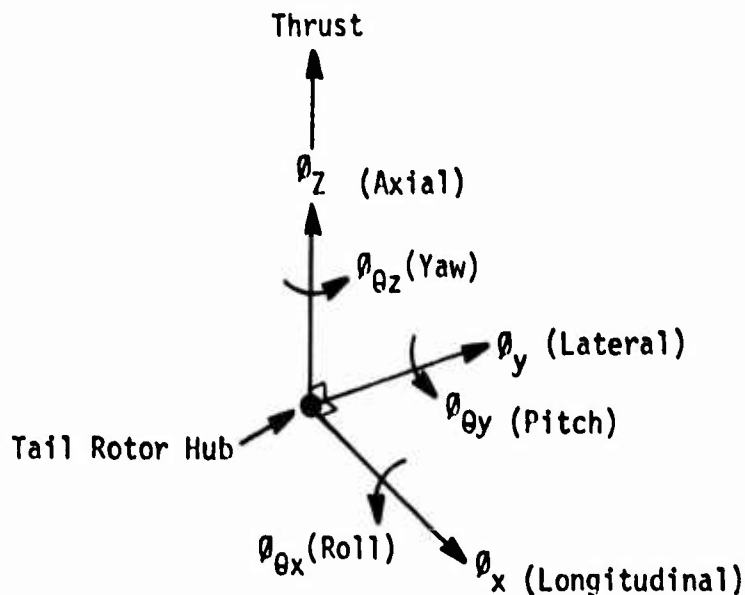


Figure 3. Axes Sign Convention

The results from the Floquet analysis are presented in Figures 4 through 6, for a range in forward speeds from zero to 150 knots. From Figure 4 it is seen that all rotating system (blade) and fixed system (tail pylon) modes are stable in the speed range investigated. The least stable modes are the blade lead-lag mode and the third fixed system mode, both showing a damping level of about one-half percent. The effect of forward speed is not significant except near 150 knots when two of the fixed system modes indicate a degradation in damping level. It is noted that the response of the two blades is not identical due to the presence of the fixed system modes and their interaction with each blade. Exclusion of

the fixed system modes from the analysis simulates a completely rigid hub.

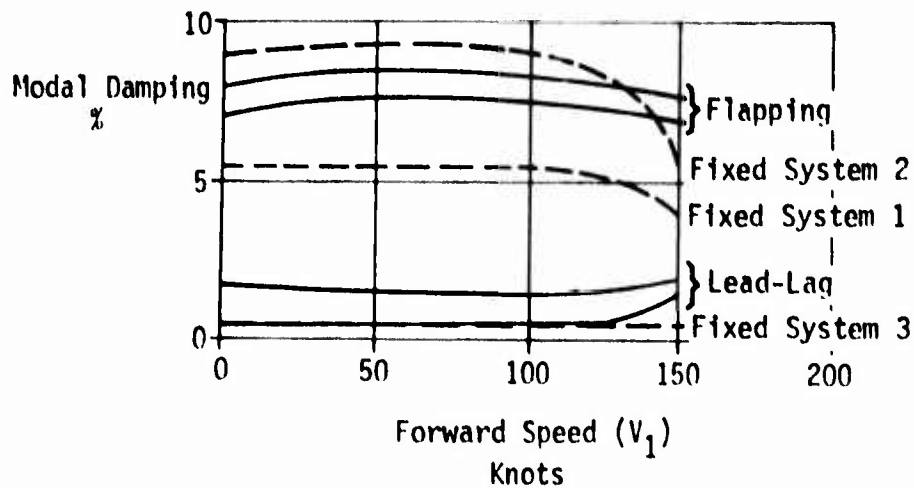


Figure 4. Modal Damping Variation with Forward Speed Including Tail Rotor Hub Flexibility

The damping associated with the blade flapping and lead-lag motions without tail rotor hub flexibility is presented in Figure 5. The results indicate that the blade lead-lag damping is lowered slightly by the flexibility of the hub while the flapping mode shows very little change in stability. Each blade now behaves exactly the same.

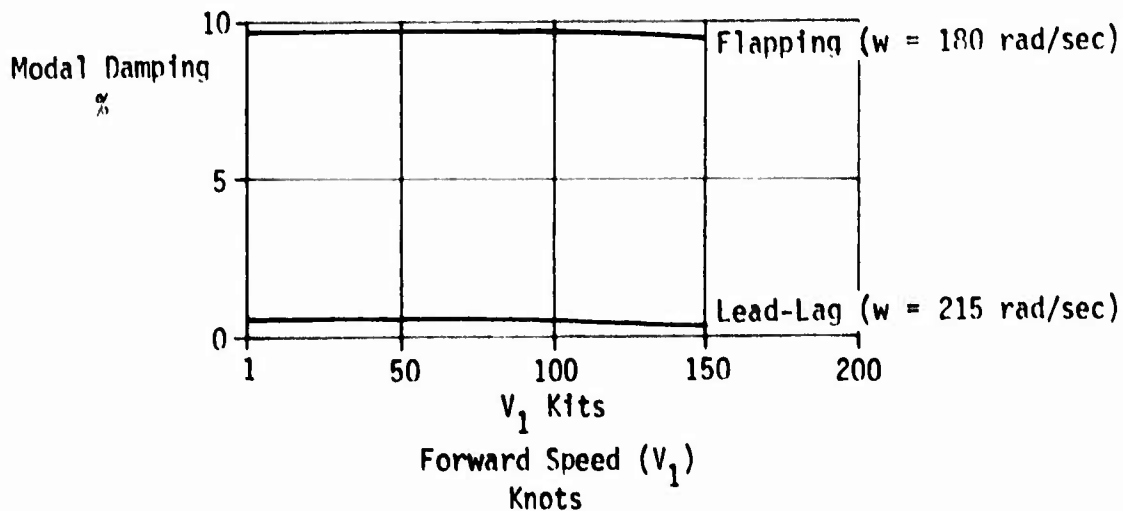


Figure 5. Modal Damping Variation with Forward Speed without Tail Rotor Hub Flexibility

The frequency of the blade and fixed system modes with forward speed is illustrated in Figure 6. This figure shows that the modal frequency is not influenced significantly by forward speed. The blade flapping mode and one of the fixed system modes have frequencies close to each other, especially at 150 knots. The coupling between these two modes results in the damping degradation seen in Figure 4. The frequencies of the blade flapping and lead-lag motions without tail rotor hub flexibility are 180 (1.42/rev) and 215 (1.69/rev) rad/sec, respectively. The increase in the blade flapping frequency over the uncoupled value of 1.152/rev given in Table 1 is due to the pitch-flap coupling of 35 degrees.

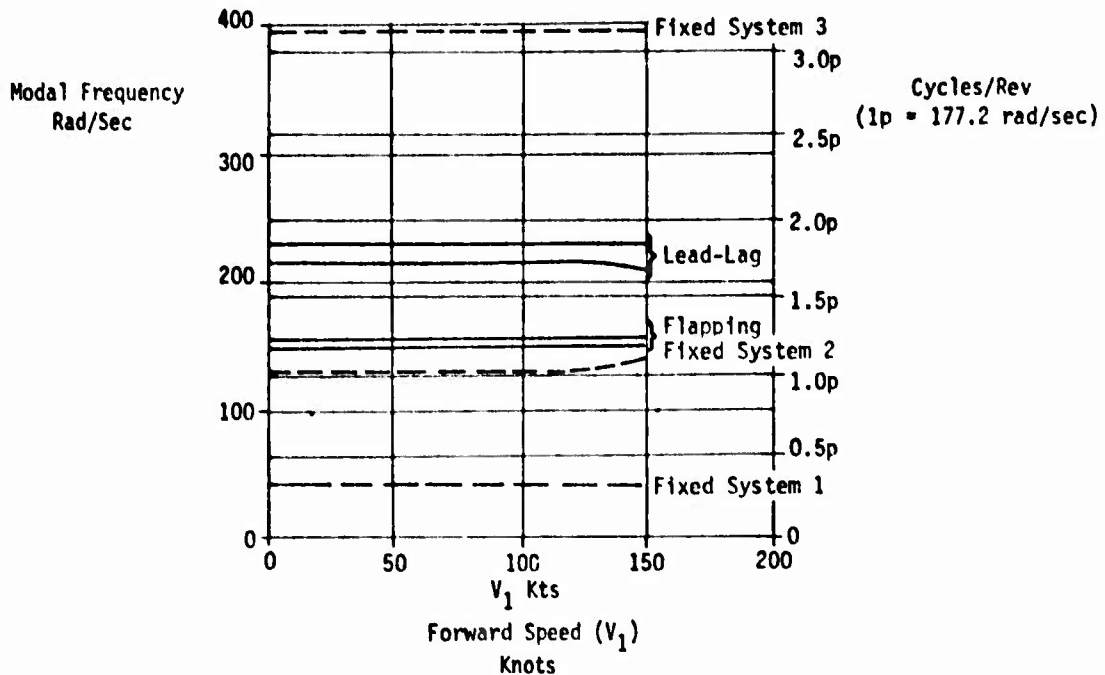


Figure 6. Modal Frequency Variation with Forward Speed Including Tail Rotor Hub Flexibility

#### TAIL ROTOR HUB LOADS AND VIBRATION RESULTS

The aeroelastic behavior of the two-bladed UH-60A tail rotor was investigated in hover and forward speeds up to 150 knots using the time history analysis discussed in Reference 2. The analysis describes the aeroelastic response of the rotor blade by a "normal modes" technique. Five rotor blade degrees-of-freedom (three flatwise, one edgewise, and one torsional) are employed to describe the aeroelastic characteristics

<sup>2</sup> Arcidiacono, P. J., Prediction of Rotor Instability at High Forward Speeds, Volume I; Sikorsky Aircraft; USAAVLABS Technical Report 68-18A, U. S. Army Aviation Materiel Laboratories, Fort Eustis, Virginia, February, 1969, AD-685860.

of the rotor system. Once the rotor flight condition is prescribed (as given by blade collective pitch input, rotor inflow, and thrust), the integration of the equations of motion proceeds around the rotor azimuth at specified intervals for a number of rotor revolutions. The displacements and velocities of all blade modes are then checked at the beginning and at the end of each complete rotor revolution. For a stable condition, this procedure usually takes up to ten rotor revolutions before the modal displacements and velocities repeat themselves within a specified tolerance for a "converged" solution. Once convergence has been reached, the rotor hub loads can be calculated both in a rotating axis system and in a fixed axis system. The hub shears and moments are then harmonically analyzed. For a two-bladed rotor, the hub loads present in the fixed axis system are the steady loads and are at frequencies that are multiples of twice the rotor speed.

The tail rotor thrust and collective pitch at the 75-percent radial location are presented as a function of forward speed in Figure 7. The thrust-pitch relation is consistent with the main rotor torque requirements for level flight operation. It should be noted that at forward speeds greater than 120 knots, the tail rotor operates increasingly in the blade stall region, resulting in degradation of rotor performance and substantial increases in rotor hub loads.



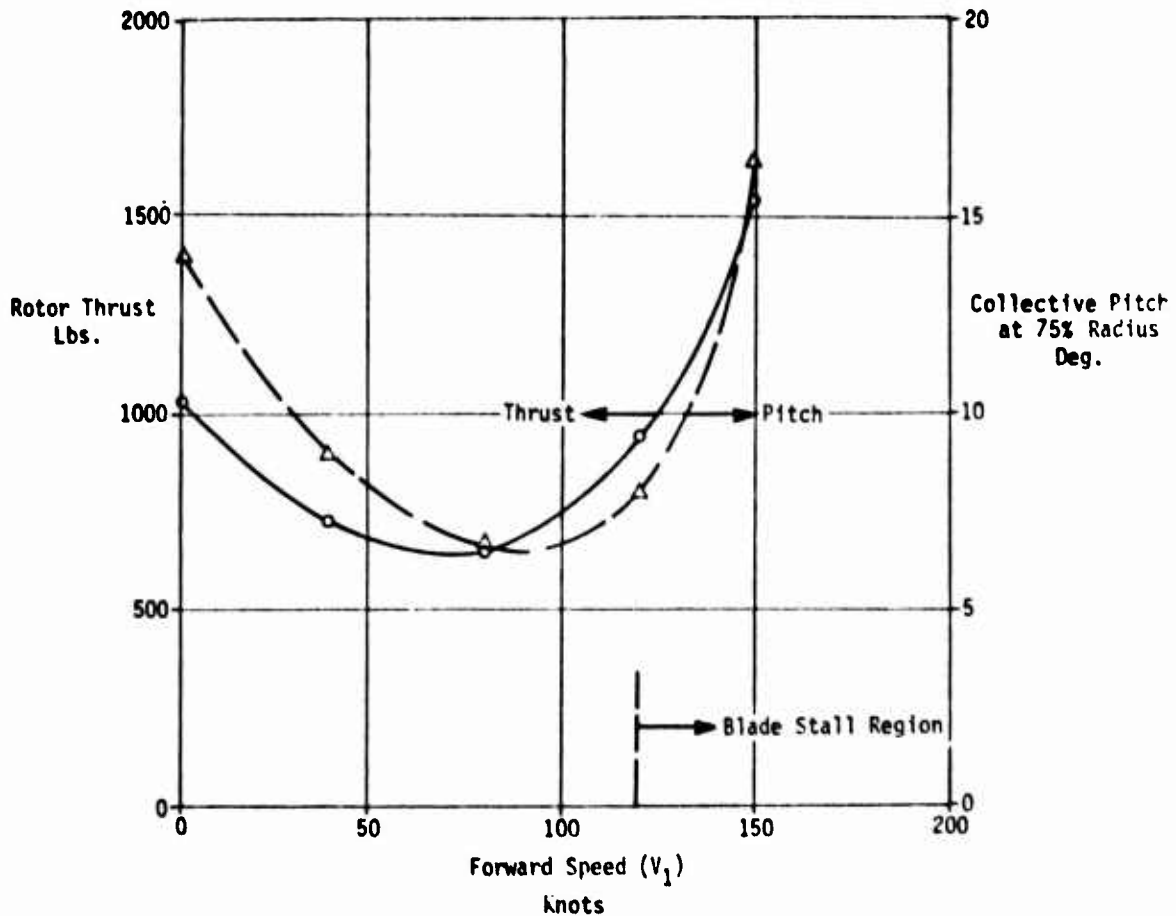


Figure 7. Tail Rotor Thrust and Collective Pitch Variations with Forward Speed

The steady and 2 and 4/rev vibratory hub shears (Figures 8, 9, and 10) and moments (Figures 11, 12, and 13) in the fixed system have been calculated for the forward speed range up to 150 knots. Higher harmonics are not presented since they are small in comparison to the 2 and 4/rev components. The positive directions of the hub shears and moments were previously illustrated in Figure 3. The results presented in Figures 8 through 13 indicate that the rotor hub loads generally increase with

forward speed. All shears and moments except the steady yaw moment increase rapidly at forward speeds greater than 120 knots as the rotor operates increasingly in the blade stall environment.

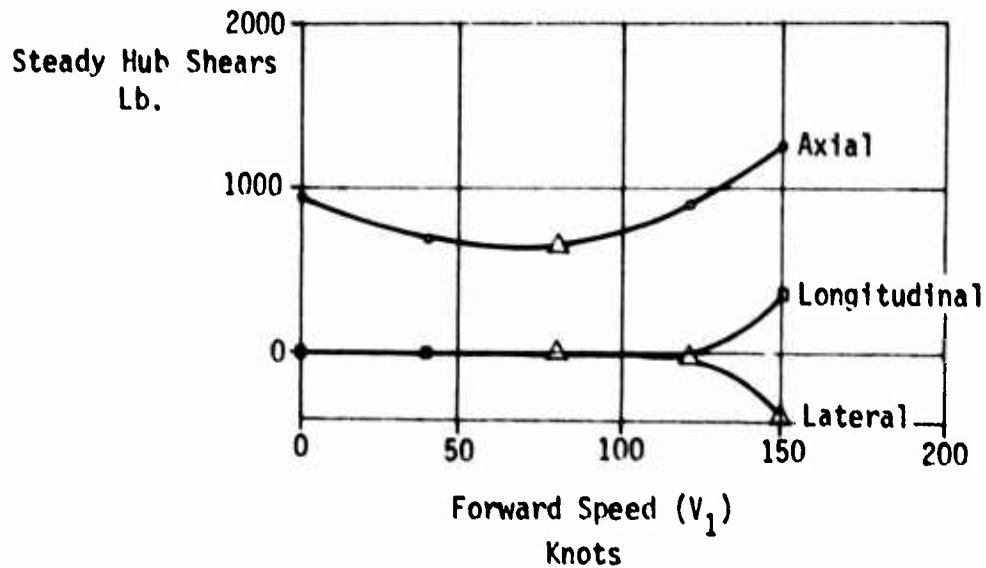


Figure 8. Tail Rotor Hub Shear Load Variations with Forward Speed (Steady Component)

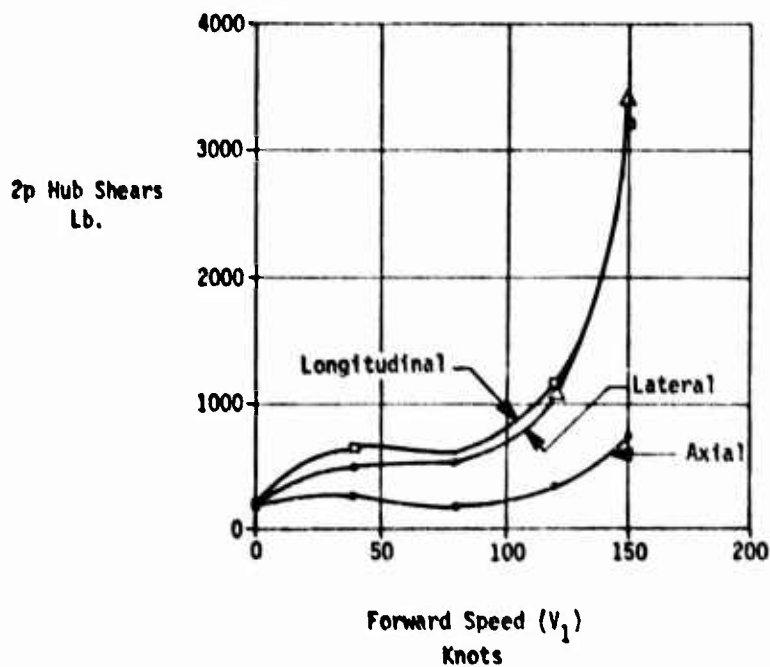


Figure 9. Tail Rotor Hub Shear Load Variations with Forward Speed (2 Cycles/Rev Component)

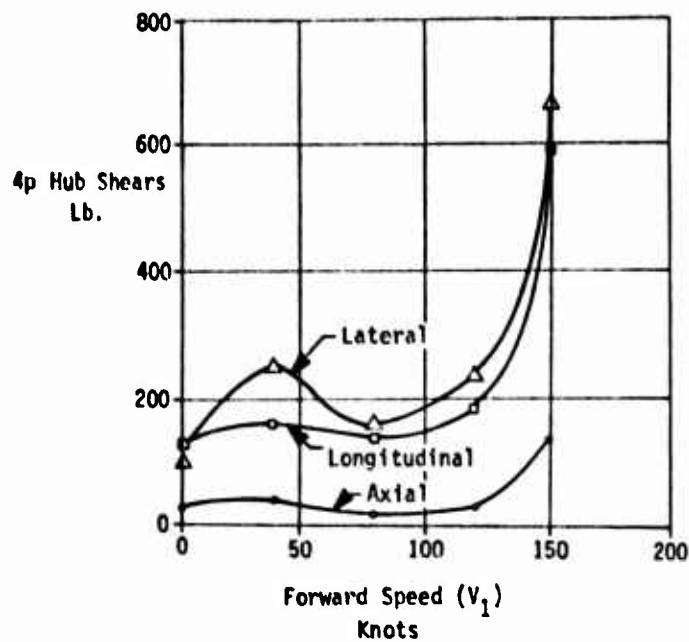


Figure 10. Tail Rotor Hub Shear Load Variations with Forward Speed (4 Cycles/Rev Component)

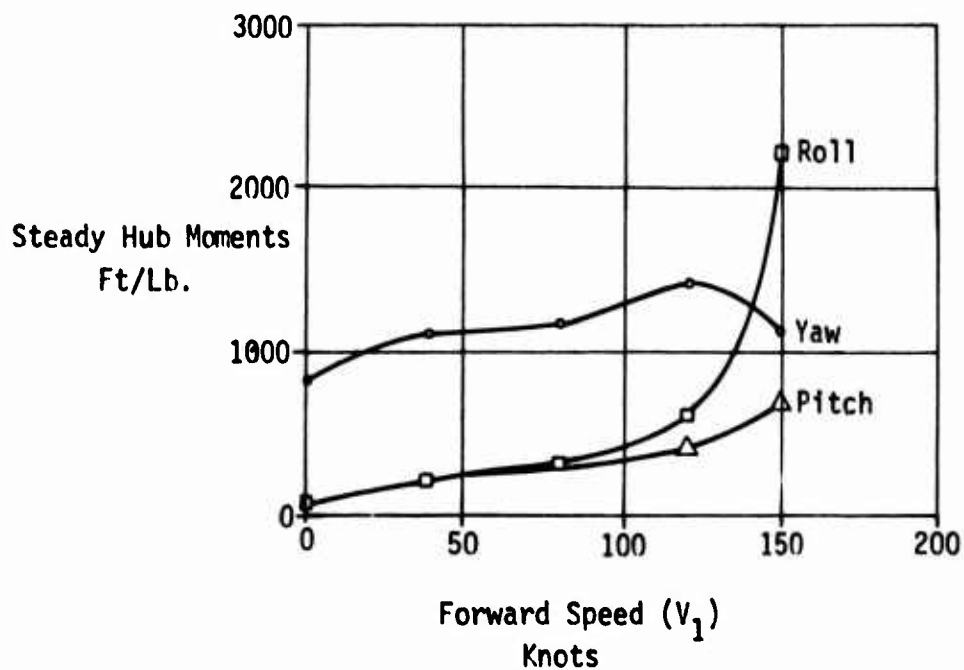


Figure 11. Tail Rotor Hub Moment Variations with Forward Speed (Steady Component)

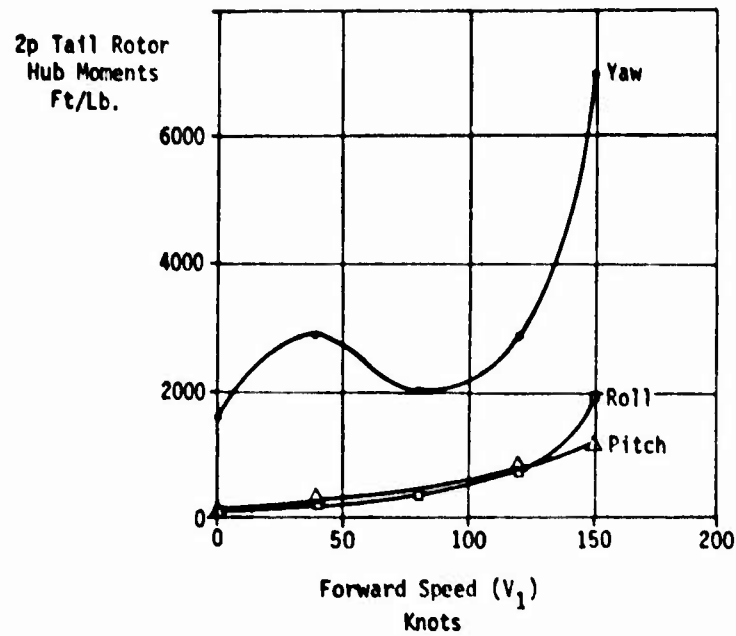


Figure 12. Tail Rotor Hub Moment Variations with Forward Speed (2 Cycles/Rev Component)

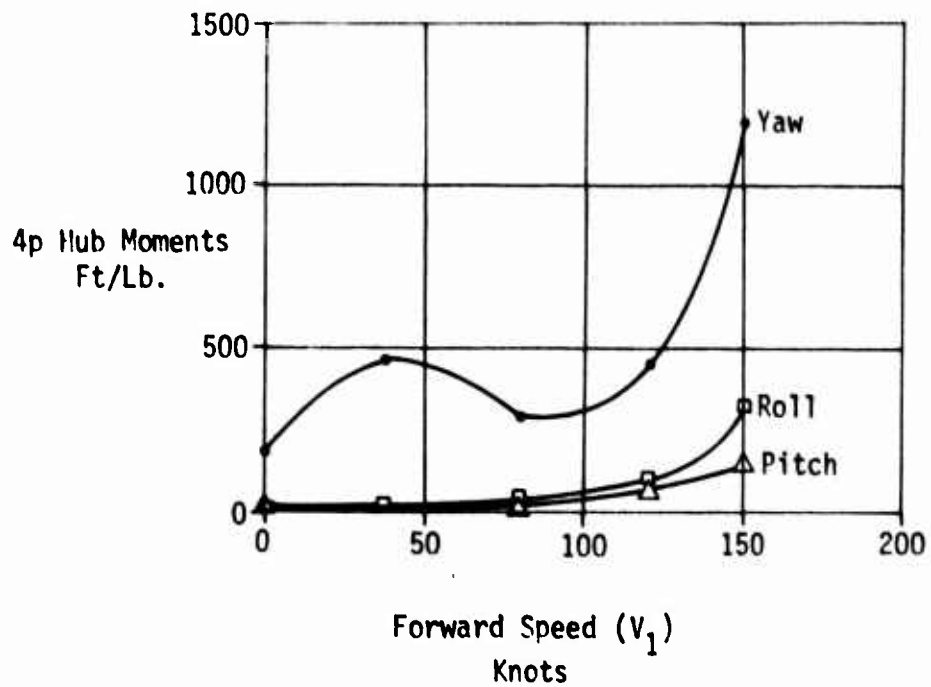


Figure 13. Tail Rotor Hub Moment Variations with Forward Speed (4 Cycles/Rev Component)

The vibratory hub loads are used in conjunction with the tail rotor pylon modes (Reference 3) presented in Table 3 to calculate the accelerations present at the tail rotor hub and gearbox.

Table 3. UH-60A Tail Rotor Pylon Modes Including Axial Modal Components

Mode	$M_G$	$\omega_G$	$\zeta_G$	$\phi_x$	$\phi_y$	$\phi_z$	$\phi_{\theta x}$	$\phi_{\theta y}$
No.	lb sec <sup>2</sup> /in	rad/sec	%	in/in	in/in	in/in	1/in	1/in
1.	0.400	38.32	4.5	.264	.056	1.0	0.	-.004
2.	1.438	182.20	3.6	-.285	1.0	-.519	-.095	-.068
3.	11.980	389.53	1.8	1.167	0.9	1.0	0.	0.

Three linear and two rotational accelerations are computed and plotted in Figures 14 and 15 for harmonic loads of two and four times the rotor speed respectively. The accelerations generally increase with forward speed as expected from the behavior exhibited by the hub shears and moments from Figures 8 through 13. Significant increases in hub and gearbox accelerations are shown for forward speeds greater than 120 knots. It is noted that the 2/rev accelerations are much higher than the 4/rev accelerations.

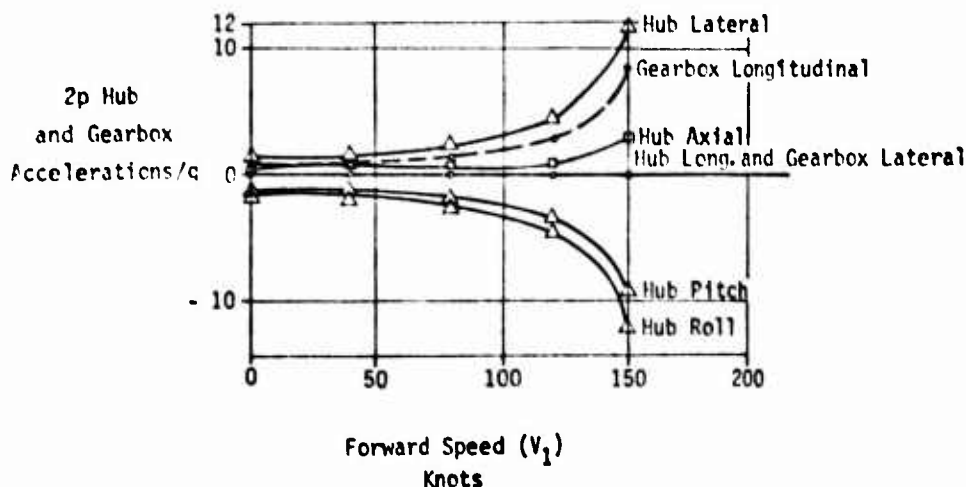


Figure 14. Tail Rotor Hub and Gearbox Accelerations with Forward Speed (2 Cycles/Rev Component)

<sup>3</sup> UTTAS Aeroelastic Stability Analysis, Sikorsky Aircraft, SER-70545, Revision 2, May 1978.

(b) Cycles/Rev Component

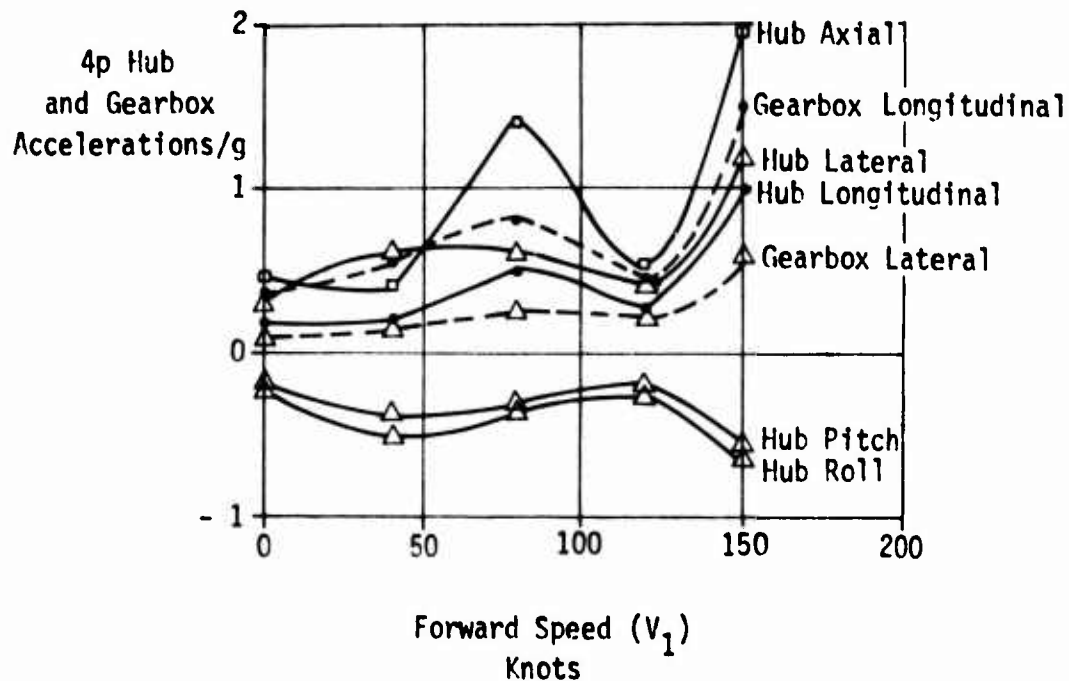


Figure 15. Tail Rotor Hub and Gearbox Accelerations with Forward Speed (4 Cycles/Rev Component)

The accelerations from Figures 14 and 15 are used to calculate the roll moment experienced at the gearbox-pylon attachment, which is a critical stress region. The steady and 2 and 4/rev roll moments at the gearbox-pylon attachment are shown in Figure 16. The highest loaded conditions occur at the maximum forward speed investigated, 150 knots. The 2/rev vibratory response is much greater than the 4/rev response. When added to the steady roll moment, the total 2/rev moment at 150 knots is approximately 20 percent of the ultimate roll moment value of 13,750 foot-pounds. This load level is acceptable to maintain a level flight operation and to conduct a safe landing to meet the required one-half hour criterion.

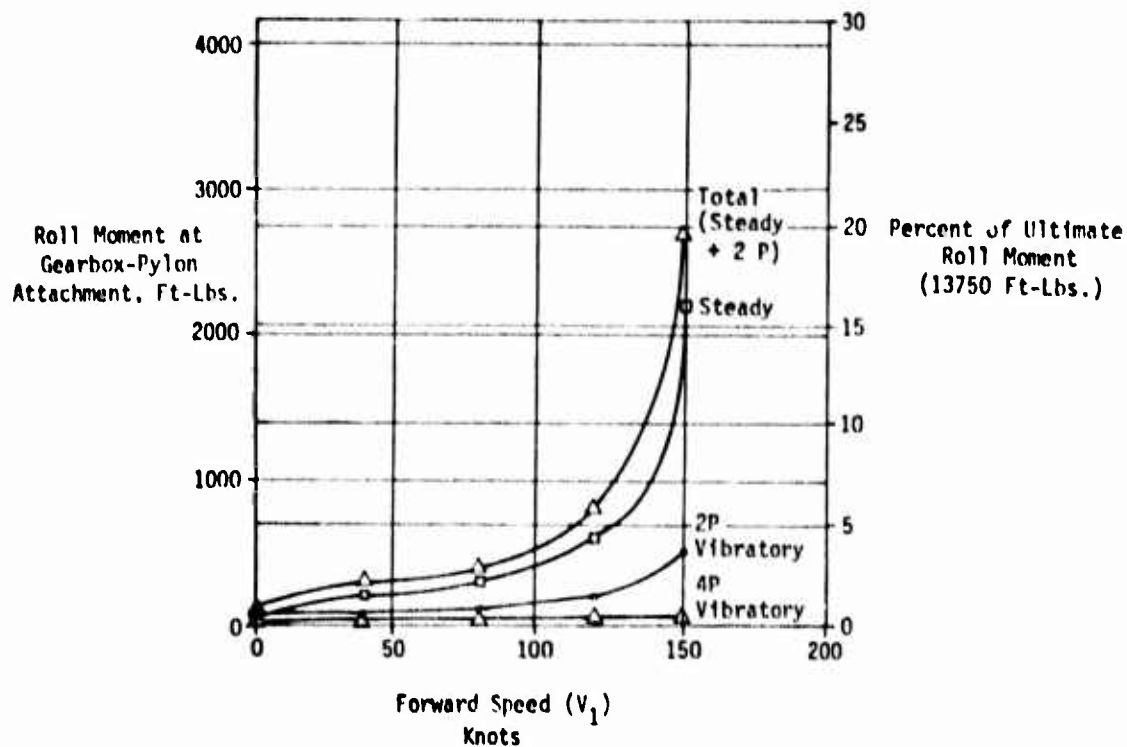


Figure 16. Variation of Roll Moment at Gearbox-Pylon Attachment with Forward Speed

#### STRUCTURAL ACCOMMODATION

The ability of the UH-60A helicopter to structurally accommodate the load caused by tail rotor blade loss has been examined. The analysis is based on the assumption that ballistic damage is limited to the complete removal of the outer 90% of one rotor blade or that area out-board of the back-to-back hub plates and that the load application time is limited to 360 degrees by removal of the opposing rotor blade. The effect of the centrifugal load on the empennage was examined using the UH-60A NASTRAN Structural Analysis Program to determine the deflections of the center of the rotor that can be expected to occur. Figure 17

shows a trace of the excursions of the rotor center through 360 degrees of the load application. With an imbalance load applied in the manner shown in the figure, the trace indicates that the rotor hub center can be expected to deflect approximately 2.2 inches rearward and 5.8 inches forward.

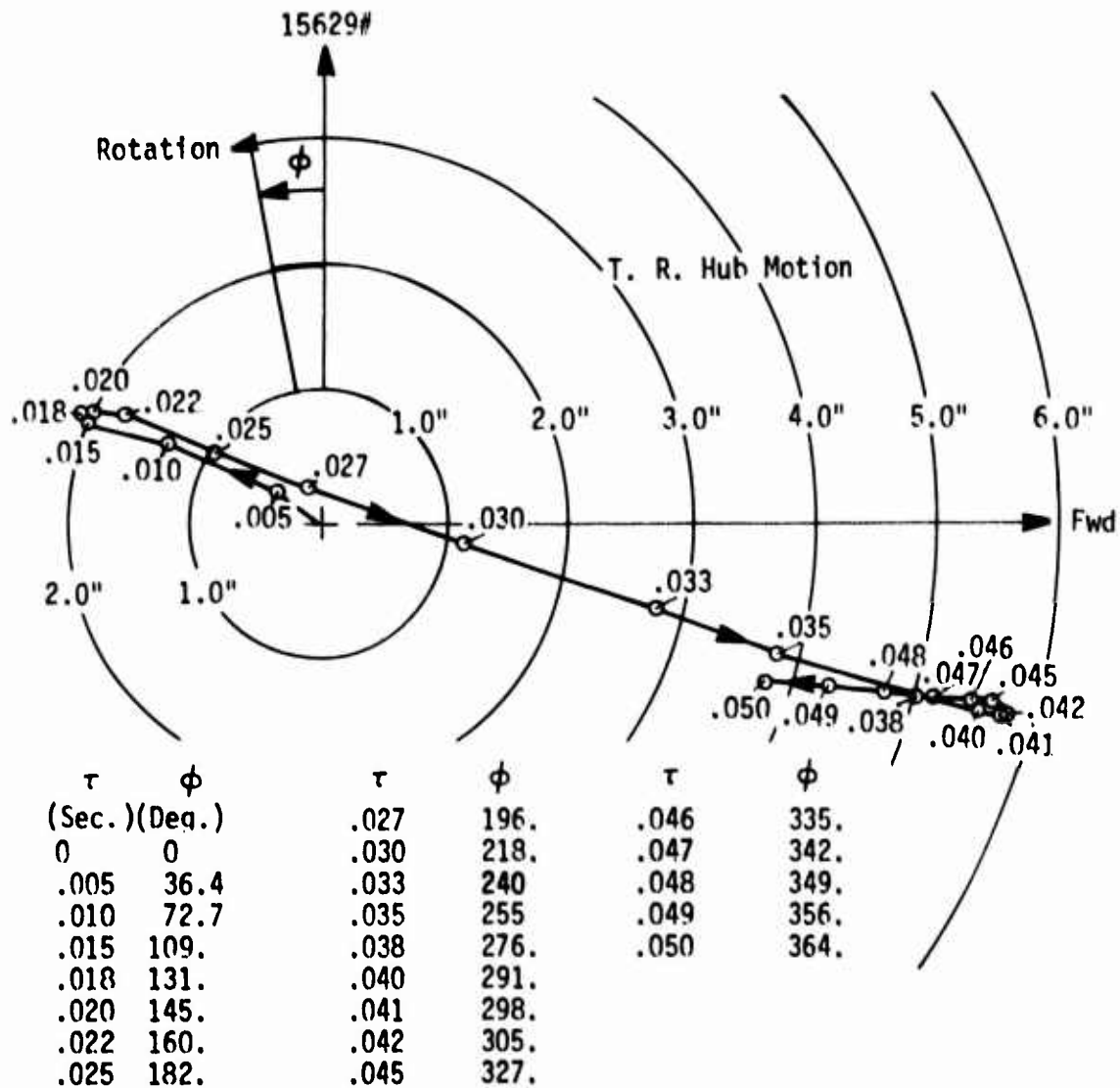


Figure 17. NASTRAN Plot of Tail Rotor Center Excursions



Due to the offset of the rotor hub center from the centerline of the tail cone and pylon, the unbalanced centrifugal load induces both torsion and vertical bending in the pylon and torsion, vertical, and horizontal bending in the tail cone. Examination of the analytical data verifies that these structural deflections all contribute to the motions of the rotor hub center. Quantifying the relative contributions of each of these structural deflections is beyond the scope of the contract. Preliminary examination indicates that the basic tail cone and pylon structure can sustain the unbalanced load over 360 degrees of rotor rotation.

The ability of the tail rotor drive shaft and tail rotor gearbox to accommodate the high centrifugal loads that accompany full blade loss has been examined. Comparing the centrifugal load against the design allowables that were established for these components of the UH-60A helicopter, the loads are expected to exceed the design limits, requiring redesign to accommodate full blade loss. It has been initially determined that the tail gearbox output can be sufficiently strengthened by a material change accompanied by the addition of a process change that will provide the necessary surface hardening characteristics. Further, it is expected that additional strength in the gearbox housing and local pylon structure can be incorporated to provide the necessary structural capability.

#### PITCH LINK ACCOMMODATION

Severing the tail rotor blade spar must be accompanied by severance of the pitch horn or link as well. The level of centrifugal load applied to the link attachment is a function of the weight of the blade remaining after ballistic damage has occurred. If the point of ballistic impact is well outboard on the rotor blade, the residual centrifugal force would be sufficient to effect automatic separation of the link as well. However, in the event that the point of ballistic damage occurred immediately outboard of the pitch horn, the resulting level of centrifugal force would be insufficient to be confident that the separation of the pitch horn would not be delayed causing the trajectory of the pitch horn to be toward the helicopter proper.

## PART II SYSTEM DESIGN

The automatic tail rotor blade jettison system is designed to effect removal of the residual portion of a severed blade and, sequentially, its opposing blade within one full rotation of the rotor system. The system confines blade jettison to an aftward/downward direction to avoid possible secondary damage to the helicopter proper or its occupants. The system is fully solid-state to achieve maximum operational reliability and employs state-of-the-art techniques to prevent inadvertent actuation.

The system is comprised of four basic elements: an electrical power transfer to the rotor system, damage detectors that initiate system operation, a logic system that determines the blade pair to be jettisoned and provides means to control the direction of blade separation, and pyrotechnic devices that sever the blade spar and associated pitch horn for blade jettison. Figure 18 is a block diagram of the system showing the interrelationship of the basic elements. The prototype system designed for fabrication and evaluation testing differed from a fully productionized configuration in several respects. Development of the pyrotechnic devices was not required, allowing evaluation tests to be performed using an engineering-type rotary test stand previously developed for other programs. As a further expedient of the evaluation tests to be performed on the system, manual switching was incorporated to allow selectable faulting of the two portions of the logic circuitry.

The prototype system has been designed to be compatible with the electrical system, rotor system, tail rotor gearbox, and deicing kit of the UH-60A.

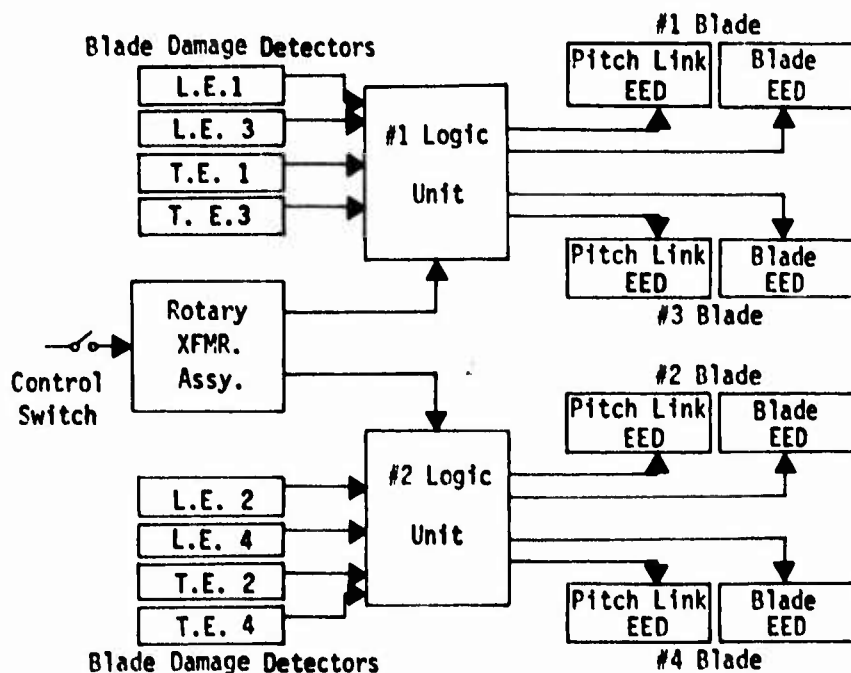


Figure 18. System Block Diagram

Figure 19 is the circuit diagram for the automatic blade jettison system. The diagram indicated the four basic elements of the system and the components that comprise those portions.

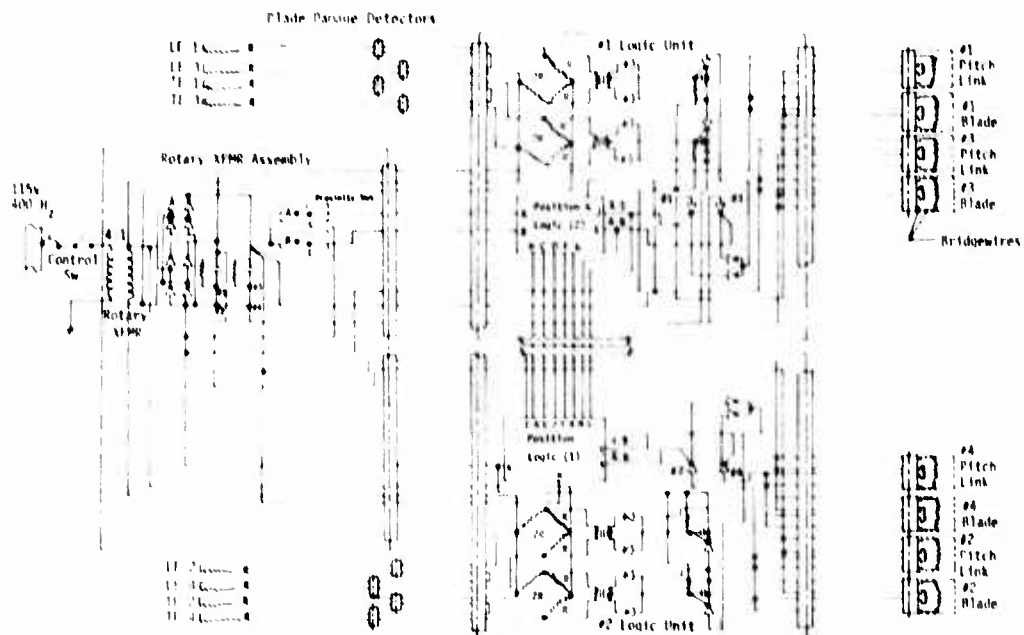


Figure 19. Tail Rotor Balance Restoration System Schematic.

ELECTRICAL POWER TRANSFER - Electrical power to operate the automatic blade jettison system is transferred from the nonrotating aircraft structure to the rotating rotor system by means of a rotary transformer. The transformer is comprised of two subassemblies: an inner frame with the primary windings of the transformer that mounts on the tail gearbox housing and an outer frame with secondary windings that is installed to rotate with the rotor system. The transformer is designed to accept 115 vac, 400 Hz aircraft power and to provide an output of 24 vdc that allows use of aircraft-type hardware. Unlike conventional transformers, the rotary transformer is designed to operate even though the components are moving with respect to each other and efficiency of the transformer's output is directly related to the narrowness of the gap between the induction plates of the two halves of the transformer. Although the output level of the rotary transformer is normally lower than that achievable with the conventional transformer, the output is more than adequate for the intended application.

The rotary transformer was selected as the electrical transfer device in lieu of the more conventional collector ring approach to minimize the requirement for field level maintenance. This not only reduces the operating costs but, perhaps more importantly, minimizes the possibility of field maintenance-induced malfunctions.

The 13-inch transformer for the UH-60A blade jettison system (see Figure 20) is the largest transformer of its type designed to date, the size of the device being dictated by a need for compatibility with the rotor blade deicing kit of the UH-60A. The transformer (part number 207073) was designed to meet Sikorsky performance requirements by Superior Electric Company of Bristol, Connecticut. Two proximity switches are assembled to the rotary transformer that gate the power output to the blade severing charges to control the direction of blade separation. These switches are installed with the transformer as a convenient and practical location to relate the gating function to rotor rotation and to maintain a kit-type approach for the installation of the blade jettison system. The proximity switches operate 90 degrees out of phase with respect to each other. Each switch is associated with one pair of opposing blade paddles. Each proximity sensor transitions from "closed" to "open" or the reverse as determined by the placement of metal targets that are installed in accordance with the blade jettison window requirement. The direction of blade jettison can easily be controlled by this design approach.

The proximity switches selected for the system are fully qualified with a mean-time-between-failures of 200,000 hours. The device, manufactured by Eldec Corporation of Lynnwood, Washington (part number SC08-260), has a switching rate capability of greater than 20,000 cycles per minute and has an operating temperature range of -65° to +180°F.

Included also as a part of the rotary transformer assembly is power rectification and charge storage capacitors that provide sufficient output to initiate the electro-explosive detonators that, in turn, initiate the blade severing devices. The relatively high power requirement to

achieve reliable initiation of the four EED's for jettison of the blade pair is achieved by capacitance discharge. Two storage capacitors are installed that charge following arming of the system by the pilot.

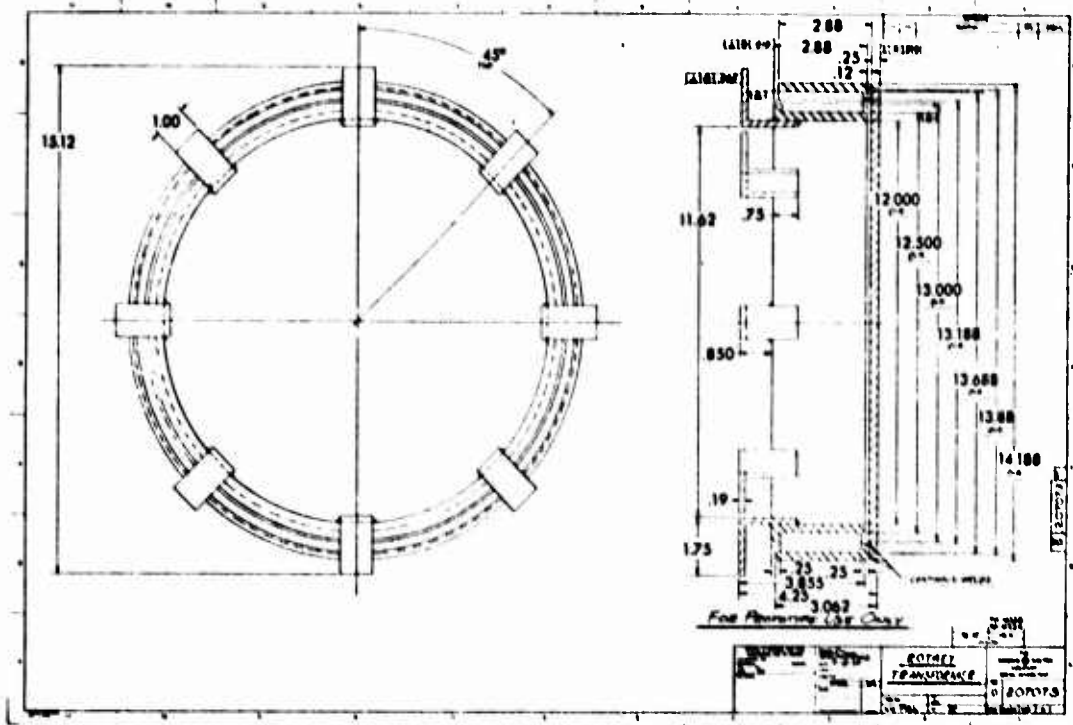


Figure 20. Prototype Rotary Transformer Fully Compatible with the UH-60A Tail Rotor Gearbox and Deicing Unit

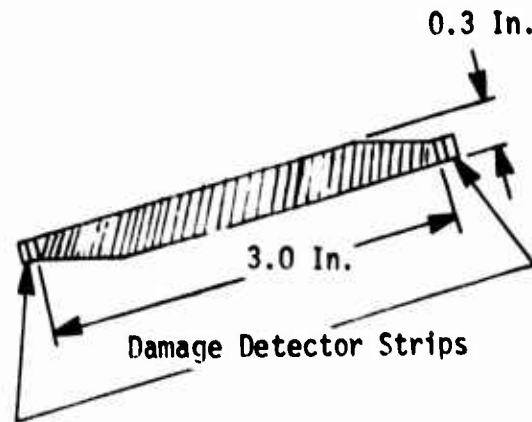
DAMAGE DETECTORS - Two sets of detectors are employed with each blade paddle to detect blade spar damage. Specifically, they are intended, by the manner in which they are installed, to differentiate between ballistic damage to the blade that is of a tolerable nature and that which will result in an intolerable rotor imbalance. This is achieved by locating independent detectors along both the leading edge and trailing edge of the blade spar. The logic system is designed to require an input from both detectors in order to activate the blade severing pyrotechnic devices. In this way, ballistic (or other) damage that does not cause spar separation will not result in blade jettison.

The detector assembly for the UH-60A is comprised of two thin strips of graphite epoxy, the same material from which the spars are fabricated, to obtain the same physical characteristics and thereby avoid differential elongations due to temperature and centrifugal force. The two halves of the detector assembly are insulated from each other and bonded together. For production installations, the detector assemblies are installed by bonding in position along the edges of the spar prior to application of the outer fiberglass wrap. For test applications where blade retrofit is required, the detector assemblies are potted in position along the spar edges following preparation of the blade by longitudinal saw cuts to a depth that is sufficient to expose the spar edges.

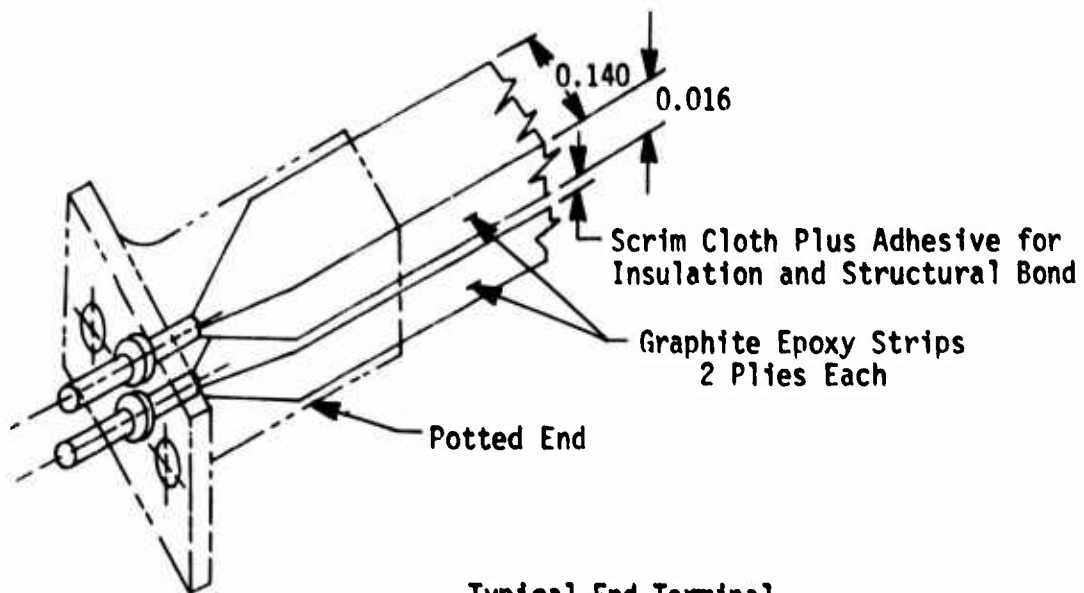
The electrical properties of the graphite epoxy allow the use of the material as a conductive element having a useful resistance level for the intended application. The detector assembly is essentially a circuit that serves to balance a conventional wheatstone bridge. As long as the circuit's resistance level remains within acceptable tolerance limits, the logic system remains inactive with regard to blade separation initiation.

In the event that the detector assembly circuitry is interrupted or the resistance level becomes significantly changed beyond the established tolerance limits, the bridge becomes unbalanced and the logic unit "senses" a fault. When both circuits exhibit faults, the logic unit has "sensed" a failed spar condition and blade jettison is initiated. In order to effect a positive indication of resistance level change, the detector assembly includes the installation of a resistor at the outer end of the spar; circuit interruption then results in significant resistance level change. The resistor further serves to allow tuning of the circuit, if required. The inner end of the detector assembly terminates in a small potted end fitting that has posts for attachment of the wires leading to the logic unit. This connection is located under the rubber boot near the root of the blade and is provided to allow rapid rotor blade change.

Figure 21 shows the general arrangement of the detector assembly. Detail design of the detector assembly was not required for the evaluation test work and was beyond the scope of the contract.



Graphite Epoxy Spar Cross Section



Typical End Terminal

**Figure 21. Damage Detector Assemblies (Fabricated from Spar Material for Elongation Compatibility)**

LOGIC UNIT - This unit is comprised of a number of switches (normally open) that gate the power output to the proximity sensors. These series oriented switches change from "Open" to "Closed" when the associated detector assembly faults and its wheatstone bridge becomes unbalanced. Silicon controlled rectifiers (SCR) were selected to perform the switching function to achieve highly reliable, solid-state performance. The logic unit also includes position logic circuitry that allows two proximity sensors to perform the timing function for the entire rotor. This is achieved by means of two additional SCR's that switch over the proximity sensors to the affected blade pair. Also included in the logic unit are the remaining three legs of the wheatstone bridge. Two logic units are required for the four-bladed UH-60A tail rotor system.

ROTOR BLADE SEVERANCE - Pyrotechnic severing devices are installed at the root of each rotor blade and on the pitch horn to effect jettisoning of the blades. The devices are both comprised of linear shaped charges supported in silicon rubber and installed in fiberglass housings. The spar severing devices are installed adjacent to the spar, immediately outboard of the rotor hub plates under the existing rubber boot of the blade. The pitch horn severing devices are installed at the horn's smaller, outer end and are nested in the cavity of the component.

The development of the actual blade and pitch severing devices was not required by this contract. Certain preliminary work has been performed which verifies that the UH-60A graphite epoxy spar can be severed by a linear shaped charge of acceptable charge size to be compatible with the intended application. Figure 22 is a photograph of a segment of graphite epoxy spar assembly of the UH-60A material type and thickness that was successfully severed by 200 grains per foot charge loading in the cross-grain manner required for a blade separation. This test performed by Teledyne McCormick Selph, was a preliminary effort only to ascertain feasibility of severing graphite epoxy spars by pyrotechnic means and no attempt was made to optimize the charge size. It is estimated that the production severing charge would be lead-sheathed and would fall in the size range of 125 to 150 grains per foot using RDX (Cyclotrimethylenetrinitramine).

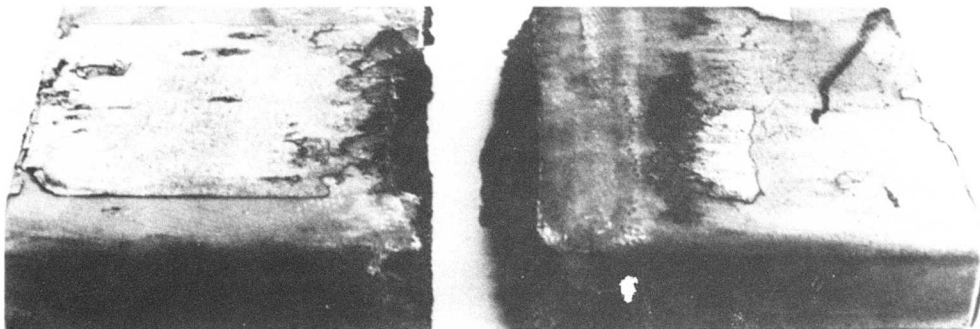


Figure 22. Graphite Epoxy Spar Severed by Linear-Shaped Charge



The chevron-shaped LSC's of both the blade severance assembly and the pitch horn severance assembly are initiated by electro-explosive detonators (EED) that are installed in the housings. Two approaches are considered to be acceptable for the severance assemblies. The first employs a single dual bridgewire EED for LSC initiation and achieves redundant initiation by means of the duality of the EED's bridgewires. The other approach, expected to be superior in terms of severance reliability, employs two individual EED's, each having single bridgewires. The EED's are physically located at opposite ends of the LSC to maximize the redundancy capability.

The blade and pitch horn severance assemblies are initiated simultaneously by the electrical power output from the logic unit. Quick disconnects are provided to accommodate blade removal/installation. The built-in test capability of the system allows preflight verification of circuit continuity up to, and including the bridgewires of the EED's to avoid a maintenance-induced error during blade replacement.

Figure 23 shows the general arrangement of the various components of the system installed on the UH-60A tail rotor.

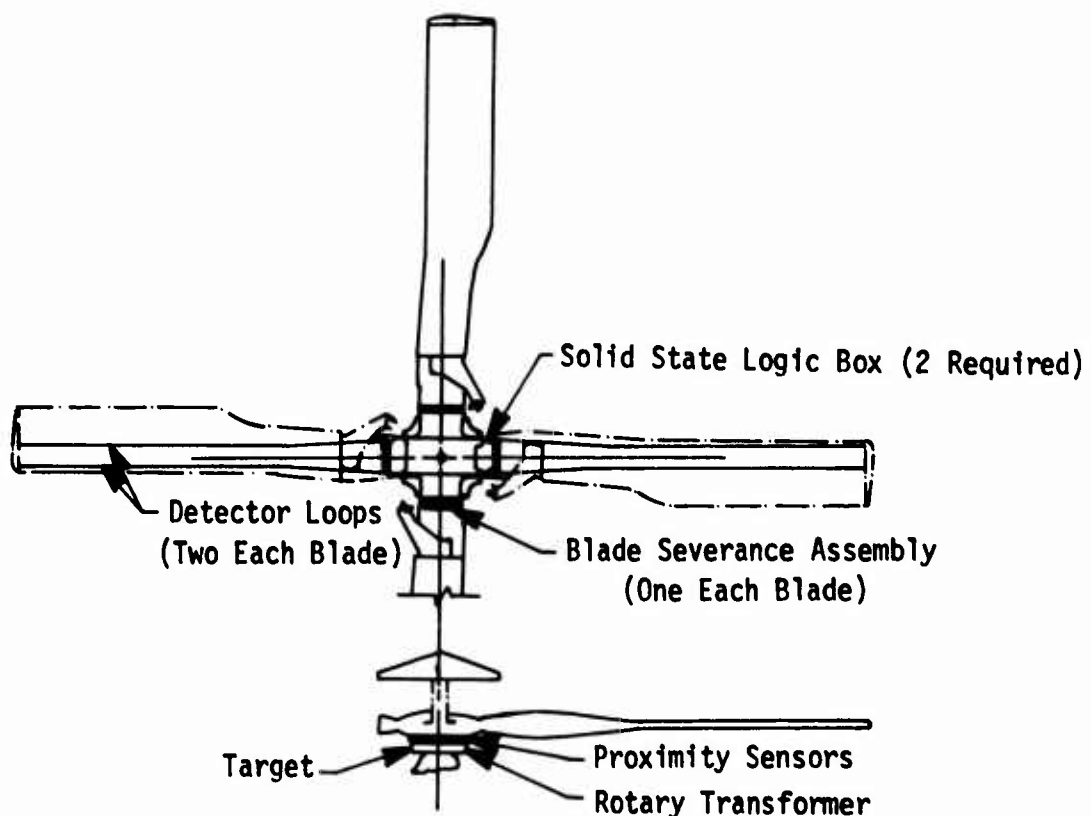


Figure 23. General Arrangement - Tail Rotor Blade Jettison Concept

SYSTEM SAFETY AND RELIABILITY CHARACTERISTICS - The following general discussion pertains to the characteristics that are, or can be, incorporated into a production version of the automatic blade jettison system that enhance reliability of operation and that enhance safety with use of the system.

#### RELIABILITY

- . Electrical components are selected to be working at approximately 50% of their rating. This practice was not employed during prototype development in order to allow any possible problem areas to surface.
- . Entire system circuitry can be preflight checked to verify operational status. All test functions, however, are removed from the airborne system in order to minimize system complexity and part count.

#### SAFETY

- . The system incorporates three SCR interlocks ahead of the firing of the EED's to prevent inadvertent blade jettison without prior loss of a blade or blade segment.
- . A control switch is employed to allow the system to be armed at the discretion of the pilot.
- . The storage capacitors are subjected to intentional discharge by bleed resistors following shutdown to maximize safety during performance of maintenance.

#### IMPACT DAMAGE

- . The logic units are fully encapsulated.
- . The rotary transformer assembly employs encapsulation.
- . The blade damage detector circuits and terminal resistors are buried within the leading and trailing edges of the blades.
- . The pyrotechnic linear shaped charges are insensitive to impact and are located such that the possibility of impact damage is remote.

#### HEAT DAMAGE

- . All components selected are compatible with the temperature requirements of the UH-60A.

### LIGHTNING

- . Tail rotor blades are covered with aluminum mesh that is grounded to the airframe. Lightning strikes will be conducted on the blade surface and not through the graphite epoxy detectors.

### MAINTENANCE

- . The EED's are disarmed during maintenance when the test box harness is installed to prevent inadvertent system initiation during maintenance of the system.
- . Power levels employed to conduct circuit continuity checks are well below the level required to initiate the EED.
- . System design is such that two ground faults are required before the system can actuate; ground faults are detected in the preflight test box.

### STATIC ELECTRICAL DISCHARGE

- . The aircraft has adequate static discharge wicks on the stabilator trailing edges to prevent static charge buildup.
- . Any small corona discharges that may develop from the tail rotor blades are insufficient to set off the blade severance system.

### STRAY VOLTAGE OR INDUCED CURRENTS

- . All SCR's incorporate anode/gate shunt capacitors to prevent inadvertent change of switch state.
- . Wheatstone bridge resistors are shielded to prevent inadvertent change of switch state.
- . The blade severance system wiring is separated to the maximum extent possible from the tail rotor blade deicing system.

### PART III SYSTEM FABRICATION AND EVALUATION

System performance evaluation has been completed on a prototype fabricated in accordance with the schematic shown in Figure 19. The prototype system includes a rotary transformer, electrical power rectifiers, two logic units, two proximity sensors and targets, and fuses to simulate initiation of EED's. The system evaluated includes a capacitance discharge concept to initiate the fuses that provide the required indications to verify proper system performance and timing.

Figure 24 shows the various components of the system with the covers removed. For the test program, the electronic components are attached to a mounting plate that secures to the rotating portion of the rotary transformer. The fuses used to provide initiation indication are installed in a light assembly at the four quadrants that represent the associated blade positions. A switch box is visible that allows either logic unit to be independently selected for testing. The slip ring assembly located at the center of the system is included as test equipment to transmit the system initiating faults and to pick off output signals that verify the positional relationship of the initiated components during the tests.

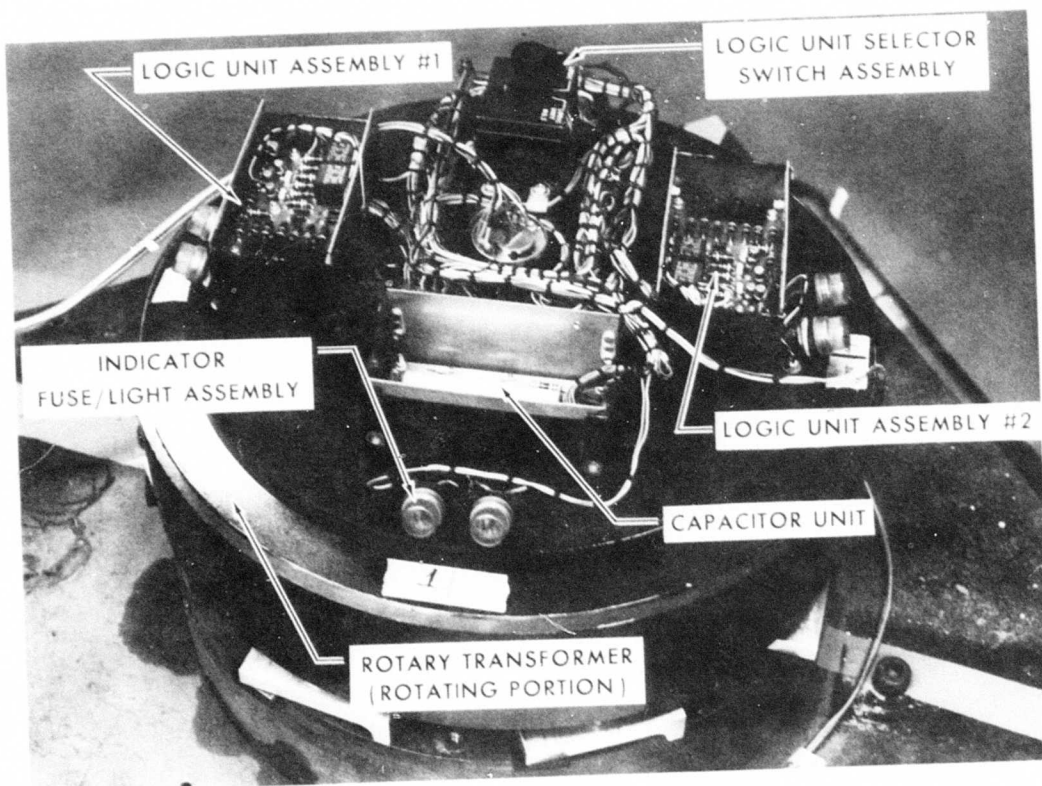


Figure 24. Prototype System Installed in Test Stand

The prototype system was installed on an engineering test stand previously developed for similar test work and upgraded to provide the high-speed capability consistent with a tail rotor application. The stand, shown in Figure 25, includes a protective drum around the upper area for safety reasons during the test operations. The test stand is belt-driven by a variable speed motor capable of rotating the system to speeds up to 1800 RPM. Also visible in Figure 25 is a small control panel containing the switches required to control the test stand drive motor to control power to the rotary transformer, and to introduce the faults that simulate interruption of the damage detectors.

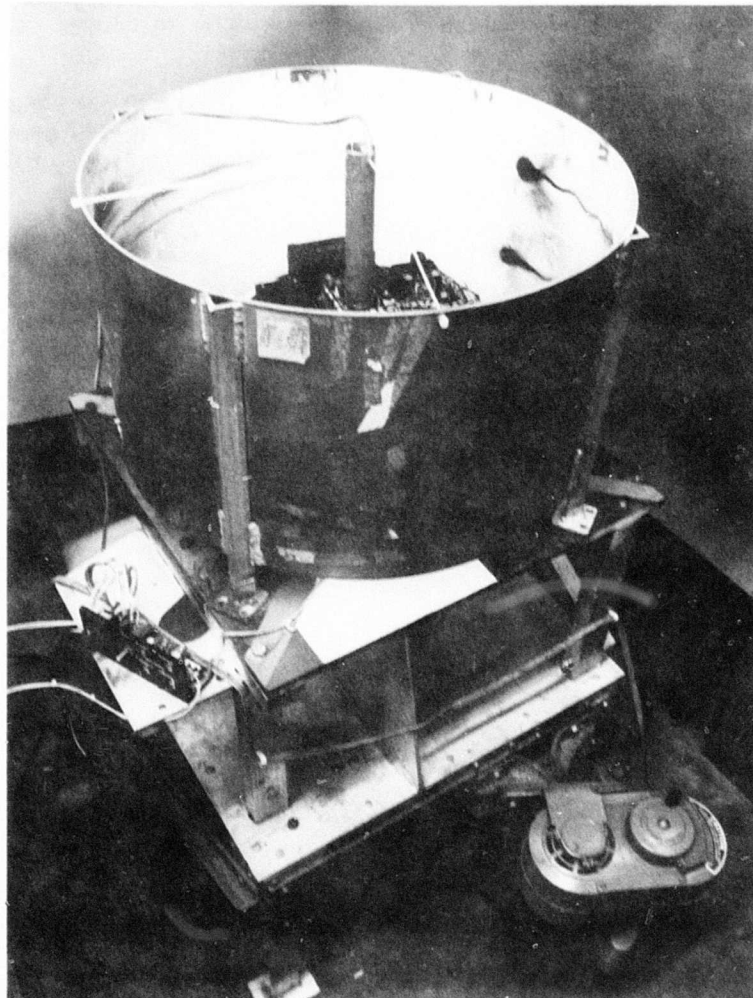


Figure 25. Engineering Rotary Test Stand used for Evaluation of Prototype System Performance Capability

**EVALUATION TESTING** - Tests were run to determine the positional relationship of certain components of the prototype system in order to verify that the system meets the jettison window requirements of the UH-60A helicopter. This was accomplished by displaying EED initiation (simulated by the use of fuses) and the open/closed status of the proximity switches using a Techtronix 654 scope with 4 trace memory. This approach allows the measurement of the time lapse between the change in state of the proximity sensor and the initiation of the EED. Further, the display provided visual verification that both blades would be jettisoned at the proper location as controlled by the location of the target. It should be noted that the EED's are initiated at a change in state of the proximity switch and the data recorded, therefore, indicates initiation only at the point where the proximity switch changes from open to closed state or the reverse.

In accordance with the system performance test plan, 28 test runs were performed using the engineering rotary test stand to verify proper prototype performance throughout the rotational speed range of 70% Nr to 150% Nr in accordance with:

<u>%N R</u>	<u>Equivalent RPM</u>	<u>Number of Tests</u>
70	834	2
80	954	2
90	1073	2
100	1192	12
110	1311	2
120	1430	2
130	1550	2
140	1669	2
150	1788	2

The prototype system successfully met the performance requirements in all tests performed, and compatibility with the UH-60A window for tail rotor blade jettison has been verified. Due to the repetitive nature of the data obtained, only the data for the 100%  $N_R$  run is included here (see Figure 26); the remainder of the data is included as Appendix A to this report. Figure 26 is the photographic record of the Techtronix scope with the various elements defined. By using this data recording approach, it was possible to record data with the required degree of accuracy.

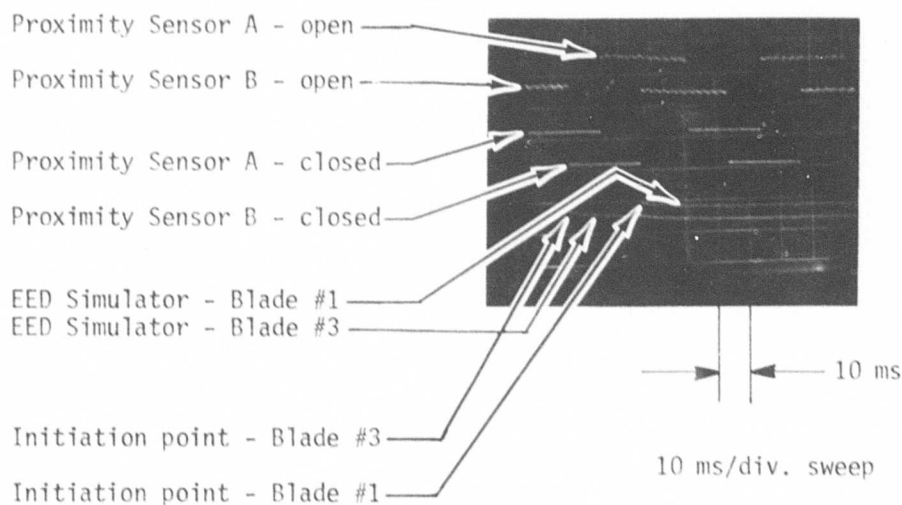


Figure 26. Prototype Performance Data - 100%  $N_R$  (1192 RPM)

The testing performed in this manner confirmed that the prototype system components were operating properly, in correct sequence, and with sufficient speed to effect blade jettison within the window tolerance limits established. An additional test was needed to verify that the severance signal occurred at the proper rotational position with respect to the location of the window. This was verified by the use of a strobe light, triggered by the output signal from the appropriate proximity switch. Since the oscilloscope record verified that the response times of the components were proper, positional accuracy of the system is a function of the response time of the proximity sensor. By utilizing the output of the proximity sensor to trigger the strobe light, rotational indexing and the output variance throughout the speed range of 834 RPM to 1788 RPM could be determined. Using this technique, it was determined that the positional characteristics of the system were well within the tolerance limits of the UH-60A blade jettison window and that the point of blade jettison varies less than six degrees throughout the entire speed range. Since the 150%  $N_r$  speed is well beyond the normal operating limits of the UH-60A helicopter, the variation is considered of negligible significance.



## PART IV FLIGHT SIMULATION ANALYSIS

An extensive simulation analysis program was conducted to determine the effects that the programmed blade jettison can induce on the performance characteristics of the UH-60A helicopter and to assess the handling qualities to be expected. The Sikorsky General Helicopter (GEN HEL) UH-60A flight dynamic simulation program and PDP-10 Hybrid Computer were employed to study the changes in helicopter trim conditions. By coupling a new subroutine for the transitional, four, to three, to two-bladed rotor condition with the basic GEN HEL Program, it was possible to ascertain the effect of the imbalance loads on the helicopter. To ascertain the change in handling qualities to be anticipated with the blade jettison, the GEN HEL Program was interfaced with the Sikorsky cockpit simulator for qualitative pilot assessment in the normal four-blade mode followed by transition to the two-blade mode.

### METHODOLOGY

The tail rotor blade severance scenario was considered as four consecutive, but distinct, handling qualities situations and the GEN HEL Program was employed to study all four of these situations:

1. Helicopter trim with four tail rotor blades
2. Severance transition from four-to three-to two tail rotor blades
3. Pilot response to loss of two opposing blades
4. Helicopter trim with two rotor blades, if possible

The basic GEN HEL Program was used to obtain UH-60A trim conditions with either four or two tail rotor blades for flight conditions and loading configurations that represent the most critical - but realistic - situations for tail rotor blade loss. A subroutine was written to program, in detail, the loads at the tail rotor during the imbalance period. This subroutine was coupled with the GEN HEL Program to produce the proper interplay between the response of the helicopter and the loads generated at the tail rotor. The UH-60A GEN HEL Program was interfaced with the cockpit simulator to determine how well the aircraft could be recovered from the loss of two opposing tail rotor blades and the flight conditions that would have to be assumed to continue flight following initial recovery from the helicopter's reaction to tail rotor blade loss. Table 4 presents the axis system, parametric definition, and sign conventions used in the program.

### BASIC PROGRAM

The GEN HEL Program is an analytic helicopter model developed by Sikorsky Aircraft and is used as the primary handling qualities design analysis tool. This computer program is a fully coupled, nonlinear model of the helicopter, containing detailed descriptions of the components of the

helicopter that affect the handling qualities of the aircraft. GEN HEL is used for solving aircraft trims for a variety of flight conditions such as level flight, autorotation, and climb, and for solving the dynamic response of the helicopter to control inputs or aircraft disturbances.

The GEN HEL program is arranged in modular form, grouping descriptions of the basic helicopter elements such as the main rotor, tail rotor, and fuselage separately to allow uncomplicated modification of particular components, if necessary. One of these particular files, called the specific file, describes all components of the helicopter that are unique to a particular model. When the specific file describing the UH-60A descriptive input and control system is assembled with the rest of the general files of GEN HEL, the resulting program then models the UH-60A helicopter. This is the basic UH-60A simulation model around which this tail rotor blade severance handling qualities study was developed.

#### SEVERANCE TRANSITION ROUTINE

To simulate the buildup of centrifugal forces in the tail rotor during the three-bladed transition period and the transfer of this load imbalance to the rest of the helicopter, a special routine was incorporated into GEN HEL that calculated the inertial loads in the three remaining blades as the tail rotor proceeded to rotate in the discrete digital program solution. The inertial loads were summed for all three blades, and the resulting forces and moments imparted on the helicopter were solved. Additionally, the calculation of the aerodynamic thrust produced at the tail rotor existing in the basic version of GEN HEL was modified to reflect the proper decrease in thrust that occurred as the number of blades was reduced.

An associated logic routine was written into GEN HEL to distinguish when the program user elected to lose the first tail rotor blade due to ballistic damage during the dynamic simulation of the helicopter. This logic then routed the program through the additional imbalance equations and kept track of the location of the remaining unbalanced blade in order to determine when it entered the jettison envelope of tail rotor azimuth. Once the imbalanced blade reached this envelope, the program logic then left the tail rotor imbalance equations and proceeded with simulation of the helicopter using only the basic GEN HEL program again, but in the two tail rotor blade mode. Figure 27 is a flow diagram that depicts the logic procedure employed.

Because the tail rotor rotates at such a high speed, the duty cycle (simulated time between program updates) had to be made small enough to sample the tail rotor imbalance whenever the severance transition period was being studied. For simulation of the severance transition, a duty cycle was selected as a function of rotor speed to yield a change in tail rotor blade azimuth of 20 deg each duty cycle. This duty cycle was approximately seven times greater than the 1/50 second (50 cycles per second) normally used for dynamic simulation.

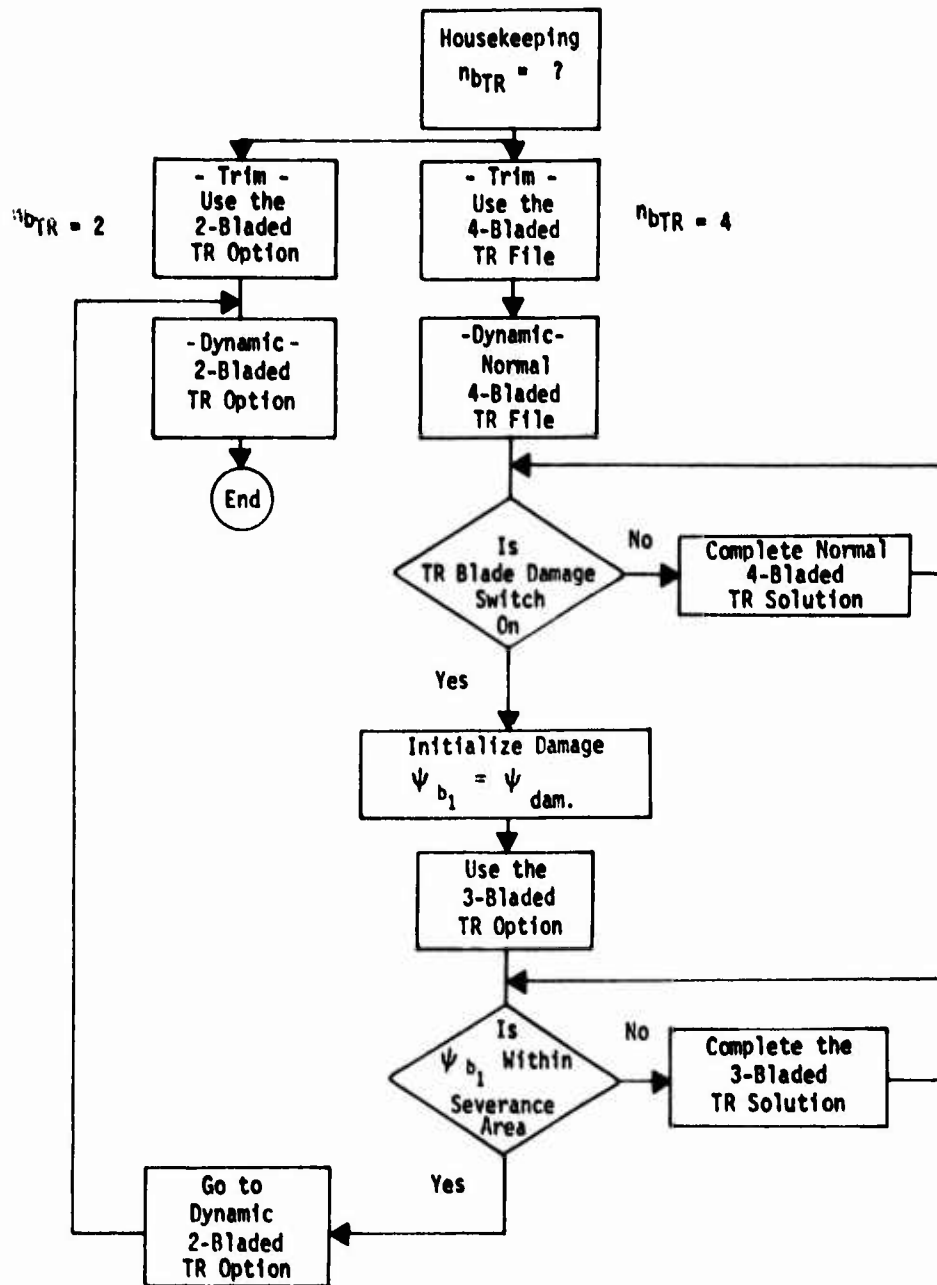


Figure 27. Flow Diagram of the Logic Modification used with GEN HEL (UH-60A) Tail Rotor File to Simulate Blade Severance Sequence

## CASES STUDIED

Aircraft level flight trims and severance period transitions were studied with variations in aircraft gross weight, fuselage station cg location, density altitude, and rotor speed. These conditions were studied over a speed range from hover to 150 knots. Level flight was considered the most relevant flight condition since in all likelihood after losing tail rotor blades, the primary concern would be to return to base, not to continue the mission. Therefore, unusual or stringent flight conditions were not considered following the loss of two tail rotor blades.

Autorotation is not a demanding flight condition if two tail rotor blades are lost. Autorotation demands from directional control are not critical even when two tail rotor blades are lost because the directional control requirements are not near control system limits.

## TWO-AND FOUR-BLADE TRIMS

Four trim cases were studied in accordance with the parametric mix shown below with trim data acquired at 0, 40, 60, 80, 100, 120, 140, and 150 knot speeds.

Case	$h$ Density	G W, LB	FSCG	Rotor $N_R$ Speed
1	SLS	Low (16450)	Aft (360.2)	100%
2	SLS	High (19900)	Aft (360.2)	100%
3	10,000	High (19900)	Aft (360.2)	100%
4	10,000	High (19900)	Fwd (347)	100%

Baseline trims were gathered using GEN HEL for the UH-60A with four tail rotor blades. Trims were then attempted for the same conditions, only with two tail rotor blades.

The result of this exercise showed that the helicopter could be trimmed with two tail rotor blades throughout the speed range for low altitudes even at high gross weight. At higher altitudes, power requirements increase and there are conditions near hover and high speed that cannot be trimmed.

For all of the cases studied at nominal (100%) rotor speed, there always was some speed range at which the helicopter could be trimmed with only two tail rotor blades. This speed range, 60 to 100 knots, corresponds to the lower power requirements of the helicopter (see Figure 28). At rotor speeds of 95%  $N_R$  and 110%  $N_R$  (see Figure 29), the helicopter could be

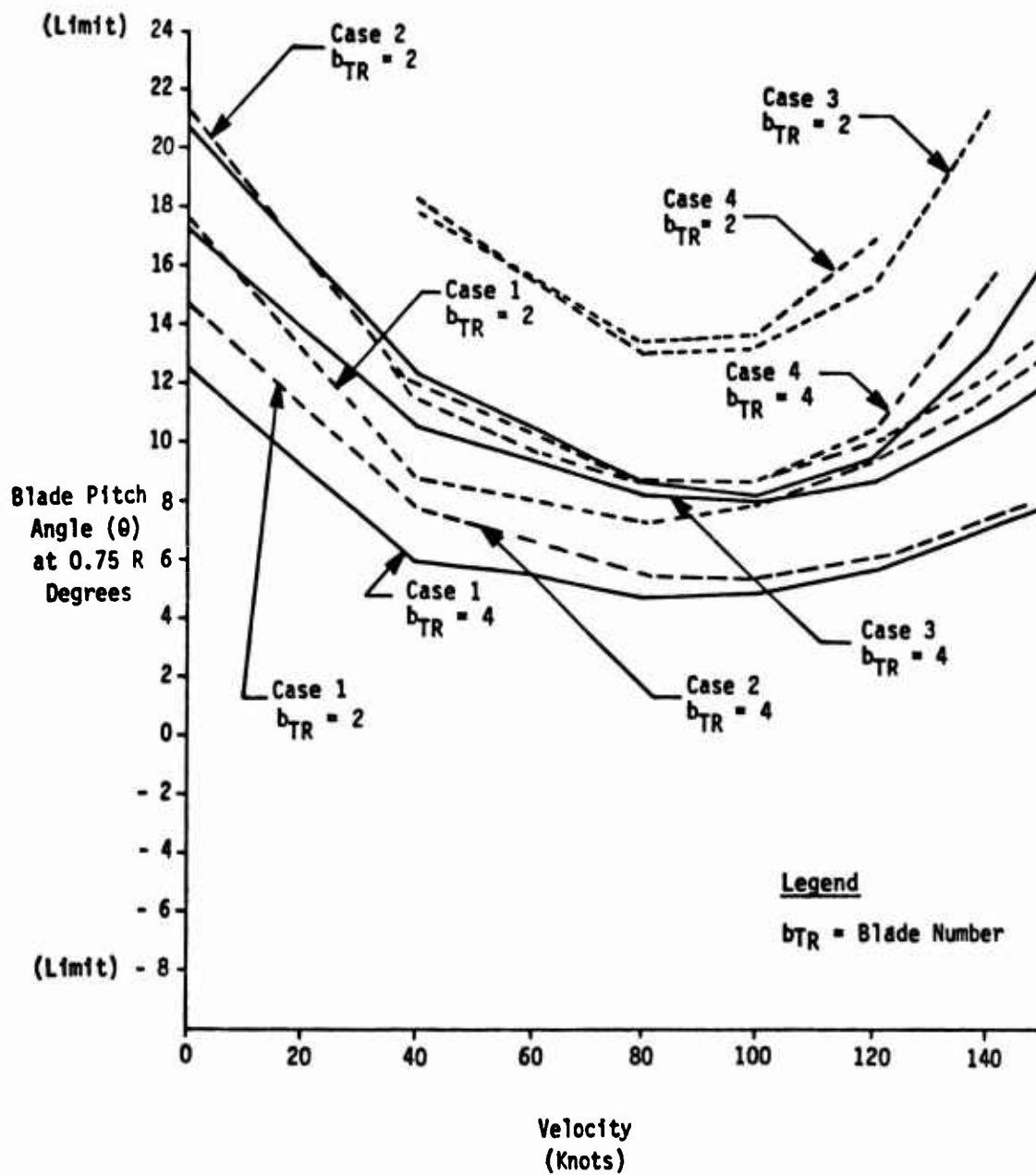


Figure 28. Two-and Four-Bladed Trims (100%  $N_p$ )

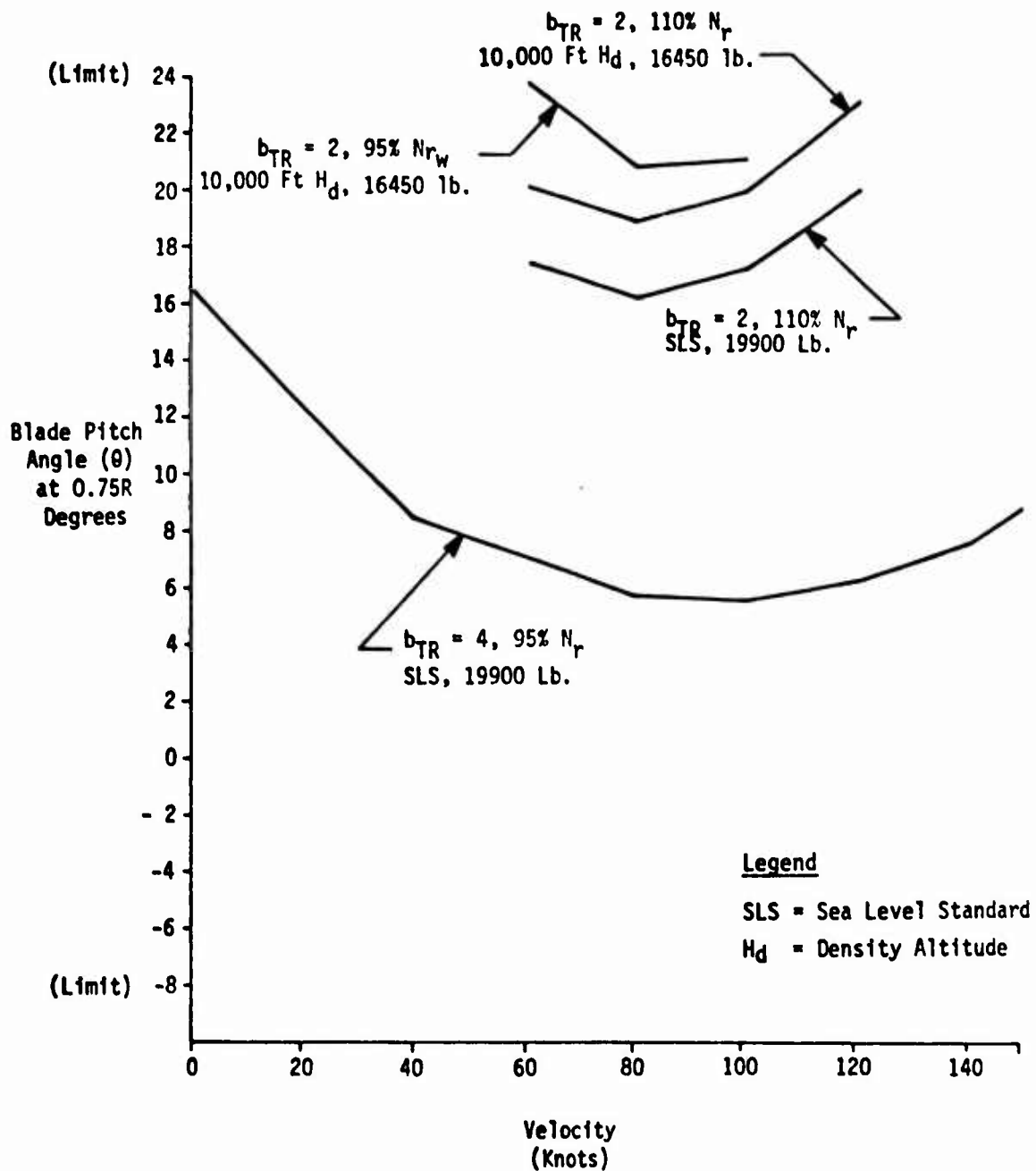


Figure 29 Two- and Four-Bladed Trims (95%  $N_R$  and 110%  $N_R$ )

trimmed at this same speed range with only two tail rotor blades. However, two blade trims become difficult (if not impossible) at any speed for low rpm at high altitudes, necessitating altitude reduction to achieve trim. Low rpm trims with two tail rotor blades are not advised because it becomes difficult to generate the required tail rotor thrust at reduced rotor speed.

These two tail rotor blade trim results indicate that for many flight conditions, the helicopter can be trimmed with only two tail rotor blades at any possible speed. At most flight conditions there exists a speed range (corresponding to the minimum power requirement) where the helicopter can be trimmed with only two tail rotor blades.

Naturally, trims with only two tail rotor blades provide less control margin and control sensitivity than the four-bladed situation, but under emergency conditions this situation could be considered acceptable.

For record, trim data printouts for the two-bladed and four-bladed conditions are provided in Appendix B.

#### AIRCRAFT "HANDS OFF" RESPONSE FOLLOWING BLADE LOSSES

The responses of the aircraft with no pilot correction for both the SAS OFF and SAS ON conditions are relatively mild, and should be acceptable to the pilot. These time history responses of the hands-off conditions, shown in Figures C-1 to C-12 (see Appendix C), demonstrate the response of the aircraft up to six seconds following blade loss. Actually, the pilot would react to the TR blade loss condition much earlier than six seconds and the response can be expected to be even less.

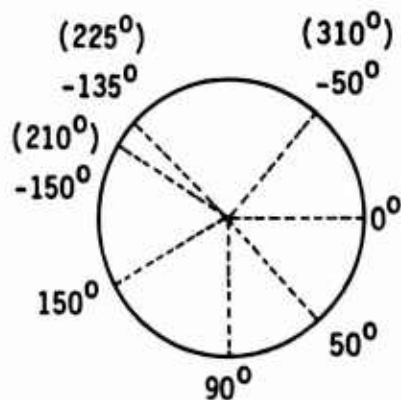
The aircraft responses vary as a function of the azimuth position where the initial blade is lost ( $\psi$  damage). This is caused by the unbalanced blade (No. 2) traveling through different percentages of tail rotor azimuth before reaching the jettison envelope for different azimuth locations of the ballistic damage to the initial blade (No. 0). The centrifugal imbalance imparts different net impulses on the helicopter for the different proportions of the revolution for which the imbalanced blade is carried before reaching the jettison envelope. Therefore, different aircraft responses follow the event as a function of damage but all of the responses are mild and acceptable for the full sweep of values of  $\psi$  damage. Table 4 presents data extracted from Figures C-1 through C-12 for: (a) the maximum roll ( $\phi_b$ ), pitch ( $\phi_b$ ), and yaw ( $\psi_b$ ) angles achieved within 6 seconds after initiation of blade loss with SAS OFF; and (b) the roll, pitch, and yaw attitudes of the aircraft at 6 seconds following blade loss with SAS ON.

Table 4. Aircraft "Hands Off" Response Following Blade Losses

(a) A/C response within 6 seconds after severance (SAS OFF)

$\psi$ Damage	<u>Maximum Value Incurred Any Time During the Time History</u>		
	$\phi_b$ Max	$\phi_b$ Max	$\psi_b$ Max
0	10	40	28
50	14	38	28
90	22	33	28
150	31	28	28
-135	30	28	29
- 50	13	39	28

SAS OFF - A/C response is low frequency, oscillatory deviation from trim.



(b) A/C response at 6 seconds after severance (SAS ON)

$\psi$ Damage	<u>Value at 6 Sec Point in the Time History</u>		
	$\phi_b$ 6 Sec	$\phi_b$ 6 Sec	$\psi_b$ 6 Sec
0	26	13	32
50	27	13	33
90	28	12	34
150	28	11	34
-135	28	11	34
- 50	27	14	33

SAS ON - A/C response is slow steady deviation from trim.

Trim condition = 16,450 Lb  
(Level Flt)  
FSCG = 360.2  
S.L.S.



### STEPPED TRANSITION TIME HISTORIES

During the three-bladed transitional period, the unbalanced centrifugal force imparts loads on the tail rotor of the helicopter. A series of ten time history cases with parameters varied in accordance with the table below were performed to examine the helicopter response to the unbalanced load during the transition from four to two blades. The simulation runs, Figures D-1 through D-10, are included in Appendix D to this report.

Table 5. Time History Case Parameters

Figure	GW(Lb)	FSCG(In)	V,Knots	$\Omega$ ,%	$\psi$ deg	SAS	H <sub>d</sub> Alt.,Ft
D-1	16,450	360.2	100 Kts	100	- 150	Off	S.L.S.
D-2	19,900	360.2	100 Kts	100	- 150	Off	S.L.S.
D-3	19,900	360.2	100 Kts	100	- 150	Off	10,000
D-4	19,900	347	100 Kts	100	- 150	Off	10,000
D-5	19,900	347	150 Kts	100	- 150	Off	10,000
D-6	19,900	360.2	150 Kts	100	- 150	(On)	10,000
D-7	19,900	360.2	Hover	100	- 150	Off	10,000
*D-8	19,900	347	Hover	100	- 150	Off	10,000
D-9	19,900	347	Hover	95	- 150	Off	10,000
D-10	19,900	347	Hover	100	- 150	Off	10,000

\*No print out

The ten aircraft configurations studied show that there are insignificant changes in the tail rotor load and aircraft response parameters with variations in gross weight, center-of-gravity location, airspeed, density altitude, or on/off condition of SAS. Two additional runs were conducted (Figures D-11 and D-12, Appendix D) to ascertain the significance of varying the rotational point at which blade loss occurs. These two cases illustrate that the loads developed at the tail rotor during the centrifugal imbalance period essentially are not dependent on the tail rotor blade azimuth location at which the first blade is lost. The centrifugal load in the unbalanced rotor blade does vary, as can be expected, with change in tail rotor speed. From the data, it can be determined that the centrifugal loads for 95% N<sub>R</sub>, 100% N<sub>R</sub>, and 110% N<sub>R</sub> are 24,000, 27,500, and 34,000 pounds, respectively.

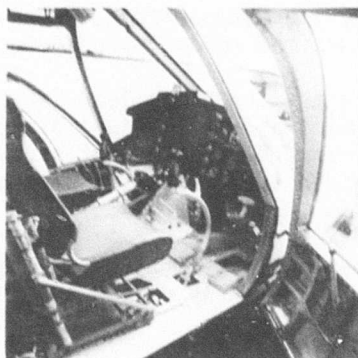
It is anticipated that the loss of tail rotor blades is felt only as an impact load by the pilot since the transitional three-blade condition is of such short duration.

### SIMULATOR INTERFACE

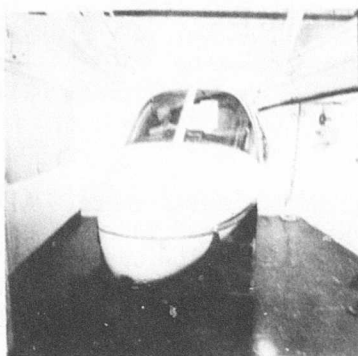
In order to qualitatively study pilot recovery from the tail rotor blade loss condition and retrimming of the helicopter, the basic GEN HEL program was coupled to a fixed base cockpit simulator (see Figure 30). Once the program is in a dynamic mode the program operator can select jettison of the two tail rotor blades. The program shifts from the four-bladed tail rotor solution to the two-bladed solution, imparting an impact-type response to the helicopter. Interpreting the blade loss condition from instrument readings and the visual display, the simulator pilot then proceeds to effect recovery of the helicopter from its response brought about by the forces from the blade loss and then trims the ship to the same or other flight conditions if necessary. The simulator pilot can proceed to a hover, if possible, and land, or conduct a run-on landing at low forward speed, if necessary.

The three-bladed severance transition portion of the solution is not used in the simulator study because real-time simulation requirements sample the tail rotor solution too infrequently to see a small enough change in tail rotor blade azimuth position. What transpires at the tail rotor during this very short imbalance period has negligible impact on helicopter handling qualities in a simulator study.

Nothing unusual or unexpected occurred during the piloted simulator portion of the handling qualities study. Even without external cues such as noise or impact motion, the simulator pilot was able to detect early the blade loss condition at the tail rotor. Yaw rates were not excessive for any of the severance cases studied using the simulator; qualitatively, these rates appeared to be between 10 deg/sec and 20 deg/sec. Typical reaction was to put in the left pedal to slow or stop the yaw rate. If the loading condition and forward speed of the original trim did not permit the helicopter to be retrimmed, the simulator pilot would reduce speed until the slip rate could be reduced. This speed range corresponded to the low power requirement range: between 60 and 100 knots. Many configurations were flown back to a trimmed hover with the two remaining tail rotor blades, from which a landing could be negotiated. The higher power configurations (high weight, high altitude) could only be flown down to 30 or 40 knots before running out of tail rotor range. These cases represented loading configurations of the aircraft that would have to be landed at forward speed.



Interior View



Frontal View

Figure 30. Cockpit Simulator

## RESULTS

### DYNAMIC STABILITY ANALYSIS

Based on a Floquet stability analysis, a two-bladed, cross-beam tail rotor system is stable up to the maximum speed investigated (150 knots).

The least stable blade/pylon modes are the blade lead-lag mode and the third fixed system mode, both showing a damping level of approximately one-half percent. The effect of forward speed is not significant except near 150 knots where two of the fixed system modes indicate a degradation in damping level.

The blade lead-lag damping is lowered slightly by the flexibility of the hub while the flapping mode shows very little change in stability.

Modal frequency is not influenced significantly by forward speed. The blade flapping mode and one of the fixed system modes have frequencies close to each other, particularly at 150 knots, resulting in modal damping degradation. However, modal frequencies do not coalesce and vibration problems from modes interacting are not likely to occur.

Vibration and load level on the two-bladed rotor increase with forward speed, and at the highest speed investigated (150 knots) the maximum 2/rev vibration levels result in a roll moment at the gearbox-pylon attachment of 20 percent of the ultimate value. This level is acceptable to maintain flight for the 30-minute minimum following ballistic damage that has been established for the UH-60A helicopter, and to conduct a landing.

Rotor hub loads generally increase with forward speed. All shear and moment loads except the steady yaw moment load increase rapidly at forward speeds greater than 120 knots as the rotor operates increasingly in the blade stall environment. The highest roll moment loading of the gearbox-pylon attachment occurs at the 150 knot maximum forward speed investigated.

Significant increases in hub and gearbox accelerations are observed for forward speeds greater than 120 knots and the 2/rev accelerations are much higher than the 4/rev accelerations.

### STRUCTURAL ACCOMMODATION

The centrifugal load resulting from loss of a full tail rotor blade applied for 0.05 second (360° rotation at 100% Ng) will result in a torsion flexure of the tailcone of approximately 0.05 inch per inch, a level not considered excessive for a single load application.

### PITCH LINK ACCOMMODATION

Severing of the tail rotor blade spar of the UH-60A must be accompanied by severing of the pitch horn fitting as well to achieve clean blade separation under all blade damage conditions.

### PROTOTYPE SYSTEM PERFORMANCE

The prototype system successfully met the performance requirements in all tests performed, and compatibility with the blade jettison window for the UH-60A helicopter has been verified.

### FLIGHT SIMULATION ANALYSIS

Helicopter trims gathered using the GEN HEL for the UH-60A with only two tail rotor blades indicated that the helicopter can be trimmed throughout the speed range for low altitudes even at high gross weights.

At higher altitudes, power requirements increase and there are conditions near hover and high speed that cannot be trimmed. At 100%  $N_r$  there is always a speed range (between 60 and 100 knots) where helicopter trim can be effected with the two-bladed tail rotor.

In general, the aft cg location is more critical for trimming the helicopter with two tail rotor blades due to the shorter moment arm provided about the cg.

The trim cases studied at 95%  $N_r$  and 110%  $N_r$  indicate that the helicopter can be trimmed in the 60-to-100-knot speed range except for low rotor speed with high altitude conditions where altitude reduction may be necessary to achieve trim due to inadequate rotor thrust at the reduced rotor speed and density altitude.

The time history studies conducted indicate that responses of the aircraft for both the SAS OFF and the SAS ON conditions are relatively mild, and should be acceptable to the pilot.

Although the aircraft responses vary with respect to the azimuthal position at which the blade is lost (onset of the centrifugal load), all of the responses are mild and acceptable for the sweep of the values of damage examined.

### FLIGHT SIMULATOR WITH PILOT-IN-THE-LOOP

Yaw rates were not excessive for any of the severance cases studied using the flight simulator, ranging between 10 and 20 degrees per second.

Following left pedal input to slow or stop the yaw rate where loading and forward speed conditions did not permit retrimming with the two-bladed tail rotor, yaw rate could be stopped and out-of-trim slip angles could be reduced by reducing speed to the low power requirement range of 60 to 100 knots.

The higher power configurations (high weight, high altitude) indicated a 30-to-40-knot minimum speed limitation, requiring run-on type landings.

## CONCLUSIONS

The prototype blade jettison system developed under this program has been verified by test to meet the rotational speed requirements of the UH-60A tail rotor and, when used in conjunction with blade severance assemblies, it will initiate tail rotor blade jettison within the blade jettison window established for that helicopter.

The dynamic stability analysis performed indicates that frequencies and amplitudes of the vibrations resulting from jettison of two opposing tail rotor blades will allow continued flight for a minimum of 30 minutes.

The simulation analysis performed to assess handling qualities indicates that the helicopter is controllable following the jettison of two opposing tail rotor blades and that the pilot work load to effect recovery is anticipated to be minimal.

An examination of the capability of the UH-60A helicopter to structurally accommodate the centrifugal force generated by the loss of an entire tail rotor blade for a period of 360° of rotor rotation indicates that re-design of the tail rotor drive shaft and the gearbox housing may be required.

For the UH-60A helicopter, the location of the pitch horn with respect to the point at which the blade spar is severed, necessitates that the pitch horn be severed simultaneously with the spar to prevent delayed blade jettison.

### RECOMMENDATIONS

Based on the conclusions drawn from the results of the work performed under this contract, it is recommended that a follow-on ground test program be conducted that will demonstrate controlled jettison of tail rotor blades using a fully instrumented UH-60A tail cone and pylon and the prototype blade jettison system. The intent of the program would be to:

- . Verify proper blade severance/jettison using full length tail rotor blades.
- . Measure loads at the critical points to determine actual load levels achieved and to verify structural adequacy.
- . Develop pyrotechnic devices, sized to sever UH-60A tail rotor blade spars and pitch horns.
- . Prepare a failure modes and effects analysis for the blade jettison system.
- . Instrument the tail rotor assembly and conduct lightning tests of the blades. Measure induced voltage levels, if present, at the logic units.

### REFERENCES

1. USA Ballistic Research Laboratories Contract Report #197, December, 1974, "Rotor Balance Restoration Study".
2. Arcidiacono, P. J., Prediction of Rotor Instability at High Forward Speeds, Volume I, Steady Flight Differential Equations of Motion for a Flexible Helicopter Blade with Chordwise Mass Unbalance, Sikorsky Aircraft, USAAVLABS Technical Report 68-18A, U. S. Army Aviation Materiel Laboratories, Fort Eustis, Virginia, February, 1969, AD-685860.
3. Sikorsky Aircraft Report, SER-70545, Revision 2, May 1978, "UTTAS Aeroelastic Stability Analysis".



## APPENDIX A

### PROTOTYPE PERFORMANCE DATA

This appendix contains the photographically recorded data obtained from the tests conducted on the prototype blade jettison system to determine the capability of the system to meet the performance requirements of the UH-60A helicopter. The data was secured by means of Polaroid photographic equipment attached to the oscilloscope. Each of the photographs includes the oscilloscope sweep rate used to obtain the data. Each of the data is in accordance with the following key:

Trace #1: Proximity Sensor A - open condition

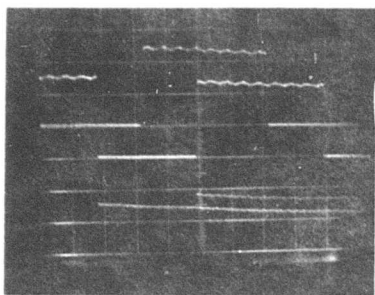
Trace #2: Proximity Sensor B - open condition

Trace #3: Proximity Sensor A - closed condition

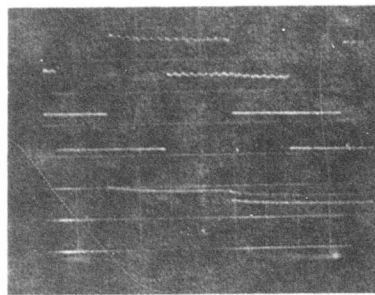
Trace #4: Proximity Sensor B - closed condition

Trace #5: EED Simulator - Blade #1 (left end is point of initiation)

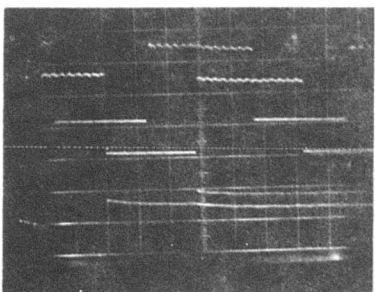
Trace #6: EED Simulator - Blade #3 (left end is point of initiation)



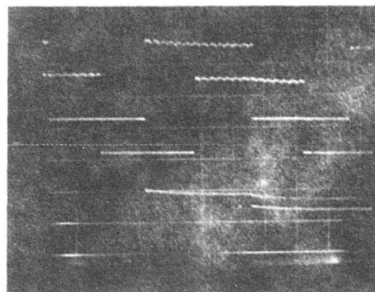
70%  $N_R$  (834 RPM) 10 ms Sweep



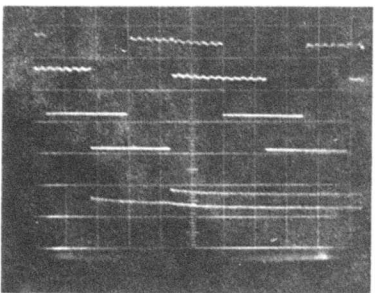
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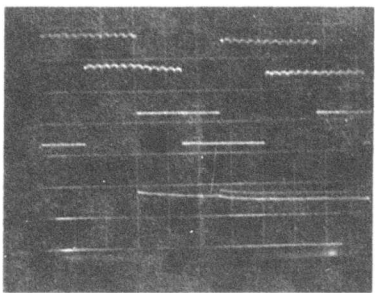
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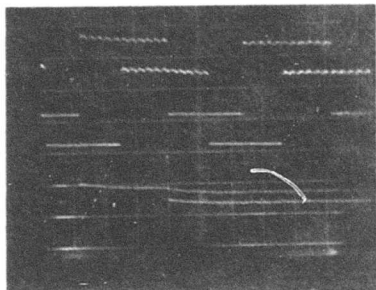
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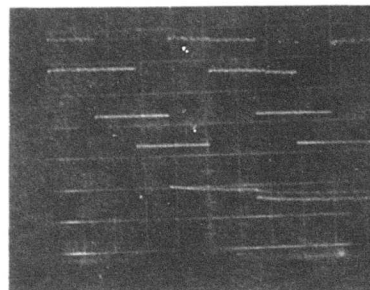
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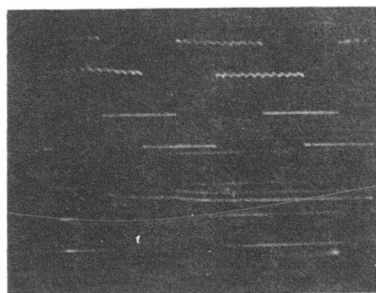
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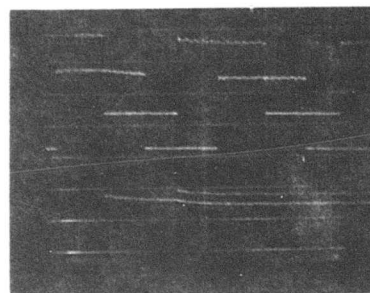
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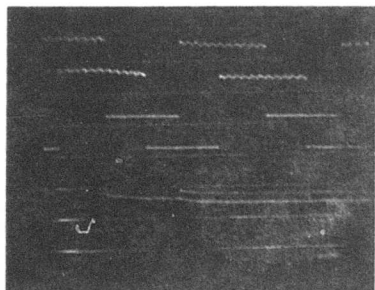
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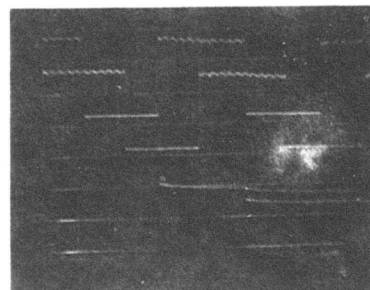
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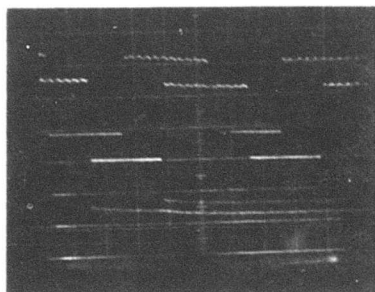
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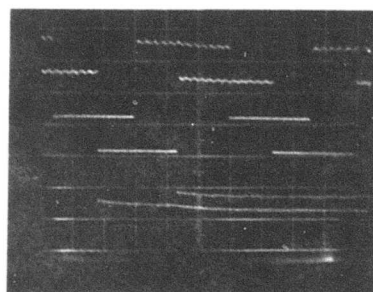
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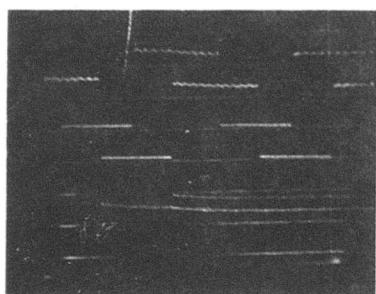
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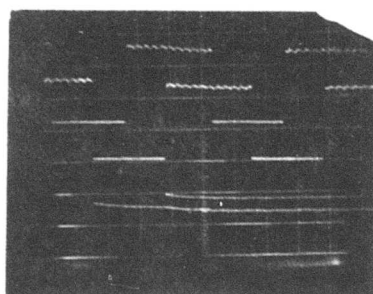
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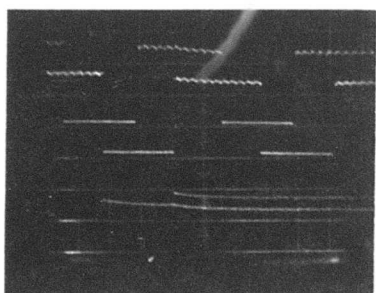
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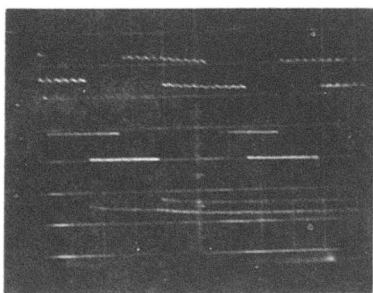
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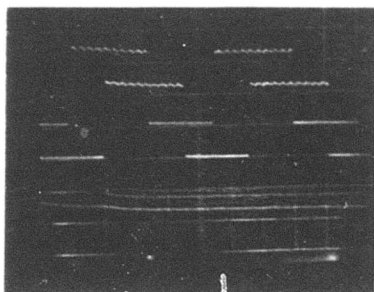
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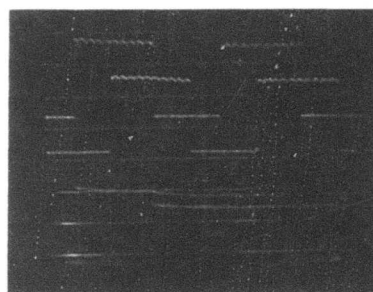
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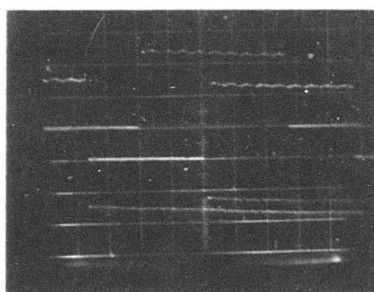
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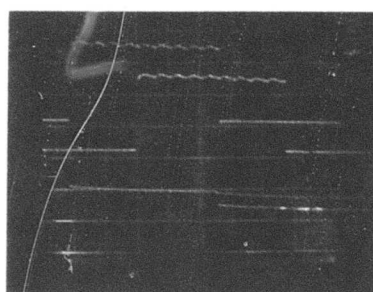
110%  $N_R$  (1311 RPM) 10 ms Sweep



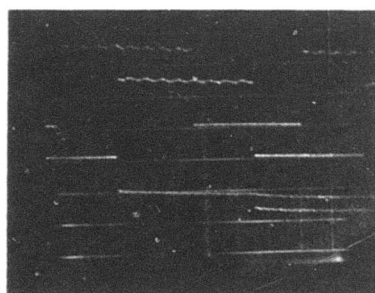
110%  $N_R$  (1311 RPM) 10 ms Sweep



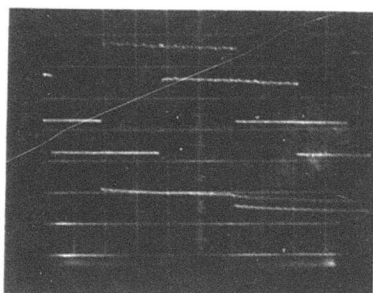
120%  $N_R$  (1430 RPM) 5 ms Sweep



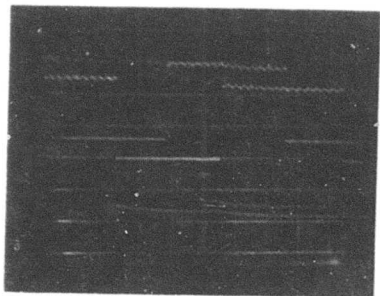
120%  $N_R$  (1430 RPM) 5 ms Sweep



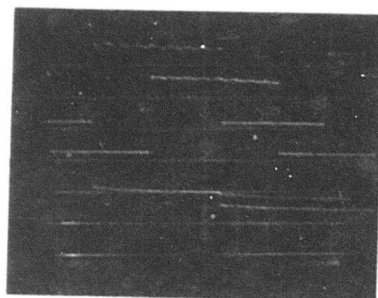
130%  $N_R$  (1550 RPM) 5 ms Sweep



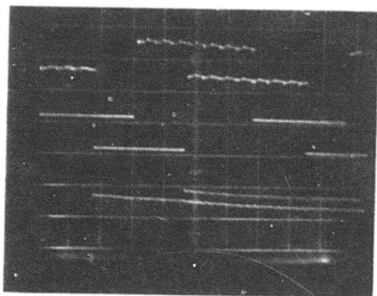
130%  $N_R$  (1550 RPM) 5 ms Sweep



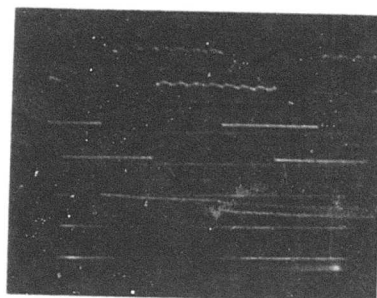
140%  $N_R$  (1669 RPM) 5 ms Sweep



140%  $N_R$  (1669 RPM) 5 ms Sweep



150%  $N_R$  (1788 RPM) 5 ms Sweep



150%  $N_R$  (1788 RPM) 5 ms Sweep

## APPENDIX B

### TWO-AND FOUR-BLADED TRIMS

The computer runs provided in this appendix are the two-and four-bladed trim data conducted to assess the ability of the UH-60A helicopter to achieve trim under varying density altitude, gross weight, and center-of-gravity conditions. Definitions of the symbols used are included.

## SYMBOLS

WEIGHT	AIRCRAFT GROSS WEIGHT			
IX	INERTIA ABOUT BODY X-AXIS LESS ROTOR, FT-LB-SEC <sup>2</sup>			
IY	INERTIA ABOUT BODY Y-AXIS LESS ROTOR, FT-LB-SEC <sup>2</sup>			
IZ	INERTIA ABOUT BODY Z-AXIS LESS ROTOR, FT-LB-SEC <sup>2</sup>			
OMEGMR	MAIN ROTOR ROTATIONAL SPEED, RAD/SEC			
OMEGTR	TAIL ROTOR ROTATIONAL SPEED, RAD/SEC			
KFR	ROTOR FILTER CONSTANT			
FSHT	FUSELAGE STATION HORIZONTAL TAIL, IN.			
LATSTK	LATERAL STICK POSITION, INTERMEDIATE CALCULATION, DEG			
LNGSTK	LONGITUDINAL STICK POSITION, INTERMEDIATE CALCULATION, DEG			
COLSTK	COLLECTIVE STICK POSITION, INTERMEDIATE CALCULATION, DEG			
PEDAL	DIRECTIONAL CONTROL PEDAL POSITION, INTERMEDIATE CALCULATION, DEG			
XAIN	LATERAL STICK POSITION, IN.			
XBACTP	LONGITUDINAL STICK POSITION WITH BIAS ACTUATOR, %			
VXB	} BODY AXIS TRANSLATIONAL VELOCITIES	} X-AXIS	} FT/SEC	
VYB				} Y-AXIS
VZB				
P	ROLL RATE, RAD/SEC			
Q	PITCH RATE, RAD/SEC			
R	YAW RATE, RAD/SEC			
ALFWF	FUSELAGE ANGLE OF ATTACK, DEG			
CHITPP	ROTOR DOWN WASH ANGLE, DEG			



EKTR	DOWNWASH FACTOR OF TAIL ROTOR ON VERTICAL TAIL	
QWF	DYNAMIC PRESSURE AT FUSELAGE, LB/FT <sup>2</sup>	
MUXS	NORMALIZED SHAFT AXIS TRANSLATIONAL VELOCITIES AT THE HUB, NORMALIZED BY $\Lambda$ MR TIP SPEED	
MUYS		
MUZS		
LAMBMR	MAIN ROTOR INFLOW RATIO	
DWSHMR	MAIN ROTOR INDUCED DOWN WASH	
XMR	ROTOR BODY AXIS FORCES, LB	
YMR		
ZMR		
LMR	ROTOR BODY AXIS MOMENTS ABOUT THE C.G.	ROLL MOMENT, FT-LB
MMR		PITCHING, MOMENT FT-LB
NMR		YAWING MOMENT, FT-LB
XWF	FUSELAGE BODY AXIS FORCES, LB	
YWF		
ZWF		
LWF	FUSELAGE BODY AXIS MOMENTS ABOUT THE C.G.	ROLL, FT-LB
MWF		PITCH, FT-LB
NWF		YAW, FT-LB
XHT	HORIZONTAL TAIL BODY AXIS FORCES, LB	
YHT		
ZHT		
FSCG	FUSELAGE STATION C.G., IN.	
WLCG	WATER LINE STATION C.G., IN.	
RHO	AIR DENSITY, SLUGS/FT <sup>3</sup>	
TIME	TIME INTERVAL BETWEEN ROTOR CALCULATIONS, SEC	

NBSS	NUMBER OF BLADES
NSSS	NUMBER OF BLADE SEGMENTS
PASCNT	NUMBER OF ROTOR CALCULATIONS FOR TRIM
SHT	HORIZONTAL TAIL AREA, FT <sup>2</sup>
AIS	LATERAL CYCLIC PITCH, DEG
BIS	LONGITUDINAL CYCLIC PITCH, DEG
THETAØ	MAIN ROTOR COLLECTIVE PITCH AT CUFF, DEG
THETTR	RAIL ROTOR IMPRESSED COLLECTIVE PITCH @ CENTER OF ROTATION, DEG
XBIN	LONGITUDINAL STICK POSITION, WITHOUT BIAS ACTUATOR, IN.
XBACTI	LONGITUDINAL STICK POSITION, WITH BIAS ACTUATOR, IN.
THETAB	AIRCRAFT PITCH ATTITUDE, DEG
PHIB	AIRCRAFT ROLL ATTITUDE, DEG
BETAWF	AIRCRAFT SIDESLIP ANGLE, DEG
GAMC	CLIMB ANGLE, DEG
OMGRAT	RATIO OF ACTUAL TO TRIMMED ROTOR SPEED
PSIDOT	EULER ANGLE YAW RATE, DEG/SEC
EKTX	MAIN ROTOR DOWNWASH FACTOR AT HORIZONTAL TAIL IN BODY X-AXIS
EKTZ	MAIN ROTOR DOWNWASH FACTOR AT HORIZONTAL TAIL IN BODY Z-AXIS
EPSWT	FUSELAGE DOWNWASH ANGLE AT HORIZONTAL TAIL, DEG
KQHT	SQUARE ROOT OF DYNAMIC PRESSURE RATIO AT HORIZONTAL TAIL
CTSIG	MAIN ROTOR THRUST COEFFICIENT SOLIDITY RATIO
CHSIG	MAIN ROTOR H-FORCE COEFFICIENT SOLIDITY RATIO
CQHSIG	MAIN ROTOR TORQUE COEFFICIENT SOLIDITY RATIO
NZ	LOAD FACTOR ALONG THE AIRCRAFT Z-AXIS

VC	RATE OF CLIMB, FT/MIN	
HBAR	MAIN ROTOR H-FORCE, LB	} SHAFT AXIS
JBAR	MAIN ROTOR SIDEFORCE, LB	
TBAR	MAIN ROTOR THRUST, LB	
LBARH	MAIN ROTOR ROLL MOMENT, FT-LB	
MBARH	MAIN ROTOR PITCH MOMENT, FT-LB	
QBAR	MAIN ROTOR TORQUE MOMENT, FT-LB	
XT	EMPENNAGE X-FORCE (VERTICAL + HORIZONTAL TAIL) IN BODY AXIS, LB	
YT	EMPENNAGE Y-FORCE (VERTICAL + HORIZONTAL TAIL) IN BODY AXIS, LB	
ZT	EMPENNAGE Z-FORCE (VERTICAL + HORIZONTAL TAIL) IN BODY AXIS, LB	
LT	EMPENNAGE ROLL MOMENT (VERTICAL + HORIZONTAL TAIL) IN BODY AXIS, FT-LB	
MT	EMPENNAGE PITCH MOMENT (VERTICAL + HORIZONTAL TAIL) IN BODY AXIS, FT-LB	
NT	EMPENNAGE YAW MOMENT (VERTICAL + HORIZONTAL TAIL) IN BODY AXIS, FT-LB	
XVT	VERTICAL TAIL X-FORCE IN BODY AXIS, LB	
YVT	VERTICAL TAIL Y-FORCE IN BODY AXIS, LB	
ZVT	VERTICAL TAIL Z-FORCE IN BODY AXIS, LB	
V	AIRSPEED, KTS	/
DELS	SWASH PLATE ROTATION, DEG	
VSOUND	SPEED OF SOUND, FT/SEC	
DEL3MR	MAIN ROTOR DELTA 3 ANGLE, DEG	
TWSTM	MAIN ROTOR TWIST, DEG	
TWSTTR	TAIL ROTOR TWIST, DEG	
WLHT	WATER LINE HORIZONTAL TAIL, IN.	

SVT	VERTICAL TAIL AREA, $\text{FT}^2$
IHT	HORIZONTAL TAIL INCIDENCE, DEG
IS	SHAFT ANGLE INCIDENCE, POSITIVE FWD, DEG
TH75MR	MAIN ROTOR COLLECTIVE PITCH AT .75 RADIUS, DEG
TH75TR	TAIL ROTOR COLLECTIVE PITCH AT .75 RADIUS, DEG
XCIN	COLLECTIVE STICK POSITION, IN.
RSTR	YAW ACCELERATION AT TAIL ROTOR, SHAFT AXIS, $\text{RAD/SEC}^2$
AA0F	FOURIER SERIES COEFFICIENT FOR MAIN ROTOR FLAPPING, NEGATIVE SERIES, DEG
AA1F	
BB1F	
AA0L	FOURIER SERIES COEFFICIENT FOR MAIN ROTOR LAGGING, NEGATIVE SERIES, DEG
AA1L	
BB1L	
EKWFX	MAIN ROTOR DOWNWASH FACTOR AT FUSELAGE, BODY X-AXIS
EKWFZ	MAIN ROTOR DOWNWASH FACTOR AT FUSELAGE, BODY Z-AXIS
SIGWT	FUSELAGE SIDEWASH ANGLE AT VERTICAL TAIL, DEG
KQVT	SQUARE ROOT OF DYNAMIC PRESSURE RATIO AT VERTICAL TAIL, DEG
TTR	TAIL ROTOR THRUST, LB
HPMR	HORSE POWER MAIN ROTOR
KTRBLK	TAIL ROTOR BLOCKAGE FACTOR
VXBDOT	BODY AXIS ACCELERATION AT C.G. IN X-AXIS, $\text{FT/SEC}^2$
VYBDOT	BODY AXIS ACCELERATION AT C.G. IN Y-AXIS, $\text{FT/SEC}^2$
VZBDOT	BODY AXIS ACCELERATION AT C.G. IN Z-AXIS, $\text{FT/SEC}^2$
PDOT	AIRCRAFT ROLL ACCELERATION, $\text{RAD/SEC}^2$
QDOT	AIRCRAFT PITCH ACCELERATION, $\text{RAD/SEC}^2$
RDOT	AIRCRAFT YAW ACCELERATION, $\text{RAD/SEC}^2$

XTR	TAIL ROTOR FORCE IN X-AXIS, LB
YTR	TAIL ROTOR FORCE IN Y-AXIS, LB
ZTR	TAIL ROTOR FORCE IN Z-AXIS, LB
LTR	TAIL ROTOR ROLL MOMENT ABOUT BODY X-AXIS, FT-LB
MTR	TAIL ROTOR PITCH MOMENT ABOUT BODY Y-AXIS, FT-LB
NTR	TAIL ROTOR YAW MOMENT ABOUT BODY Z-AXIS, FT-LB
ALFHTT	LOCAL ANGLE OF ATTACK OF HORIZONTAL TAIL
ALFVTT	LOCAL ANGLE OF ATTACK OF VERTICAL TAIL
AABB1F	$\sqrt{(AA1F)^2 + (BB1F)^2}$
PSITR2	AZIMUTH POSITION OF TR BLADE NUMBER 2, DEG
VXSTR.	LINEAR ACCELERATION AT TAIL ROTOR IN TAIL ROTOR SHAFT X-AXIS, FT/SEC <sup>2</sup>
VYSTR.	LINEAR ACCELERATION AT TAIL ROTOR IN TAIL ROTOR SHAFT Y-AXIS, FT/SEC <sup>2</sup>
VZSTR.	LINEAR ACCELERATION AT TAIL ROTOR IN TAIL ROTOR SHAFT Z-AXIS, FT/SEC <sup>2</sup>
PSTR.	AIRCRAFT ROLL ANGLULAR ACCELERATIONS AT TAIL ROTOR IN SHAFT AXIS
WLV	WATERLINE VERTICAL TAIL
FSVT	FUSELAGE STATION VERTICAL TAIL
XA	LATERAL STICK POSITION, %
XB	LONGITUDINAL STICK POSITION, %
XC	COLLECTIVE STICK POSITION, %
XP	PEDAL POSITION, %
XPIN	PEDAL POSITION IN INCHES
PSTR	AIRCRAFT ROLL ANGULAR ACCELERATIONS AT TAIL ROTOR IN TR SHAFT AXIS, RAD/SEC <sup>2</sup>

QSTR	AIRCRAFT PITCH ANGLULAR ACCELERATIONS AT TAIL ROTOR IN TR SHAFT AXIS, RAD/SEC <sup>2</sup>
RSTR	AIRCRAFT YAW ANGLULAR ACCELERATIONS AT TAIL ROTOR IN TR SHAFT AXIS, RAD/SEC <sup>2</sup>
TITR	TAIL ROTOR INERTIA THRUST (SHAFT AXIS), LB
HITR	TAIL ROTOR INERTIA H-FORCE (SHAFT AXIS), LB
JITR	TAIL ROTOR INERTIA J-FORCE (SHAFT AXIS), LB
MHITR	TAIL ROTOR INERTIA HUB PITCHING MOMENT (MOMENT ABOUT SHAFT Y AXIS), FT-LB
LHITR	TAIL ROTOR INERTIA HUB ROLLING MOMENT (MOMENT ABOUT SHAFT X AXIS), FT-LB
QHITR	TAIL ROTOR INERTIA HUB YAW MOMENT (MOMENT ABOUT SHAFT Z AXIS), FT-LB
XITR	TR INERTIA X-FORCE (BODY AXIS), LB
YITR	TR INERTIA Y-FORCE (BODY AXIS), LB
ZITR	TR INERTIA Z-FORCE (BODY AXIS), LB
LITR	TR INERTIA ROLL MOMENT (BODY AXIS), FT-LB
MITR	TR INERTIA PITCH MOMENT (BODY AXIS), FT-LB
NITR	TR INERTIA YAW MOMENT (BODY AXIS), FT-LB
AXP	LONGITUDINAL ACCELERATION AT PILOT'S LOCATION, FT/SEC <sup>2</sup>
AYP	LATERAL ACCELERATION AT PILOT'S LOCATION, FT/SEC <sup>2</sup>
AZP	VERTICAL ACCELERATION AT PILOT'S LOCATION, FT/SEC <sup>2</sup>
VXP	LONG. VEL AT PILOT'S LOCATION (ALONG BODY X-AXIS), FT/SEC
VYP	LATERAL VELOCITIE AT PILOT'S LOCATION (ALONG BODY Y-AXIS), FT/SEC
VZP	VERTICAL VELOCITY AT PILOT'S LOCATION (ALONG BODY Z-AXIS), FT/SEC
RSTR.	YAW ACCELERATION AT TAIL ROTOR, SHAFT AXIS, RAD/SEC <sup>2</sup>
PSIDMG	AZIMUTH SELECTED FOR DAMAGE OCCURANCE, DEG

BTR	NUMBER OF TAIL ROTOR BLADES
MADD	AUXILIARY PITCHING MOMENT (BODY AXIS SYSTEM), FT-LB
XADD	AUXILIARY X-FORCE (BODY AXIS SYSTEM), LB
YADD	AUXILIARY Y-FORCE (BODY AXIS SYSTEM), LB
ZADD	AUXILIARY Z-FORCE (BODY AXIS SYSTEM), LB
NADD	AUXILIARY YAWING MOMENT (BODY AXIS SYSTEM), FT-LB
LADD	AUXILIARY ROLLING MOMENT (BODY AXIS SYSTEM), FT-LB

UTIAS(S76) 1-21-77 16-SEP-77 RUN 22.

WEIGHT	19900.0	FSCG	360.20000	V	40.0	PSIIR2	0.0
IX	6265.0	MLCG	246.29999	DELS	-5.0	VXSTR.	0.0
IY	41507.0	RMO	0.17500000E-2	VSUUNU	1077.0	VYSTR.	0.0
IZ	36224.0	TIME	0.20200000E-1	DELJMK	0.0	VZSTR.	0.0
OMEGMX	27.019479	NBS3	4.0	THS1MK	-16.0	PSTR.	0.0
OMEGTY	120.62000	NBS3	5.0	THS1TH	-16.0	FLVT	273.0
KPM	15.0	PASLNT	692.0	MLMT	234.0	FSVT	695.0
FSMT	705.40000	SMT	45.0	SVT	32.500000	OSTH.	0.0
LATSTK	-2.116300	AIS	-3.0734014	IMT	31.582001	XA	36.000562
LONGTK	5.707940E	BIS	4.4315940	IS	-3.0	XB	20.911037
COLSTK	19.027877	THETAU	19.027877	TH75MR	9.7478772	XC	50.424233
PEOAL	20.017620	THETM	31.035001	TH75TH	10.335001	XP	24.446502
XAIN	3.0004562	XBIN	2.0911037	XCIN	5.0424233	XPIN	1.320011
XBACTP	35.510725	XBALTI	3.5510725	RSTM.	0.0	PSTR	0.0
XAB	67.584674	THETAB	4.4910113	AAUP	4.3234276	QSTR	0.0
VTO	0.0	PMIB	-1.5037090	AAIF	-2.2735399	RSTR	0.0
VZB	5.2442291	BETANF	0.0	BBIF	-0.33071902	TITR	0.0
P	0.0	GAML	0.0	AAOL	-6.5007754	HITR	0.0
O	0.0	OMGRAT	1.0	AAIL	0.20154563	JITR	0.0
R	0.0	PSIDOT	0.0	BBIL	0.04644779E-1	MMITR	0.0
ALPWF	-10.010192	EKTZ	0.96973353	EMPX	0.69240102	LMITR	0.0
CHITPP	62.492440	EKTZ	2.0277043	EMFZ	1.0350151	QMITR	0.0
EKTH	0.0	EPSMT	0.44999999	SIGMT	0.0	XITH	0.0
OMF	7.7526100	KUMT	0.93516002	KOVI	0.04052013	YITM	0.0
MUXS	0.93205097E-1	CISIG	0.11161442	LTOI	-31.028381	ZITR	0.0
MUTS	0.0	CHSIG	-0.36497394E-2	DTOT	30.011919	LITM	0.0
MUZS	0.2427421E-2	QMSIG	0.94369209E-6	TTR	1161.9499	MITH	0.0
LAMBMR	-0.43430306E-1	NZ	0.99655093	MPHM	1707.5339	NITH	0.0
UMSHMR	0.40357740E-1	VC	0.13353024	KTRBLK	1.0	AXP	2.5297503
XMK	1019.7477	HBAR	-023.21614	VXUOT	0.10044655E-1	AYP	0.91320406
YMK	-504.54950	JBAR	544.39954	VYUOT	0.27040060E-1	AZP	-32.061428
ZMK	-14990.055	TBAR	19050.071	VZUOT	-0.26503080E-2	VXP	67.589674
LMM	-0051.1029	LBARM	-1505.3965	PUOI	0.15501459E-2	VYP	0.0
MMK	15024.022	MBARM	-6069.2910	QUOI	0.10375086E-3	VZP	5.2942291
NMK	53721.550	QBAR	34753.262	RDOI	0.12604034E-2	RSTR.	0.0
NKF	-150.03485	XT	32.240909	XTR	0.0	PSIDMO	0.0
YMF	0.0	YT	-5.5032411	YTR	1091.9569	BTR	2.0
ZMF	500.40204	ZT	65.449772	ZTR	-597.44061	MAUD	0.0
LMF	0.0	LT	-12.422711	LTR	6670.4302	XADD	0.0
MPF	-5145.0140	MT	1092.0683	MTR	-12314.034	YADD	0.0
NMF	0.0	NT	155.77242	NTR	-33032.466	ZADD	0.0
XMT	33.036003	XVT	-1.5959737	ALFMTT	-1.9017445	MAUD	0.0
YMT	0.0	YVT	-5.5032411	ALFVTT	0.0	LAUD	0.0
ZMT	60.524237	ZVT	0.92553544	AAHIF	2.2906331		



UTTA8(376)

1-21-77 30-AUG-77

RUN 51.

HEIGHT	19980.0	PSCG	347.0	DEL3	0.0	P31R2	0.0
IX	6260.0	WLCG	246.29999	VOUNO	-5.0	VXSTR.	0.0
IY	41367.0	RMO	0.17500000E-2	VOUNO	1077.0	VYSTR.	0.0
IZ	30224.0	TIME	0.20000000E-1	DEL3MR	0.0	VZSTR.	0.0
OMCHMR	27.01999	N883	4.0	DEL3MR	-10.0	WLV	273.0
OMECTR	124.62000	N883	5.0	WLSITH	-10.0	WLV	273.0
KPR	15.0	PASCT	2070.0	WLV	234.0	WLV	693.0
FSMT	700.40000	SMT	45.0	SVT	32.30000	QSTR.	0.0
LATSTK	1.7713119	A18	1.0214275	IMT	33.202421	XA	61.07000
LNGSTK	4.2610260	B18	-0.33549594	IS	-3.0	X0	34.941240
COLSTK	17.760431	THETAB	17.760431	TH75MR	7.6004314	XC	45.502097
PEDAL	29.430000	THETTR	37.5	TH75TR	24.0	XP	0.0
XAIN	0.1070099	XBIN	3.0941240	XCIN	4.5502097	XPIN	0.0
XOACTP	39.947009	XOACTI	3.9947009	RSTR.	0.0	PSTR	0.0
VXB	67.590005	THETAB	0.27022903	AAOF	3.0930599	QSTR	0.0
VYB	103.49543	PHIB	5.0406344	AAIF	4.5023030	RSTR	0.0
VZB	0.32030200	BETANF	50.249247	BWIF	-0.93397370	YSTR	0.0
P	0.0	GMC	0.0	AAOL	-3.2546704	MITR	0.0
Q	0.0	OMGRAT	1.0	AAIL	-0.95000230E-1	JSTR	0.0
R	0.0	P31DOT	0.0	BWIL	-0.45149101	MMTR	0.0
ALHFP	-12.730494	EKTX	1.00497143	EKMF	0.05092052	LMTR	0.0
CHIPP	76.26230	EKTX	2.1495279	EKMFZ	1.0137337	OMTR	0.0
EKTR	0.0	EP3MT	1.7599999	IGMT	2.0	XSTR	0.0
GMF	15.050035	KMT	0.07177079	KMT	1.0	YSTR	0.0
MUXS	0.93130024E-1	CT816	0.10000000	ETOT	10.432414	ZSTR	0.0
MUYS	0.14270204	CH816	0.00452336E-2	DTOT	64.004462	LSTR	0.0
MUZS	-0.44271310E-2	CH816	0.04992933E-6	TTR	0.62.61370	MITR	0.0
LAMBMR	-0.30692736E-1	NZ	0.99498302	MPM	943.09963	NSTR	0.0
DM8MR	0.26205004E-1	VC	-0.11.00005	KTRBLK	1.0	AXP	0.15000934
XMR	-170.09275	MBAR	1127.7642	VXDOT	0.12903007E-2	AYP	-3.1063450
YMR	-022.90074	JBAR	022.90074	VYDOT	-0.25305491E-1	AZP	-32.012104
ZMR	-10147.010	TBAR	10115.022	VZDOT	0.23370113E-2	VXP	67.594903
LMR	-9593.0003	LBARM	-3002.5020	PDOT	0.16200020E-2	VYP	103.49543
MMR	21402.733	MBARM	11195.409	QDOT	-0.47363997E-4	VZP	0.32050200
NMR	10561.000	QBARM	19197.069	RODT	-0.73306749E-3	RSTR.	0.0
NMR	166.00534	XT	105.57302	XTR	0.0	P31OM6	0.0
YMF	-1510.0000	YT	-370.75642	YTR	0.0	QSTR	270
ZMF	-207.00140	ZT	-302.20503	ZTR	-295.05377	MADD	0.0
LMP	5035.7302	LT	-702.54052	LTR	4952.0303	XADD	0.0
MPF	-1267.0710	MT	-10071.123	MTR	-9466.3003	YADD	0.0
NMP	-3342.0770	NT	10757.006	NTR	-26000.410	ZADD	0.0
XMT	-126.05614	XVT	232.42997	ALFMTT	4.0061331	NADD	0.0
YMT	-13.043056	YVT	-257.71256	ALPVT	56.229334	LADD	0.0
ZMT	-217.00004	ZVT	-125.23509	AABMF	4.5902351		

UTTAB(876) 1-21-77 38-AUG-77 RUN 92.

WEIGHT	19980.0	PSC6	347.8	V	150.0	PS1R2	0.0
IX	6268.0	WLC6	240.2999	DELS	-5.0	VX1R.	0.0
IY	81507.0	WMO	0.17500000E-2	V8OUND	1077.0	VX1R.	0.0
I2	30224.0	TIME	0.20000000E-1	DELJMR	0.0	VZ1R.	0.0
OMEGMR	27.01999	NBS3	4.0	TM31MR	-10.0	PSTR.	0.0
OMEGTR	124.62000	NBS8	5.0	TM31TR	-10.0	MLVT	273.0
KPR	15.0	PASCNT	2723.0	WLMT	234.0	PSVT	695.0
FSMT	700.40000	3MT	45.0	SVT	32.50000	QSTR.	0.0
LAT8TK	-0.11033919	A18	-1.2041795	IMT	9.7067363	XA	49.310253
LNG8TK	10.00177	013	6.5982609	IS	-3.0	XB	14.650029
COL8TK	21.076314	THETAB	21.076314	TM75MR	11.796314	XC	71.220965
PEDAL	29.436000	THETTR	37.5	TM75TR	24.0	XP	0.0
XAIN	4.9310235	XBIN	1.4050029	XCIN	7.1220965	XPIN	0.0
XBACTP	9.3971197	XOACTI	0.93971197	RSTM.	0.0	P3TK	0.0
VXB	252.22549	THETAB	-5.7525320	AAP	3.0410210	QSTR	0.0
VYB	01.405359	PHIB	13.503062	AA1P	3.2410725	R3TR	0.0
VZB	-25.409000	DETAMP	17.204977	BB1F	-0.91955432	T1TR	0.0
P	0.0	GMC	0.0	AAUL	-7.3060046	H1TR	0.0
Q	0.0	OMGRAT	1.0	AA1L	0.6220000E-1	J1TR	0.0
R	0.0	PS1DOY	0.0	BB1L	-0.2720016	MH1R	0.0
ALPMP	-7.5544977	EKTX	1.0520910	EKMPX	0.93211034	LM1R	0.0
CHITPP	02.470027	EATZ	1.9704972	EKMPZ	1.0075299	OM1R	0.0
EKTR	0.0	EP8MT	0.93229063	SIGMT	1.0440995	X1TR	0.0
OMF	66.309572	KOMT	0.0177979	KUVT	0.76271000	Y1TR	0.0
MUX3	0.3450006	CT81G	0.1001291	LTOI	0.1177002	Z1TR	0.0
MUY3	0.11234670	CM81G	0.9333000E-2	DIOI	36.555397	L1TR	0.0
MUZ3	-0.5320020E-1	CM81G	0.9333000E-2	TTR	1300.5541	M1TR	0.0
LAMBMR	-0.6572330E-1	NZ	0.0000025	MPMR	1909.0040	N1TR	0.0
OM8MR	0.1251500E-1	VC	-1177.3059	KTRBLK	1.0	AP	-3.0036341
XMR	-625.52095	MBAR	1599.0610	VX8DOY	0.15257655E-2	AP	-9.1274420
YMR	-1229.4009	JBAR	1229.4009	VY8DOY	0.11005700E-1	AP	-31.100047
ZMR	-10519.301	YBAR	10402.673	VZ8DOY	-0.2003742E-1	VXP	252.22549
LMR	-15104.219	LBARM	-5715.4305	POOI	-0.53139100E-2	VYP	61.405359
MMR	21526.101	MBARM	0400.0621	QDOI	-0.52517034E-1	VZP	-25.409000
NMR	39511.119	QBARM	4000.307	ROOI	0.45517610	RSTR.	0.0
XMP	-1510.9294	XY	224.04672	XTR	0.0	PS1UMG	0.0
YMP	-3275.4072	YT	-1100.5315	YTR	1229.7300	STR	2.0
ZMP	192.30000	ZI	293.05007	ZTR	-447.50601	MADD	0.0
LMP	9140.1000	LI	-2535.4071	LTR	7912.0529	XADD	0.0
MPF	-15732.630	MI	0540.1054	MTR	-14360.051	YADD	0.0
NMP	-10401.523	NI	33034.972	NTR	-39453.039	ZADD	0.0
XMT	35.001254	XVT	100.24547	ALPMTT	-1.9032661	NADD	0.0
YMT	-12.346370	YVT	1130.1051	ALPVTI	20.000100	LADD	0.0
ZMT	334.00026	ZVT	-30.949309	AABWIF	3.3689956		

RUN 53.

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WEIGHT	19900.0	PSCB	347.0	DEL8	00.0	P31TR2	0.0
IX	6260.0	WLCC	246.29999	VOUNO	-5.0	VXSTR.	0.0
IY	41507.0	RMO	0.17500000E-2	VSOUNO	1077.0	VYSTR.	0.0
IZ	30224.0	TIME	0.20000000E-1	DEL3MR	0.0	VZSTR.	0.0
OMEGHR	27.01999	NS88	4.0	TMSTR	-10.0	PSTR.	0.0
OMESTR	124.02000	NS88	5.0	TMSTR	-10.0	HLVT	273.0
KPR	15.0	PASCNT	0.50.0	MLMT	236.0	PSVT	693.0
FSMT	700.00000	SMT	45.0	SVT	32.300000	OSTR.	0.0
LATSTK	-1.6519014	AIS	-2.0142400	INT	31.032472	XA	39.075010
LNGSTK	2.1550702	019	0.75175139	IS	-3.0	X0	42.302790
COLSTK	19.023131	THETAB	19.023151	TM75MR	9.7431513	XC	50.394696
PEDAL	20.130203	THETTR	31.349905	TH75TR	17.049905	XP	25.775600
XAIN	3.9075010	XBIN	4.2302709	XCIN	3.0390096	XPIN	1.3918094
XBACTP	47.591939	XBACTI	4.7591930	RSTR.	0.0	PSTR	0.0
VIB	67.505355	THETAB	0.01355204	AA0P	4.3466350	OSTR	0.0
VIB	0.0	PHIB	-1.10608190	AA1P	1.7007909	RSTR	0.0
VZ0	0.95975095	BETAMP	0.0	001P	-0.27305103E-1	TSTR	0.0
P	0.0	GANC	0.0	AA0L	-6.1445566	HSTR	0.0
Q	0.0	OMGRAT	1.0	AA1L	0.15203055	JSTR	0.0
R	0.0	PSIDOT	0.0	001L	-0.20220731	MMSTR	0.0
ALPMP	-20.020439	EKTX	0.05664040	EKMPX	0.71005732	LMSTR	0.0
CHITPP	63.050564	EKZ	2.1410453	EKMPZ	1.0322908	OMSTR	0.0
EKTR	0.0	EPST	0.49999999	SIGMT	0.0	XSTR	0.0
QW	0.2257532	KQMT	0.97402531	KQVT	0.04052013	YSTR	0.0
MUX0	0.93102324E-1	CT916	0.11247063	LTOT	-35.096690	ZSTR	0.0
MUX5	0.0	CM810	0.1010714E-2	DTOT	31.713559	LSTR	0.0
MUX9	-0.35570507E-2	CM816	0.94075064E-6	TTR	1121.0200	MSTR	0.0
LAMBHR	-0.4922097E-1	NZ	0.99934097	MPHR	1673.4533	NSTR	0.0
DM3MR	0.45605040E-1	VC	0.10193070E-1	KTRBLK	1.0	AXP	0.42151644
XMR	292.17495	MBAR	713.94445	VXBDOT	-0.3511727E-1	AYP	0.69464945
YMR	-634.94043	JBAR	634.94043	VYBDOT	0.29000164E-1	AZP	-32.152062
ZMR	-19219.626	TBAR	19205.073	VZBDOT	0.40606394E-2	VXP	67.505355
LMR	-6425.2177	LBAMH	-0.50.00764	PDOT	-0.23157150E-3	VYP	0.0
MHR	12799.661	MBAMH	4001.3073	ODOT	0.07610690E-5	VZP	0.95975095
NMR	33649.003	GBAR	30063.633	RDOT	0.20996624E-3	RSTR.	0.0
XWF	-146.10739	XT	100.10017	XTR	0.0	PSIDMG	0.0
YWF	0.0	YT	-525772977	YTR	1053.5001	STR	2.0
ZWF	360.50205	ZT	102.05607	ZTR	-303.44343	MADD	0.0
LWF	0.0	LT	-12.409407	LTR	6435.5169	XADD	0.0
MWF	-5300.4171	MT	4003.2636	MTR	-12302.143	YADD	0.0
NWF	0.0	NT	101.74163	NTR	-33799.795	ZADD	0.0
XMT	105.52013	XVT	-1.3399675	ALPMTT	-4.9514746	MADD	0.0
YMT	0.0	YVT	-5.5772977	ALFVT	0.0	LADD	0.0
ZMT	101.05503	ZVT	1.00010405	AA001P	1.7010114		

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RUN 54.

WEIGHT	19900.0	PSCG	347.8	V	40.0	PS1TR2	0.0
IX	6260.0	WLCG	246.29999	DELS	-5.0	VXSTR	0.0
IY	41907.0	RHO	0.17500000E-2	VROUND	1077.8	VYSTR	0.0
IZ	30224.0	TIME	0.20000000E-1	DELJMR	0.0	VZSTR	0.0
OMEGMR	27.01999	NBS	4.0	TMSTR	-10.0	PSTR	0.0
OMEGTR	124.62000	NBS	5.0	TMSTR	-10.0	WLVT	273.0
KPR	15.0	PASCNT	000.0	MLMT	234.0	PVVT	093.0
PSMT	700.40000	SMT	45.0	SVT	32.30000	OSTR	0.0
LATSTK	-1.6500335	A18	-2.6134093	IMT	31.047129	XA	39.007103
LNGSTK	3.2922040	B18	0.74925965	IS	-3.0	XB	30.366404
COLSTK	19.033745	THETAB	19.033745	TM7SMR	9.7537459	XC	50.400913
PEDAL	24.230567	THEITR	35.455062	TM7STR	21.955062	XP	14.430672
XAIN	3.9607105	XBIN	3.8366404	XCIN	3.8460912	XPIN	0.77923606
XOACTP	43.500770	XMACTI	4.3540776	RSTR	0.0	PSTR	0.0
VXB	67.500027	THETAB	0.74207536	AADP	4.3402007	OSTR	0.0
VYB	0.0	PHIB	-1.2244400	AAIF	1.7055091	RSTR	0.0
VZB	0.07637330	SETAMP	0.0	001P	-0.20420647E+1	TSTR	0.0
P	0.0	CAMC	0.0	AABL	-6.1590049	MITR	0.0
O	0.0	OMGRAT	1.0	AAIL	0.13200099	JSTR	0.0
R	0.0	PSIDOT	0.0	BAIL	-0.20259296	MMTR	0.0
ALPMP	-20.077173	EKTX	0.035335009	EKMPX	0.70940000	LMTR	0.0
CHITPP	63.003759	EATZ	2.3408577	EKMPZ	1.0323924	OMTR	0.0
EKTR	0.0	EPMT	0.049999999	BIGMT	0.0	XSTR	0.0
QMP	0.2265305	KOMT	0.97507524	KOVT	0.04052013	YSTR	0.0
MUX3	0.9315000E+1	CT8IG	0.11249199	LTOT	-39.202390	ZSTR	0.0
MUY3	0.0	CM8IG	0.41005576E-2	DTOT	31.771004	LSTR	0.0
MUZ3	-0.30719940E-2	COM8IG	0.94910196E-0	TTR	1123.3193	MSTR	0.0
LAMBMR	-0.49327001E-1	NZ	0.99945942	MPMH	1677.3430	NSTR	0.0
DM8MR	0.45055006E-1	VC	0.17139702E+1	KTRBLK	0.79599999	ASTP	0.42335179
XMR	292.45341	H0AR	713.05673	VX0DOT	0.64510299E-2	ATP	0.09634766
YMR	-635.05721	JBAR	0.3505721	VY0DOT	0.10032393E-1	AZP	-32.150622
ZMR	-19210.203	T0AR	19200.721	VZ0DOT	0.54072907E-3	VTP	67.506627
LMR	-6437.0059	LBARM	-050.26002	POOT	0.02003500E-4	VTP	0.0
MMR	12012.055	H0ARM	4074.4100	QDOT	-0.13632999E-4	VZP	0.07637330
NMR	33720.205	0BAR	34342.000	RUOT	0.55019027E+3	RSTR	0.0
XMP	-145.07070	XT	104.70379	XTR	0.0	PSIOMG	0.0
YMP	0.0	YT	-5.3773901	YTR	1095.0533	STR	2.0
ZMP	302.19370	ZT	102.61501	ZTR	-304.22714	MADU	0.0
LMP	0.0	LT	-12.409711	LTR	0440.0702	XADD	0.0
MPF	-5306.3942	MT	4900.2509	MTR	-12327.207	YADD	0.0
NMP	0.0	NT	101.74454	NTR	-33000.077	ZADD	0.0
XMT	106.04320	XVT	-1.3394110	ALPMTT	-4.9690531	MAOD	0.0
YMT	0.0	YVT	-5.3773901	ALPYTT	0.0	LADD	0.0
ZMT	101.61310	ZVT	1.0026209	AAB01P	1.7050000		

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RUN 55.

WEIGHT	19000.0	FACG	347.0	V	1.0E-2	PSITR2	0.0
IX	0200.0	MLCG	240.29999	DEL3	-5.0	VXSTR.	0.0
IY	41507.0	RMO	0.1750000E-2	VROUND	1077.0	VYSTR.	0.0
IZ	30224.0	TIME	0.20000000E-1	DEL3MR	0.0	VZSTR.	0.0
OMEGMR	27.01999	NBS3	4.0	TMSTR	-10.0	PSTR.	0.0
OMEGTR	124.02000	NBS3	5.0	TMSTR	-10.0	MLVT	273.0
KFR	15.0	PASCNT	1631.0	MLMT	234.0	F8VT	695.0
PMT	700.40000	AMT	45.0	SVT	32.30000	OSTM.	0.0
LAT3TK	0.39602424	A10	-0.71475409	IMT	34.0	XA	52.400131
LNG3TK	2.0365976	B10	-1.3421012	IS	-3.0	XB	42.003501
COL3TK	21.27230	THETAB	21.272030	TM75MR	11.192030	XC	67.450190
PEDAL	29.430000	THETTR	37.5	TM75TR	24.0	XP	0.0
XAIN	5.2400131	XOIN	4.2003541	XCIN	6.7450190	XPIN	0.0
XBACTP	40.300430	XOACTI	4.0300435	MSTR.	0.0	PSTR	0.0
VX0	0.16092000E-1	THETAB	1.5065052	AA0P	4.3696401	QSTR	0.0
VY0	0.0	PHI0	-1.9203306	AA1P	1.0633212	RSTR	0.0
VZ0	0.46791933E-3	DETAMP	0.0	BB1P	-0.79400935	TSTR	0.0
P	0.0	QAMC	0.0	AA0L	-7.9990100	MSTR	0.0
Q	0.0	OMGRAT	1.0	AA1L	-0.10034130	JSTR	0.0
R	0.0	PSIDOT	0.0	BB1L	-0.95750331E-1	MMSTR	0.0
ALPMP	-05.774001	EKTX	-0.47997000	EKMPX	0.13497050E-1	LMSTR	0.0
CHITPP	1.6072313	EKYZ	0.50832509	EKMFZ	0.10720267	OMSTR	0.0
EKTR	0.0	EP8WT	0.44999999	SIGMT	0.0	XSTR	0.0
OWF	0.76192019E-1	KQMT	1.0	KUVT	0.04052013	YSTR	0.0
MUX3	0.2330240E-4	CY8IG	0.10971005	LTOI	-70.0	ZSTR	0.0
MUY3	0.0	CH8IG	0.20012200E-2	DTOI	45.079999	LSTR	0.0
MUZ3	-0.57400767E-6	CUM8IG	0.95377906E-6	TTR	1134.0900	MSTR	0.0
LAMBMR	-0.60507003E-1	NZ	0.99006922	MPMR	2165.0455	NSTR	0.0
DM3MR	0.60547100E-1	VC	0.14349207E-4	KTRBLK	0.79599999	AXP	0.70062030
XMR	409.19520	MBAR	491.90659	VXBDOT	0.06371657E-3	AYP	0.19090122
YMR	-426.00053	JBAR	426.00053	VYBDOT	0.24690559E-3	AZP	-32.14231
ZMR	-10733.329	TBAR	10734.711	VZBDOT	-0.09290551E-4	VXP	0.16092000E-1
LMR	-7079.2023	LBARM	-2237.6661	POOI	-0.32506075E-3	VYP	0.0
MMR	11069.005	MBARM	4549.1701	QDOI	-0.11617910E-4	VZP	0.46791933E-3
NMR	43674.505	QBARM	44070.136	RDOI	0.24730507	RSTR.	0.0
XMF	5.0650097	XT	34.751130	XTR	0.0	PSIDMC	0.0
YMF	0.0	YT	-0.34000072E-6	YTR	1066.5270	BTR	2.0
ZMF	3.0104043	ZT	47.062951	ZTR	-300.10513	MADD	0.0
LWF	0.0	LT	-0.77565442E-6	LTR	6515.0991	XADD	0.0
MMF	-40.619009	MT	1433.4030	MTR	-12454.272	YADD	0.0
NMF	0.0	NT	0.10109652E-4	NTR	-34217.767	ZADD	0.0
XMT	34.751131	XVT	-0.05414900E-7	ALFMTT	-17.279165	MADD	0.0
YMT	0.0	YVT	-0.34000072E-6	ALFVTT	0.0	LADD	0.0
ZMT	47.062951	ZVT	0.01590511E-7	AABVTF	1.0431536		

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HEIGHT	19000.0	F3C6	347.8	1.0E-2	PSITRZ	0.0
IX	6200.0	WLCG	246.2999	-5.0	VXSTR.	0.0
IY	41507.0	RMO	0.175000E-2	1077.0	VZSTR.	0.0
IZ	30224.0	TIME	0.2000000E-1	0.0	PSTR.	0.0
ONEGHR	27.01999	NB33	4.0	-10.0	WLVT	273.0
ONEGTR	124.6200	NB38	5.0	-10.0	PST	0.0
KFR	15.0	PASCT	4432.0	236.0	PST	0.0
FSMT	700.4000	GMT	43.0	32.30000	OSTR.	0.0
LATSTR	-1.1170125	A18	-2.1662506	29.111044	XA	43.010671
LANGSTR	0.4660420	B18	-3.2071154	-3.0	XB	46.350373
COLSTR	20.066055	THETAB	20.066055	10.300055	XC	63.667044
PEDAL	29.436000	THETTR	37.5	24.0	XP	0.0
RAIN	4.3010671	XBIN	4.8350373	0.0	XPIN	0.0
XBACTP	53.594721	XOACTI	5.3594721	0.0	PSTR	0.0
V30	0.16095922E-1	THETAB	0.90610033	4.2907000	OSTR	0.0
V70	-30.170771	PHID	-2.0040477	1.7075093	RSTR	0.0
V20	0.20725624E-3	0ETAMP	075.457140	-1.0544009	TSTR	0.0
P	0.0	CAMC	0.0	-7.4013620	HSTR	0.0
Q	0.0	OMGRAT	1.0	-0.70010591E-1	JSTR	0.0
R	0.0	PSIDOT	0.0	0.30100103E-1	HHSTR	0.0
ALPHF	-05.769437	EKTZ	0.0	0.14512106E-1	LMSTR	0.0
CHITPP	1.0140200	EKTZ	0.6133291	0.20135630	OMSTR	0.0
EKTR	0.0	EPST	-0.30999999	-2.0	XSTR	0.0
OHF	1.0009606	KOHT	1.0	0.97467943	VSTR	0.0
MUXS	0.23291979E-4	CT810	0.10075513	-0.0	ZSTR	0.0
MUY3	-0.4714605E-1	CM810	0.47105023E-2	0.3579999	LSTR	0.0
MUZ3	-0.05100519E-0	COM810	0.93655002E-0	0.3357356	MSTR	0.0
LAMBMR	-0.005004954E-1	NZ	0.90001270	2017.0531	NSTR	0.0
DMSMR	0.005004102E-1	VC	-103.10200	0.79599999	AXP	0.11505129
XMR	167.32500	HBAR	005.71419	-0.94770633E-2	AYP	-1.0495971
YMR	-437.71007	JBAR	437.71007	-0.77753300	AZP	-31.320000
ZMR	-10505.732	TBAR	10570.450	0.27601275	VXP	0.16095922E-1
LMR	-7001.7530	LBARM	-2044.0139	-0.31770540	VYP	-34.170771
MHR	13004.070	HBARM	5237.5335	0.12705392	VZP	0.26725624E-3
NHR	00020.015	QBAR	41057.707	0.30736146	RSTR.	0.0
XPF	47.440233	XT	01.460144	0.0	PSIDMG	0.0
YPF	107.90115	YT	43.493100	703.30116	STR	2.0
ZPF	-09.769009	ZT	27.070347	-205.12070	HADD	0.0
LMP	-1.00993194	LT	-0.4000314	4705.5107	XADD	0.0
MMP	20.359011	MT	032.04029	-9147.6223	YADD	0.0
NMP	602.42517	NT	-1334.5510	-25132.037	ZADD	0.0
XMT	63.220009	XVT	10.239455	-22.500437	NADD	0.0
YMT	33.750043	YVT	11.730537	-09.900046	LADD	0.0
ZMT	50.105013	ZVT	-23.027065	2.0753913		

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WEIGHT	10050.0	FSCU	300.20000	Y	100.0	PSIR2	2.2
IX	5629.0	WLC6	206.29999	DEL5	-5.0	VISTR.	2.0
IY	39490.0	AMO	0.23700000E-2	VSDUNU	1117.0	VISTR.	2.0
I2	37226.0	TIME	0.20000000E-1	DEL3MH	2.0	VISTR.	3.0
OMEGM	27.01999	NBS3	0.0	TM31MR	-10.0	PSTM.	2.0
OMEGTR	124.02000	NBS3	5.0	TM31TR	-10.0	MLVT	273.0
KPR	15.0	PASCMT	770.0	KCMT	230.0	PSVT	095.0
F5MT	700.00000	SMT	45.0	SVT	32.300000	OSTM.	0.0
LATSTR	-0.90430113	A13	-1.9032022	IMT	-5.5920071	XA	45.047010
LGSTR	15.471040	B13	10.049704	IS	-3.0	XB	10.236504
CULSTR	19.001309	TMETAR	19.001309	TM75MR	9.3213045	XC	55.750500
PEDAL	14.507741	TMETTR	25.093305	TM75TR	11.593305	XP	41.717202
XAIM	0.3007010	XOIN	1.0230504	XOIN	9.5750359	XPM	2.2920700
XOALTP	12.030090	XOACTI	1.2030096	WSTM.	0.0	PSTM	0.0
VIB	250.30003	TMETAB	2.5700000	AA2P	3.2250001	OSTM	0.0
VIB	14.071704	PHIB	0.0	AA1P	-0.6235321	OSTM	0.0
VZB	10.720000	DELAMF	3.3209210	OB1P	-0.30590005	TITM	0.0
P	0.0	GAMC	0.0	AA2L	-6.5599059	MITM	0.0
Q	0.0	OMGRAT	1.0	RAIL	0.3203991	JITM	0.0
R	0.0	PSIDOT	0.0	OB1L	0.69210171	MMTR	0.0
ALPHF	0.94900102	EKTZ	1.5303705	EXMPX	0.04312500	LMTR	0.0
CHITPP	79.375001	EKTZ	1.7056234	EXMPZ	1.0100249	OMTR	0.0
EKTR	0.0	EP3MT	0.00320921	SIUMT	0.50000226	XITR	0.0
GMP	70.030095	KUMT	0.07177479	KUVI	0.03272602	YITR	0.0
MUX3	0.32631004	CT310	0.04313305E-1	ETOI	0.0300023	ZITR	0.0
MUX3	0.19010076E-1	CHS10	-0.69350030E-2	DTOT	24.52136	LITM	0.0
MUX3	-0.22095509E-2	CHS10	0.51009971E-6	TIR	1532.0324	MITR	0.0
LAMMR	-0.11429934E-1	NZ	0.94090766	MPMH	1702.0000	NITR	0.0
DMSMR	0.41003030E-2	VC	0.14305114E-4	KIRBLK	1.0	AXP	1.0091500
XMR	240.0753	MDAH	-1609.3107	VIBUOT	-0.5503052E-1	AYP	-2.45301203E-1
YMR	-332.50300	JHAM	332.50300	VIBUOT	-0.57020002E-1	AZP	-3.129013
ZMR	-15975.513	TBAR	10003.026	VZBUOT	-0.21017436E-2	VXP	230.50403
LMR	-7909.2010	LWARM	-0.090.0422	PUOT	-0.11125551E-1	VTP	10.071704
MMR	-11515.090	MWARM	-23377.202	UOOT	0.67055040E-2	VZP	10.720000
NMR	35053.021	QBAR	36274.110	RUOT	0.24370500E-2	RYTR	0.0
XMT	-1000.0103	XT	-76.050392	XTR	0.0	PSIDMG	0.0
YMT	-610.33232	YT	-310.36077	YTR	1252.0059	BITM	0.0
ZMT	-310.70967	ZT	1120.0344	ZTR	-455.09032	MAUU	0.0
LMT	900.01074	LT	-095.50533	LTR	7651.0201	XADD	0.0
MMT	-5001.0130	MT	31750.700	MTR	-14125.001	YADD	0.0
NMT	-5390.5209	NT	0000.1400	NTR	-30000.007	ZADD	0.0
XMT	-53.270004	XVT	-23.500327	ALFMT	-6.2720595	MAUU	0.0
YMT	-5.197021	YVT	-310.42704	ALFVT	3.3004907	LABU	0.0
ZMT	1119.7500	ZVT	0.27970117	AABVIF	0.6209573	LABU	0.0

WEIGHT	16450.0	FSCG	300.20000	V	150.0	PSTR2	0.0
IX	5629.0	WLCG	246.29999	DELS	-5.0	VSTR.	0.0
IY	39496.0	RHO	0.23700000E-2	VROUND	1117.0	VSTR.	0.0
IZ	37226.0	TIME	0.20000000E-1	DEL3MR	0.0	VSTR.	0.0
OMEGMR	27.019999	NRSS	4.0	TMSMR	-10.0	PSTR.	0.0
OMEGTR	124.62000	NSSS	5.0	TMSITR	-10.0	MLVT	273.0
KPH	15.0	PASCNT	401.0	MENT	234.0	FST	095.0
FST	700.40000	SMT	45.0	SVT	32.50000	QSTR.	0.0
LATSTR	-1.2311505	AIS	-2.2507430	IMT	-6.0057127	XA	42.505259
LNGSTR	15.535312	BIS	15.000003	IS	-3.0	XB	9.4150571
COLSTR	20.456547	THETAB	20.456547	TH75MR	10.376547	XC	62.353425
PEUAL	14.520290	THETTR	26.500155	TH7STR	15.000155	XP	41.327620
XAIN	4.2505259	XBIN	0.90150571	XCIN	0.2553425	XPM	2.2510330
XOACTP	7.1076531	XOACTI	0.71076531	RSTR.	0.0	PSTR	0.0
VXB	253.20000	THETAB	2.3000000	AAOP	3.2010174	QSTR	0.0
VYB	15.100622	PHIB	0.0	AAIF	-9.5523507	RSTR	0.0
VZB	10.500259	RETMF	3.3362536	BBIF	-0.40000413	YSTR	0.0
P	0.0	GML	0.0	AAOL	-7.5114740	HSTR	0.0
Q	0.0	ORGNAT	1.0	AAIC	0.34991310	JSTR	0.0
R	0.0	PSIDOT	0.0	BBIL	0.79026230	MMSTR	0.0
ALFMF	0.90064477	ERTX	1.5007970	EKMPX	0.00231009	LMSTR	0.0
CHITPP	70.591001	EKTZ	1.7302029	EKMFZ	1.0116001	OMSTR	0.0
EKTR	0.0	EPST	0.00336253	SIGMT	0.50710005	XSTR	0.0
OWF	79.910000	KOMT	0.87177979	KQVI	0.0326236	YSTR	0.0
MUXS	0.30902707	CTSIG	0.09914954E-1	LTOT	3.9556610	ZSTR	0.0
MUYS	0.20029979E-1	CHSIG	-0.77779017E-2	OTOT	24.517443	LSTR	0.0
MUZS	-0.39750000E-2	CHMSIG	0.52703229E-6	TSTR	1520.7905	MSTR	0.0
LAMBHR	-0.12570397E-1	NZ	0.99936765	MPHR	2010.4040	NSTR	0.0
DMSHR	0.06025000E-2	VC	0.10305114E-4	KTRBLA	1.0	APX	1.3170944
XMR	2651.1307	MBAN	-1004.7521	VXBDOT	0.46440699E-2	AYP	-0.12504270
YMR	-597.14501	MBAN	397.14301	VYBDOT	-0.60602003E-1	AZP	-32.159010
ZMR	-16104.000	TBAR	16222.610	VZBDOT	-0.77015274E-2	VXP	253.20409
LMR	-9245.4501	LBARM	-4710.4015	PUOT	-0.39640717E-1	VYP	15.100622
MMR	-15004.012	MBARM	-25002.019	QUOT	0.47504139E-2	VZP	10.300259
NMR	40117.730	QBAM	41005.200	RUOT	-0.61705999E-2	RSTR.	0.0
XMF	-1416.0050	XI	-91.440501	XSTR	0.0	PSIDMG	0.0
YMF	-699.50401	YI	-305.03700	YSTR	1429.1019	OTR	2.0
ZMF	-346.30397	ZI	1342.0077	ZSTR	-520.10009	MADD	0.0
LWF	1104.0617	LI	-790.75205	LSTR	0730.4444	XADD	0.0
MWF	-6750.0992	MI	30002.640	MSTR	-16116.931	YADD	0.0
NWF	-6104.1200	NI	10200.962	NSTR	-44200.019	ZADD	0.0
XMT	-64.393691	XVT	-27.046009	ALFMTT	-6.6344276	MADD	0.0
YMT	-4.0077009	YVT	-561.14921	ALFVTT	3.300177	LADD	0.0
ZMT	1342.5099	ZVT	0.29774070	AABVIF	9.5640660	LADD	0.0



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WEIGHT	1900.0	PSCG	300.20000	V	1.0E+2	PSIR2	0.0
IX	6200.0	MLCG	246.29999	DELS	-5.0	VXSTR.	0.0
IY	41507.0	RMO	0.1750000E-2	VROUND	1077.0	VYSTR.	0.0
IZ	50224.0	TML	0.2000000E-1	DELJMH	0.0	VZSTR.	0.0
OMEGMR	24.72000	NOSS	4.0	TASTMR	-10.0	PSTR.	0.0
OMEGIR	137.07999	NSSS	5.0	TWSTIR	-10.0	MLVI	273.0
KFR	15.0	PASGNT	1305.0	MCMT	236.0	PSYI	095.0
FSMT	700.40000	SMT	45.0	SVT	32.50000	OSTR.	0.0
LATSTR	-0.10000719	AIS	-1.0992175	IMT	29.702701	XA	40.070954
LMGSK	3.1652100	GIS	1.0593656	IS	-5.0	XB	30.015490
COLSTR	19.590150	TMETAB	19.590150	TM7SHR	9.3101502	XC	55.730490
PEVAL	20.001020	TMETR	34.703617	TM7STR	17.263617	XP	25.907391
XAIN	4.0070934	XBIN	3.003490	XCIN	5.5750490	XPIN	1.0032020
XBACTP	45.570000	XBACTI	4.5570009	RSTR.	0.0	PSTR	0.0
VXB	0.10037379E-1	TMETAB	4.0000504	AABP	3.5010033	OSTR	0.0
VYB	0.0	PMIB	-2.9721521	AAIF	-1.7046364	RSTR	0.0
VZB	0.14503907E-2	DETAMP	0.0	BBIF	-1.1039717	TITR	0.0
P	0.0	GMC	0.0	AAEL	-0.5223501	HITH	0.0
Q	0.0	OMGRAT	1.0	AAIL	-0.1572700E-1	JITR	0.0
R	0.0	PSUDOT	0.0	BBIL	0.12097491	MMITR	0.0
ALPMP	-13.230100	ERTX	-0.20104423	EKMPX	0.79995393E-5	LMITR	0.0
CHITPP	-1.7606501	ERTZ	0.24202269	EKMPZ	0.11099360E-3	OMITR	0.0
ERTR	0.0	EPST	0.44999999	SIGMT	0.0	XITR	0.0
QMF	0.2742405E-6	KQMT	0.07177979	KQVI	0.04052013	VITR	0.0
MUXS	0.0	CTSI0	0.0909000E-1	LTOI	-20.771052	ZITR	0.0
MUYS	0.0	CM5IG	-0.31010500E-2	DTOT	26.627203	LITR	0.0
MUZS	0.09619090E-6	CM5IG	0.63105210E-6	TTR	1426.0223	MITR	0.0
LAMBMR	-0.6205020E-1	NZ	0.99000526	MPHM	2290.0596	NITR	0.0
DW5HMR	0.6205021E-1	VC	0.1232427E-3	KTRBLK	0.79599999	AXP	2.7470035
XMH	1624.1901	MPAR	-655.19994	VXDUOT	0.94352139E-2	AYP	1.6699127
YMH	-350.50012	JMH	350.50012	VYDUOT	0.71051254E-2	AZP	-32.009246
ZMR	-10510.732	TBMH	10571.011	VZDUOT	-0.25760700E-3	VXP	0.16037379E-1
LMH	-0109.0105	LBARM	-3005.0195	PDOT	0.11449512E-3	VYP	0.0
MMH	14079.140	MDAMH	-5902.1947	QUOT	0.50359400E-4	VZP	0.0
NMH	41556.573	QMAR	42379.974	RUOT	-0.20709040E-3	RSTR.	0.0
XMF	-0.50030052E-5	XT	0.0130094	XTR	0.0	PSIUMG	0.0
YMF	0.0	YT	-0.50902633E-6	YTR	1340.0741	OTR	0.0
ZMF	0.7217330E-5	ZT	0.4019962	ZTR	-000.03922	MADD	0.0
LMF	0.0	LT	-0.77050361E-6	LTR	0190.9907	XADD	0.0
MMF	-0.10300670E-3	MT	244.30003	MTR	-15121.001	YADD	0.0
NMF	0.0	NT	0.97370347E-5	NTR	-01544.75	ZADD	0.0
XMT	6.0150096	XVT	-0.79245321E-7	ALFMTT	-11.027455	MADD	0.0
YMT	0.0	YVT	-0.50902633E-6	ALFVTT	0.0	LADD	0.0
ZMT	0.4019962	ZVT	0.60427693E-7	AAB01F	2.1416620		

RUN 29.

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UTIAS(876)

HEIGHT	1998.8	PSCG	308.20888	V	48.8	PSSTR2	0.8
IX	6268.8	WLCG	246.29999	DELS	-5.3	VXSTR.	0.8
IY	41587.8	RMO	0.1752088E-2	VSOUMU	1377.8	VYSTR.	0.8
IZ	38224.8	TIME	0.24803208E-1	DELJMR	0.8	VZSTR.	0.8
ONEGMR	29.120888	MS3	4.8	TMSTRM	-10.2	PSSTR.	0.8
ONEGTR	137.87999	MS3	5.8	TMSTRM	-10.2	MLVT	273.8
KPR	15.8	PASCENT	776.8	PCMT	238.8	PSVT	695.8
FSMT	788.42040	SMT	45.8	SVT	32.58888	OSTM.	0.8
LATSTR	-1.8623889	A18	-2.0402275	IMT	28.42888	XA	30.302569
LONGSTR	4.5856219	B18	4.1527865	IS	-3.8	XB	33.796388
CULSTR	10.112277	THETAB	10.110277	TH7SMR	0.8382776	XC	47.689235
PEDAL	14.879096	THETTR	24.835429	TH7STR	10.535429	XP	44.355132
IAIN	3.8363569	XBIN	3.3796388	XCIN	4.768235	XPIN	2.1791288
XOACTP	44.545287	XOACTI	4.8545287	RSIM.	0.8	PSIM	0.8
VXB	67.351296	THETAB	4.8653151	AAOP	3.4938685	GSTR	0.8
VVB	8.8	PMIB	-1.6598391	AAIP	-2.6327256	RSIM	0.8
VZB	5.7332120	BETAMP	0.8	BBIP	-0.58590428	TITR	0.8
P	8.8	GAMC	0.8	AABL	-5.2941614	MITH	0.8
Q	8.8	UMGRAT	1.8	BBIL	8.22598267	JITR	0.8
R	8.8	PSIUOT	0.8	BBIL	0.12645654	MHITR	0.8
ALFMP	-17.886901	ERTX	0.97795463	ERMPX	0.68903678	LMITR	0.8
CHITPP	62.295131	ERTZ	2.0161556	ERMPZ	1.8350897	OMITR	0.8
ERTP	8.8	EP3MT	0.44999999	SIGMT	0.8	XITR	0.8
QF	7.9435622	KOMT	4.93257828	KUVT	0.84052813	YITR	0.8
MUXS	0.84718988E-1	CT3IG	8.92688288E-1	LTOT	-38.773882	ZITR	0.8
MUYB	8.8	CM3IG	-8.33631088E-2	DIOT	29.984997	LITR	0.8
MUZB	8.27591628E-2	CM3IG	0.63835053E-6	TTR	1143.4731	MITH	0.8
LAMBMR	-0.39630301E-1	NZ	0.99597988	MPMR	1041.7487	NITH	0.8
DMSMR	0.42397543E-1	VC	0.15147328	KTBULK	1.8	AXP	2.7515185
KMH	1645.7923	MBAR	-694.77522	VX800T	0.22714213E-1	AYP	0.95865826
YMR	-588.14386	JBAR	388.14386	V7800T	0.38328287E-1	KZP	-52.888888
ZMR	-1982.472	TBAR	19146.568	VZ800T	-0.51649546E-2	VXP	67.351296
LMR	-6557.8378	LBARM	-1798.7748	POOT	-0.18838189E-2	VYP	0.8
MMR	12749.675	MBARM	-6628.1184	QUOT	0.18775330E-3	VZP	5.7332120
NMR	33114.781	QBARM	38883.357	ROOT	-0.69834818E-3	WSTR.	0.8
XMF	-158.96575	XT	0.7518338	XTR	0.8	PSIDMG	0.8
YMF	7.8	YT	-5.5843539	YTR	1078.3931	STR	4.8
ZMF	585.61888	ZT	156.73581	ZTR	-391.12467	MADD	0.8
LMF	8.8	LT	-12.425187	LTR	6564.3677	XADD	0.8
MMF	-5104.2757	MT	4537.3834	MTR	-12118.222	YADD	0.8
NMF	0.8	NT	155.88347	NTR	-33294.477	ZADD	0.8
XMT	88.918543	XVT	-1.4882123	ALFMT1	-4.8552675	MADD	0.8
YMT	8.8	YVT	-5.5843539	ALFVT1	8.8	LADD	0.8
ZMT	155.881619	ZVT	8.91962239	AAB01F	2.6508388		

UTIAS(S76) 1-21-77 0-SEP-77 RUN 30.

HEIGHT	19900:0	PSCG	300-20000	Y	00.0	PSIR2	2.0
IX	6200.0	MLCG	246.29999	ULLS	-5.0	VXSR.	0.0
IY	41507.0	RMO	0.1752000E-2	VOUND	1077.0	VYSTR.	0.0
IZ	30224.0	TIME	0.20000000E-1	DELMM	0.0	VZSTR.	0.0
OMEGMR	29.720000	NSS	4.0	TMTM	-10.0	PSTM.	0.0
OMEGTR	137.07999	NSS	5.0	T-SITR	-10.0	PLVT	273.0
KPR	15.0	PASCNT	1595.0	KCMT	238.0	PSVT	095.0
FSMT	700.40000	SMT	45.0	SVT	32.50000	USTH.	0.0
LATSTK	-1.0040093	AIS	-1.7075504	IS	20.054502	XA	43.72440
LMGSK	5.1095420	WIS	4.4729500	IS	-5.0	XB	31.945070
COLSTK	17.309717	TMETAB	17.509717	TMTMM	7.2297170	XC	42.605730
PEVAL	14.777301	TMETTH	22.972963	TMTSTR	9.4729630	XP	40.637331
XAIN	4.3724400	XBIN	3.1945070	XCM	4.2005737	XPM	2.1943500
XOACTP	36.002150	XOACTI	3.6002150	XSTH.	0.0	PSTM	0.0
VIB	101.23045	TMETAB	3.1041000	AAP	3.3500099	OSTH	0.0
VIB	10.700043	PMH	0.0	AAP	-1.7030703	MSTM	0.0
VZB	5.6322750	BETAMP	0.7106346	001F	-0.00200670E-1	VITH	0.0
P	0.0	GAMC	0.0	AABL	-4.1090185	MITH	0.0
Q	0.0	OMGRAT	1.0	AAIL	0.10997900	JITH	0.0
R	0.0	PSIDOT	0.4	BAIL	0.55203020E-1	HMITH	0.0
ALFMF	-0.5034027	ERTX	1.2607330	EMAX	0.04050757	LMITH	0.0
CHITPP	75.326140	EKTZ	1.9474107	EMFZ	1.0146730	OMITH	0.0
ERTP	0.0	EP9MT	0.53710633	SIGMT	1.3411107	XITH	0.0
QMF	13.453550	KGMT	0.07177979	KQVT	0.73900551	VITH	0.0
MUS	0.12714045	GT816	0.91301501E-1	LTOT	-7.9570454	ZITH	0.0
MU2S	0.23559400E-1	CM516	-0.19046652E-2	DTOT	27.005971	LITH	0.0
MU2S	0.00002732E-3	CM516	0.60450435E-6	TTR	944.43595	MITH	0.0
LAMBMR	-0.29097545E-1	NZ	0.99037233	MPHR	1510.5206	NITH	0.0
OM3MR	0.29506372E-1	VL	0.71525573E-5	KTRBLK	1.0	AXP	1.7063109
XMR	1390.9626	MBAR	-410.00676	VXBUOT	-0.64754310E-3	AYP	0.66731109E-3
YMR	-470.51056	JBAR	470.51056	VYBUOT	0.19031103E-2	AZP	-32.121729
ZMR	-10021.216	TBAR	10070.000	VZBUOT	0.34937545E-3	VXP	101.23605
LMM	-5045.1019	LBARM	-1560.3721	PUOT	-0.63575558E-3	VYP	10.706043
MRR	16750.715	MBARM	-5990.4033	QUOT	0.67754700E-4	VZP	5.6322750
MRR	27202.375	QBARM	20101.029	ROOT	0.66905464E-4	RSTM.	0.0
XMF	-311.00402	XT	-25.297420	XTR	0.0	PSIDMG	0.0
YMF	-311.00702	YT	-103.97236	YTR	007.54540	STR	4.0
ZMF	155.19304	ZT	-67.067341	ZTR	-323.04076	MAUU	0.0
LRF	640.51240	LT	-225.29700	LTR	5421.7496	XADD	0.0
MRF	-4757.7502	MT	-1970.2643	MTR	-10000.079	YADD	0.0
MRF	-2600.9214	NT	2401.6654	NTR	-27499.117	ZADD	0.0
XMT	-31.050945	XVT	0.5015750	ALFMTT	1.6200460	NADD	0.0
YMT	-1.0509019	YVT	-102.11345	AEVTT	12.550330	LADD	0.0
ZMT	-05.570441	ZVT	-2.2003900	AAB01F	1.7062900		

RUN 31.

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UITAS(376)

WEIGHT	19900.0	FSCG	360.20000	V	00.0	PSITR2	0.0
IX	6260.0	MLCG	246.29799	UELS	-5.0	VASIR.	0.0
IY	41507.0	RMO	0.17500000E-2	V SOUND	1077.0	VSTR.	0.0
IZ	30224.0	TIME	0.20000000E-1	DEL SPM	0.0	VSTR.	0.0
OMEGMR	29.720000	NBSS	4.0	TASIMR	-10.0	PLVT.	0.0
OMEGTR	137.07999	NSSS	5.0	TASIMR	-10.0	MLVT	273.0
KFR	13.0	PASCENT	1007.0	HEMT	230.0	PSVT	695.0
FSMT	700.40000	SMT	45.0	INT	32.500000	OSTH.	0.0
LATSTK	-0.06380913	A13	-1.5620650	IS	-5.0	XA	44.603192
LNGSTK	6.5006975	B19	6.0730307	TH75MR	7.1667565	XC	27.425096
COLSTK	17.266756	THETAB	17.266756	TH75TR	0.1792552	XP	42.292229
PEDAL	13.559147	THEITR	21.679255	XCIN	4.2292229	IPIN	44.014330
XAIN	4.4603192	XBIN	2.7423096	RSTM.	0.0	PSTR	2.3767125
XBACTP	50.699056	XBACTI	3.0699056	AARP	3.3119296	OSTR	0.0
VX0	130.95721	THETAB	3.3700634	AAIF	-2.0742610	RSTR	0.0
VY0	16.663559	PHI0	0.0	001P	0.12632037E-1	TSTR	0.0
VZ0	7.9705939	BETAMP	6.3493937	AABL	-4.1637265	MITM	0.0
P	0.0	GAMC	0.0	AAIL	0.22006940	JTR	0.0
R	0.0	OMGRAT	1.0	B01L	0.16515222	MMTR	0.0
ALPWF	-3.9247009	ERTX	1.4150427	EMPRX	0.09823934	LMTR	0.0
CHITPP	79.039941	EKTZ	1.7901927	EKPFZ	1.0101600	OMTR	0.0
EKTH	0.0	EPST	0.51349395	SIGMT	1.0473250	XITM	0.0
QMF	20.567207	KUMT	0.07177979	KQVT	0.79462050	YITM	0.0
MUXS	0.16932721	CTSIG	0.91608117E-1	LTOT	-1.8397098	ZITR	0.0
MUZS	0.2110500E-1	CHSIG	-0.29059606E-2	DTOT	25.309637	LITM	0.0
MUZS	0.11256073E-2	CHMSIG	0.59732579E-0	TTR	950.09496	MITM	0.0
LAMBMR	-0.21601152E-1	NZ	0.94819076	MPMH	1500.0521	NITM	0.0
DMSMR	0.22704750E-1	VC	0.35763706E-5	KTMOLK	1.0	AXP	1.9105933
XMK	1006.4196	M0AR	-610.00174	VXUUT	0.12561543E-1	AYP	-0.1605710E-2
YMR	-420.95904	J0AR	420.95904	VYUUT	-0.32027503E-2	AZP	-32.117190
ZMR	-10075.292	T0AR	10934.996	VZUUT	0.43332430E-3	VXP	134.95721
LMR	-5793.9561	L0ARM	-1792.7701	PUOT	0.10023207E-3	VYP	16.063559
MMR	12000.346	M0ARM	-9557.0988	QUOT	-0.59530000E-3	VZP	7.9703939
NMR	27009.950	Q0AR	27040.079	RUOT	-0.51200110E-3	RSTR.	0.0
XMF	-479.33020	XT	5.1546376	XTR	0.0	PSIOMG	0.0
YMF	-339.94231	YT	-139.10040	YTR	0.99700004	STR	0.0
ZMF	62.290921	ZT	06.770994	ZTR	-327.23391	MADD	0.0
LWF	599.52227	LT	-293.47235	LTR	5492.1253	XADD	0.0
MWF	-4356.7046	MT	2462.4000	MTR	-10130.797	YADD	0.0
NWF	-2915.9429	NT	3742.0797	NTR	-27056.062	ZADD	0.0
XMT	4.2032710	XVT	0.07130637	ALFMTT	-1.4361324	NADD	0.0
YMT	-1.5000132	YVT	-132.59230	ELPVT	7.0330000	LADD	0.0
ZMT	86.920516	ZVT	-0.15752107	AAB01F	2.0742007		

UTIAS(376)

1-21-77 0-SEP-77

RUN 32.

WEIGHT	1990.0	PSCG	300.20000	DEL3	100.0	PSITR2	0.0
IX	6260.0	ALCC	200.29999	VSOUND	-5.0	VXSTR.	0.0
IY	41507.0	RHO	0.1750000E-2	YSTR.	1077.0	VYSTR.	0.0
IZ	30220.0	TIME	0.2000000E-1	DEL3MH	0.0	VZSTR.	0.0
OMEGMR	24.72000	MS93	4.0	TM31MH	-10.0	PSTR.	0.0
OMEGTR	137.07999	MS93	5.0	TM31TH	-10.0	MLVT	273.0
KPR	15.0	PASCNT	1078.0	MLMT	230.0	PSY	095.0
FSMT	700.00000	SMT	45.0	SVT	32.50000	QSTR.	0.0
LATSTK	-0.02073773	AIS	-1.5033414	IMT	0.3100020	XA	44.020309
LONGSTK	0.3081412	BIS	0.3060096	IS	-3.0	XB	20.324412
CULSTK	17.012075	JMETAB	17.012075	TM75MH	7.5520752	XC	44.575470
PEDAL	12.900977	JMETTR	21.503460	TM75TR	0.0034600	XP	45.716960
XACTP	22.316242	XOIN	2.0324012	XCIN	0.4575470	XPIN	2.0000510
VIB	160.00267	XOACTI	2.03276292	RSTH.	0.0	PSIN	0.0
VIB	16.000000	JMETAB	3.9000096	AADP	3.3062001	QSTR	0.0
VIB	11.709545	PMID	0.0	AAIP	-4.5202006	RSTR	0.0
P	0.0	DELAMP	5.2095393	BBIP	0.00694003E-2	TITR	0.0
Q	0.0	GANC	0.0	AAOL	-4.5034114	MITR	0.0
R	0.0	OMGRAT	1.0	AAIC	0.27105975	JITR	0.0
ALRMP	-0.98771667	PAIOUT	0.0	BBIL	0.32303940	MMTR	0.0
CHITPP	0.1464500	EKTA	1.3024710	EKMPX	0.91903952	LMTR	0.0
ERK	0.0	EKTZ	1.0997029	EKMFZ	1.0005354	QMTR	0.0
QHP	29.290001	EPST	0.50209539	SIGMT	0.91590207	XITR	0.0
MUS	0.21190075	KOHT	0.07177979	KUVT	0.01027659	VITR	0.0
MUS	0.21190075	CT910	0.02432559E-1	CTOT	1.0720475	ZITR	0.0
MUS	0.30479315E-2	CH910	-0.49240732E-2	OTOT	24.753723	LITR	0.0
LAMBMR	-0.10079360E-1	CUM910	0.59650797E-6	TIR	1067.0070	MITR	0.0
DMSMR	0.10527500E-1	NZ	0.99762792	MPHM	1649.4045	NITR	0.0
XMR	2015.2090	VC	0.71525573E-5	KTRMLK	1.0	AXP	2.2400346
YMR	-0.2145001	MBAR	-1017.4165	VXBUOT	0.52200777E-2	AYP	-0.23040003E-2
ZMR	-19010.500	JBAR	421.45001	VYBUOT	-0.37055947E-2	AZP	-32.090532
LMR	4301.1411	TBAR	19095.399	VZBUOT	0.67652910E-3	VXP	160.60267
MMR	29004.077	LBARM	-2201.6090	PUOT	-0.10100409E-3	VYP	16.064006
XMF	-691.52344	MBARM	-14997.523	DOOT	0.12902560E-2	VZP	11.749545
YMF	-400.52006	QBAR	30523.973	RUOT	-0.69660390E-3	RSTK	0.0
ZMF	-42.916909	XT	6.0095030	XTR	0.0	PSIDMG	0.0
LWF	652.05220	YT	-177.20119	YTR	1002.7339	STR	0.0
MMF	-3779.0502	LT	-300.33170	ZTR	-364.46602	MADD	0.0
NMF	-3507.0031	MT	10700.571	LTR	6125.4016	XADD	0.0
XMT	9.7065251	NT	4905.0120	MTR	-11507.065	YADD	0.0
YMT	-2.0033000	XVT	-3.2967392	NTR	-31060.040	ZADD	0.0
ZMT	374.36909	YVT	-170.75704	ALFMTT	-4.745133	NADD	0.0
		ZVT	0.29235434	ALFVTT	5.0505320	LADD	0.0
				AAB01P	4.5202050		

UTIAS(376) 1-21-77 8-3EP-77 RUN 33.

WEIGHT	1900.0	FSCG	360.20000	V	120.0	PSIRZ	0.0
IX	6260.0	WLCG	246.29999	DELS	-5.0	VXSTR.	0.0
IY	41507.0	RHO	0.17500000E-2	V SOUND	1077.0	VYSTR.	0.0
IZ	30224.0	TIME	0.20000000E-1	DELSMR	0.0	VZSTR.	0.0
OMEGMR	29.72000	NOSS	4.0	THSTR	-10.0	PSTR.	0.0
OMEGTR	137.07999	NSSS	5.0	THSTR	-10.0	WLVT	273.0
KFR	15.0	PASCNT	923.0	WLMT	230.0	FSVT	695.0
FSMT	700.40000	SMT	45.0	SVT	32.30400	QSTM.	0.0
LATSTR	-0.06035361	AIS	-1.0795210	IMT	-1.2005797	XA	44.571530
LNSTR	9.3633607	BIS	9.5936403	IS	-3.0	XB	16.913961
COLSTR	18.351533	THETAB	18.351533	TH7SMR	0.2715330	XC	49.197007
PEDAL	12.753790	THETIR	22.199630	TH7STM	0.6996300	XP	46.246954
XAIN	4.4571330	XBIN	1.0913961	XCIN	4.9197007	XPIN	2.4972706
XOACTP	17.145520	XOACTI	1.7145520	RSTM.	0.0	PSTR	0.0
VXB	202.49720	THETAB	3.0006592	AARP	3.2030330	QSTR	0.0
VYB	17.254001	PHIB	0.0	AAIP	-4.9227747	RSTM	0.0
VZB	10.785430	BLTAMP	4.0120010	BBIP	-0.23252390E-1	TITR	0.0
P	0.0	GMC	0.0	GAOL	-5.3454601	HITH	0.0
Q	0.0	OMGRAT	1.0	AIL	0.29737302	JITR	0.0
R	0.0	PSIDUT	0.0	BOIL	0.40102949	HMITR	0.0
ALFHF	-0.44969907	ERTX	1.3053399	EKMPX	0.92132250	LMITR	0.0
CHITPP	0.040199	ERTZ	1.6016221	EKMPZ	1.0003590	OMITR	0.0
ERTR	0.0	EPSWT	0.49012000	SGWT	0.81172625	XITR	0.0
OMF	40.291239	KUNT	0.8177979	KLVT	0.82650066	YITR	0.0
MUXS	0.25820099	CYSIG	0.92007675E-1	LTOT	2.3051923	ZITR	0.0
MUYS	0.2163062E-1	CHSIG	-0.06761326E-2	DTOT	24.502415	LITR	0.0
MUZS	0.2160099E-3	COMSIG	0.59245085E-0	YTR	1250.5213	HITR	0.0
LAMBHR	-0.15200270E-1	NZ	0.99069149	HPHM	1922.7106	NITR	0.0
OM3MR	0.15500274E-1	VC	0.71525373E-3	KIMBLA	1.0	AXP	1.7012054
XMR	1965.0700	HBAH	-966.02993	VXDUOT	-0.15970950E-1	AYP	0.30676194E-1
YMR	-450.70372	JBAR	450.70372	VYDUOT	0.21029900E-1	AZP	-32.136103
ZMR	-19053.314	TBAR	19131.576	VZDUOT	-0.59262140E-2	VXP	202.49720
LMR	-7429.3032	LBARM	-2005.4062	PUOT	0.10595650E-1	VYP	17.254001
MMR	3445.7030	MBARM	-10271.909	QUOT	-0.55024709E-2	VZP	10.705430
NMR	30027.009	QBAR	33501.791	ROOT	0.60970112E-3	RSTR.	0.0
XMF	-951.00701	XT	-0.3002097	XTR	0.0	PSIDMG	0.0
YMF	-400.03207	YT	-220.79003	YTR	1100.0310	BTR	0.0
ZMF	-05.416314	ZT	505.49636	ZTR	-029.70041	MADU	0.0
LMF	772.33105	LT	-491.30073	LTR	7213.3471	XADD	0.0
MMF	-4620.4055	MT	14345.301	MTR	-13316.277	YADD	0.0
NMF	-4315.1024	NT	6273.0001	NTR	-30500.100	ZADD	0.0
XMT	-1.2023415	XVT	-7.1050000	ALFMTT	-0.7507045	NADD	0.0
YMT	-2.7270003	YVT	-222.00003	ALPVT	0.9065022	LADD	0.0
ZMT	505.00057	ZVT	0.43570593	AABHIF	4.9220394		

UTIAS(376) 1-21-77 0-SEP-77 RUN 34.

WEIGHT	19900.0	PSCG	300.20000	Y	140.0	PSITR2	0.0
IX	6266.0	WLC6	246.29949	DELS	-5.0	VXSTR.	0.0
IY	41507.0	RMO	0.17500000E-2	VSOUND	1077.0	VYSTR.	0.0
IZ	30224.0	TIME	0.20000000E-1	DEL3MH	0.0	VZSTR.	0.0
OMEGMR	29.720000	NBS3	4.0	TMS1MH	-10.0	PSY.	0.0
OMEGTR	137.07949	NSS3	5.0	TMS1TR	-10.0	MLVT	273.0
KFR	15.0	PASCNT	1007.0	MLMT	234.0	PSVT	635.0
FSMT	700.40000	SMT	45.0	SVT	32.30000	QSTR.	0.0
LATSTR	-1.1377135	A13	-2.0796200	IMT	-2.6254759	XA	42.009290
LONGTK	10.900463	B13	11.377025	IS	-3.0	XB	11.460325
COLSTR	19.024000	THETAR	19.024000	TM75MH	9.340002	XC	57.155052
PEDAL	15.200700	THETTH	24.102550	TM75TH	10.602550	XP	40.985617
XAIN	4.2009209	XBIN	1.1000325	XCIN	3.7153051	XPIN	2.0291001
XBACTP	9.0390011	XBACTI	0.90390011	RSTM.	0.0	PSR	0.0
VXB	250.47002	THETAB	2.0155900	AARP	3.2099344	QSTR	0.0
VYB	19.075013	PHIB	0.0	AAIP	-5.6721763	RSTR	0.0
VZB	0.3222070	BEYAMF	0.0157017	BBIP	-0.21711430	TSTR	0.0
P	0.0	GANC	0.0	AA8L	-6.0022009	MTTR	0.0
R	0.0	OMGRAT	1.0	AAIL	0.3430790	JSTR	0.0
ALFMR	-0.50031063	PSIDOT	0.0	BBIL	0.52950709	MMTR	0.0
CHITPP	0.0766110	ERTX	1.4793429	ERMPX	0.90995941	LMTR	0.0
ERTN	0.0	ERTZ	1.0002424	ERMPZ	1.0092230	OMTR	0.0
QMP	53.370071	EPST	0.49015701	SLMT	0.0123760	XSTR	0.0
MUXS	0.24007343	KUMT	0.07177979	KQVT	0.02640275	VSTR	0.0
MUTS	0.24025912E-1	CT910	0.93300090E-1	LTOT	2.1000003	ZSTR	0.0
MUZS	-0.50903063E-2	CHS10	-0.45409000E-2	DTOT	24.503150	LSTR	0.0
LAMBMR	-0.10470251E-1	CHS16	0.59355039E-0	TTR	1000.5053	MTM	0.0
OMSHMR	0.13390051E-1	NZ	0.990001479	MPMH	2440.7140	MTM	0.0
XMR	1906.2001	VC	0.14305114E-4	KTRBLK	1.0	AXP	1.1165260
YMR	-574.30010	MBAN	-930.91900	VX800T	-0.44009550E-2	AYP	-0.50474600E-1
ZMR	-19197.737	JBAN	579.10010	VY800T	-0.29330000E-1	AZP	-32.127057
LMR	-9091.7502	TBAN	19274.707	VZ800T	0.20539400E-1	VXP	230.47062
MMR	1334.3227	LBARM	-3073.2051	PDOT	-0.16070500E-1	VYP	14.075613
NMR	40017.007	MBARM	-10730.600	QDOT	0.63705050E-2	VZP	0.3222676
XMF	-1201.1144	QBAN	45242.020	RUOT	-9.20452100E-2	RSTR.	0.0
YMF	-605.50005	XT	-16.434600	XTR	0.0	PSIDMG	0.0
ZMF	-102.90720	YT	-302.53150	YTR	1509.7710	STR	0.0
LWF	1020.0193	ZT	700.07052	ZTR	-549.51279	MADD	0.0
MMF	-0310.5390	LT	-600.15027	LTR	9222.7345	XADD	0.0
NMF	-5722.4003	MT	2207.272	MTR	-17025.737	YADD	0.0
XMT	-6.1943011	NT	0442.4200	NTR	-46777.739	ZADD	0.0
YMT	-3.9900190	XVT	-10.240345	ALFMTT	-5.6272312	NADD	0.0
ZMT	700.53351	YVT	-290.53690	ALFVTI	4.0507007	LADD	0.0
		ZVT	0.53701391	AA00IF	5.6765300		

UTIAS(1576) 1-21-77 0-SEP-77 RUN 35.

WEIGHT	19900.0	FSCG	360.20000	V	150.0	PS1TR2	0.0
IX	6260.0	WLCG	244.29999	DELS	-5.0	V1STR.	0.0
IY	411.07.0	RMD	0.17500000E-2	V5OUND	1077.0	V1STR.	0.0
I2	30224.0	TIME	0.20000000E-1	DELJMR	0.0	V2STR.	0.0
OMEGMR	24.720000	NBS	4.0	TWSTMR	-10.0	PSTR.	0.0
OMEGTR	137.07999	NSS	5.0	TWSTTR	-10.0	MLVT	273.0
KTR	15.0	PASCNT	900.0	WLMT	234.0	F5VT	695.0
FSMT	700.40000	SMT	45.0	SVT	32.300000	OSTR.	0.0
LNGSTK	-1.3630394	AIS	-2.3009447	IMT	-2.0001100	XA	41.401003
LANGSTK	11.023017	BIS	12.446415	IS	-3.0	XB	8.2197262
COLSTK	20.440245	THETA0	20.440245	TH7SHR	10.360245	XC	62.251535
PEDAL	13.510497	THETTR	25.470792	TH7STR	11.970792	XP	44.127029
XAIN	4.1401005	XBIN	0.02197261	XCIN	6.2251535	XPIN	2.3827976
XBACTP	5.6647397	XBACTI	0.56647396	RSTR.	0.0	PSTR	0.0
VXB	253.34864	THETA0	1.5016719	AA0P	3.3054247	OSTR	0.0
VYB	21.320423	PHIB	0.0	AA1P	-6.1142350	RSTR	0.0
VZB	6.6432341	BLTAMF	4.6450350	BB1F	-0.35353374	TSTR	0.0
P	0.0	GAMC	0.0	AR0L	-7.7638701	MTR	0.0
Q	0.0	OMGRAT	1.0	AA1L	0.37319753	J1TR	0.0
R	0.0	PSIDOT	0.0	BB1L	0.01204597	MMTR	0.0
ALFWF	-0.7529760	EKTX	1.5402260	EKMPX	0.90169414	LMTR	0.0
CMITPP	80.130320	EKTX	1.0004013	EKMPZ	1.0090096	QMTR	0.0
EKTR	0.0	EPST	0.49645035	SIGMT	0.01766713	X1TR	0.0
OMF	60.667659	KGMT	0.87177979	KQVT	0.02633720	Y1TR	0.0
MUXS	0.51776104	CTSIG	0.95021943E-1	L1UT	1.9519770	Z1TR	0.0
MUTS	0.26745304E-1	CHSIG	-0.44804303E-2	DTOT	24.509166	L1TR	0.0
MUZS	-0.83119494E-2	COMSIG	0.59635312E-6	TTR	1034.5744	M1TR	0.0
LAMBHR	-0.20067926E-1	NZ	1.0007173	MPMR	2790.6509	M1TR	0.0
OMSHMR	0.12555977E-1	VC	0.35762706E-5	KIRBLK	1.0	AXP	0.0376090
XMR	1930.6271	MDAR	-925.60031	VXDDOT	-0.22431003E-1	AYP	0.53100193E-1
YMR	-620.13007	JUAR	620.13007	VYDDOT	0.30503711E-1	AZP	-32.215273
ZMR	-19305.919	TUAR	19302.420	VZDDOT	-0.35945342E-1	VXP	253.39004
LMR	-10066.444	LAARM	-4068.4799	PUOT	0.15224445E-1	VYP	21.320423
NMR	118.07903	MBARM	-20179.105	ODOT	-0.98799490E-2	VZP	6.6432341
NMR	50311.195	QBAR	51044.092	RUOT	0.19045071E-2	RSTR.	0.0
XMF	-1433.1357	XT	-10.558516	XTR	0.0	PSIDMG	0.0
YMF	-730.43218	YT	-347.39607	YTR	1724.0642	BTR	4.0
ZMF	-99.493226	ZT	931.25112	ZTR	-627.50926	MADD	0.0
LWF	1102.0711	LT	-737.65063	LTR	10531.791	XADD	0.0
MWF	-7505.0330	MT	20419.205	MTR	-19442.320	YADD	0.0
NWF	-6547.7305	NT	9696.4696	NTR	-53417.255	ZADD	0.0
XMT	-6.0348707	XVT	-11.724046	ALFMTT	-5.0890502	NRDU	0.0
YMT	-4.7094209	YVT	-342.60664	ALFVTT	4.0342614	LADU	0.0
ZMT	930.61405	ZVT	0.01629634	AAB01P	6.1244601		



**Run 29.**

32-AUG-77

1-21-17

UTIAS(510)

RELIGHT	199275	PSCB	30000000	V	1.0E-2	PSITR2	0.0
IX	6200.0	WLCB	240.24994	DELS	-5.0	VISTR.	0.0
IY	41707.0	WMO	0.23700000E-2	VSOUND	1117.0	VTSTR.	0.0
IZ	30200.0	TIME	0.20000000E-1	UELSMK	0.0	VZSTR.	0.0
ONEGTH	27.01494	MOSS	4.0	FASTMK	-10.0	PSTR.	0.0
ONEGTH	124.00000	MOSS	5.0	FASTMK	-10.0	WLV	273.0
KPM	13.0	PASGNT	1300.0	WCMT	230.0	PST	0.0
PSMT	700.00000	SMI	45.0	SVI	32.500000	QSTM.	0.0
LATSTK	-0.31372510	BIS	-1.1012031	IMT	20.000350	XA	0.030792
LANGSTK	3.0302004	BIS	2.0127131	IS	-5.0	XB	30.353035
CULSTK	10.001405	THESTAR	10.001405	TM75MK	0.0214550	XC	52.034100
PEUAL	10.330037	THELTM	20.330037	TM75MK	14.935704	XM	30.180319
RAIF	4.0030792	XGIN	3.0303835	XCIN	3.2030100	XPIN	1.0025259
XHALIF	45.000000	XHALTI	4.5092269	RSTM.	0.0	PSTR	0.0
VXB	0.10625000E-1	THESTAR	5.3063004	AAFP	4.1300530	QSTR	0.0
VVB	0.0	FMD	-2.7159400	YAAIP	-2.2111319	PSTM	0.0
VZB	0.13794100E-2	BEAMP	0.0	BBIP	-1.3107922	TITM	0.0
P	0.0	GAML	0.0	AAVL	-7.0930024	MITM	0.0
Q	0.7	OMGRAT	1.0	RAIL	-0.1353170E-1	JITM	0.0
ALPAP	-10.330001	PSIOUT	0.0	BBIL	0.10350057	MHITR	0.0
CMITTP	-0.10330001	PAIX	-0.025261120	EMPTX	0.79945395E-5	LMITM	0.0
ELM	0.0	PAIX	0.20475170	EMPTX	0.11099360E-3	OMITR	0.0
UAP	0.0	PSMT	0.00000000	SIGMT	0.0	XITR	0.0
MUX	0.0	ALMT	0.07171974	KUVT	0.04082013	VITM	0.0
MUTS	0.0	CMIS16	0.00101400E-1	LIOT	-13.0505004	ZITM	0.0
MUTS	0.0	CMIS16	-0.03111075E-2	LIOT	25.232740	LIOT	0.0
MUTS	0.0	CMIS16	0.00071053E-6	TIR	1314.4224	MITM	0.0
MUTS	0.0	CMIS16	0.000037635	MPKM	1926.0061	NITM	0.0
MUTS	0.0	VC	0.01212710E-3	KTR0LA	0.79544999	APX	3.0190747
MUTS	0.0	MHAM	-0.01005222	VADUOI	0.12030003E-1	ATP	1.5219619
MUTS	0.0	JBAM	330.21310	VADUOI	0.55403004E-2	APX	-31.993302
MUTS	0.0	JBAM	10004.005	PUOI	0.10650214E-3	VAP	0.10825000E-1
MUTS	0.0	LEAMH	-3525.5420	PUOI	-0.40695517E-3	VAP	0.0
MUTS	0.0	MBAMH	-0.01002304	QUOI	-0.40695517E-3	VAP	0.0
MUTS	0.0	MBAMH	3920.332	RUOI	-0.40695517E-3	VAP	0.0
MUTS	0.0	AT	4.2016272	XIR	0.0	PSTM.	0.0
MUTS	0.0	YI	-0.00740466E-6	VIM	1234.9436	PSIUMG	0.0
MUTS	0.0	ZI	5.9059734	ZIR	-451.50347	MAOU	0.0
MUTS	0.0	LI	-0.0100557204E-5	LIM	7574.4440	MAOU	0.0
MUTS	0.0	MI	172.93656	MIM	-13402.005	YAOU	0.0
MUTS	0.0	NI	0.13230122E-4	NIM	-30417.500	ZAOU	0.0
MUTS	0.0	XVT	-0.11051500E-6	ALPMTI	-10.0099024	MAOU	0.0
MUTS	0.0	VVT	-0.00740466E-6	ALPMTI	0.0	MAOU	0.0
MUTS	0.0	ZVT	0.006947293E-7	AAOUI	2.5704631	MAOU	0.0

UT143(S76) 1-21-77 30-AUG-77 MUN 21.

WEIGHT	19900.0	FSCG	350.20000	V	07.0	PSIR2	0.0
IX	6267.0	WLCG	246.29999	UCLS	-5.0	VXSR.	0.0
IY	41587.0	PHO	0.23700000E-2	VSDUND	1117.0	VYSR.	0.0
IZ	32224.0	TIME	0.20000000E-1	UCLSHK	0.0	VZSR.	0.0
OMENH	27.01999	NBS	4.0	T-SIMM	-18.0	PSM.	0.0
OMELTM	124.00000	NSS	5.4	T-SITM	-18.0	WVT	273.0
KPR	15.0	PASCNT	001.0	PLMT	230.0	FST	695.0
FST	100.00000	SMT	45.0	SVI	32.50000	USIR.	0.0
LAISTR	-1.1230699	AIS	-2.4207350	IMT	27.093837	XA	59.226930
LNOSTR	4.2000000	DIS	4.1282743	IS	-5.0	XB	34.953036
CULSTR	17.323106	THETAU	17.525126	TH7SMH	7.2051063	XC	42.781915
PEVAL	12.770070	THETTR	21.192404	TH7STM	7.6924045	XP	45.624647
XAIN	3.9226938	XBIN	3.4953236	XGIN	4.2781915	TPIN	2.4638868
XBALTP	41.355011	XBALTI	4.1559610	XSTH.	0.0	PSM	0.0
VXB	67.589759	THETAB	4.4929877	AAOF	4.0023362	OSTR	0.0
VVB	0.0	PHIB	-1.4441558	AAIF	-2.5977633	RSTM	0.0
VZB	5.2432611	BETAMF	0.0	BBIF	-0.10374639	TSTR	0.0
P	0.0	GAML	0.0	AAUL	-5.1521993	MITM	0.0
Q	0.0	UMGRAT	1.0	BBIL	0.2530888	JTR	0.0
H	0.0	PSIOUT	0.0	BBIL	0.13440699	MSTR	0.0
ALTRF	-15.814771	ERTX	1.1118810	ERHFX	0.76216400	LMTR	0.0
CHITPP	67.050770	ERTZ	2.0433416	ERHFX	1.3224024	QSTR	0.0
ERTN	0.0	EPSNT	0.40999999	SIGMT	0.0	XSTR	0.0
QAP	9.5312901	KWMT	6.07177979	KSVI	0.04052013	VSTR	0.0
MUIS	0.93205745E-1	CTSIG	0.02080912E-1	LTOT	-21.005250	ZSTR	0.0
MUS	0.0	CMSIG	-0.29463899E-2	DTOT	26.011485	LSTR	0.0
MUSZ	0.24201227E-2	CUMSIG	0.05278071E-6	TTR	958.71363	MSTR	0.0
LARDHM	-0.33000132E-1	NZ	0.12208342	MPHM	1401.4072	NSTR	0.0
ORSHMH	1074.6742	MOAN	-603.06110	KIMBLK	1.0	ASP	2.5063854
XMM	-432.77039	JBAM	432.77039	VABUOT	-0.12867916E-1	AYP	0.77569170
YMM	-10703.550	IBAM	14046.911	VZBUOT	0.33855262E-2	AZP	-32.050400
LMM	-3004.3799	LBAMH	-1414.2902	PDUOT	-0.00452913E-3	VXP	67.389759
MMH	14375.002	HOAMH	-6936.0676	QUOT	-0.72125019E-5	VZP	5.2932611
NMM	27040.014	UPAM	20920.054	RDUOT	-0.21501300E-3	PSM.	0.0
XMP	-1470.4533	XT	7.2214542	XIM	0.0	PSIMG	0.0
YMP	0.0	YT	-7.5008240	YTR	922.00311	STR	0.0
ZMP	201.00045	ZI	31.138914	ZTR	-327.92439	MAUD	0.0
LMP	0.0	LI	-16.000603	LTH	5503.7159	XAUD	0.0
MPF	-5112.6470	MI	695.10576	MTH	-10160.190	YAUD	0.0
NMP	0.0	NI	211.67201	NTH	-27910.040	ZADD	0.0
XMT	9.02170101	XVI	-1.9961550	ALPMT	-0.01411409	NAUD	0.0
YMT	0.0	YVI	-7.5008240	ALPMT	-0.01411409	NAUD	0.0
ZMT	30.00045	ZVI	1.0432174	AAUDIF	2.5002536	LADD	0.0



UNITAS (S/P)

1-21-77

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MUN 25.

WEIGHT	1972P.0	FSCG	360.20000	V	80.0	PSIK2	2.0
IX	6260.0	ALCG	246.29999	DEL5	-5.0	VSTR.	0.0
IY	81587.0	RHO	4.23780700E-2	V SOUND	1117.0	VSTR.	0.0
IZ	36224.0	TIME	0.20000000E-1	NELSHM	0.0	VSTR.	0.0
ONEGMP	27.019499	ADSS	0.0	TWSTIM	-18.0	PSTR.	0.0
ONEGTH	124.72300	ADSS	0.0	TWSTIM	-18.0	MLVT	273.0
KPR	13.0	PASGNT	1259.8	RLMT	234.0	FST	695.0
FST	700.42100	SMT	45.0	SVT	32.30000	QSTR.	0.0
LATSTK	0.09313247	ALS	-1.5054155	IMT	0.59350695	XA	44.417797
LNGSTK	0.0504050	ALS	0.1433457	IS	-3.0	XB	21.602806
COLSTK	16.012650	THETA0	16.012450	TH75MR	6.7324506	XC	39.379067
PEUAL	11.417620	THETA1	19.016039	TH75TK	5.5160395	XP	49.951045
XAIN	0.0417796	XBIN	2.1022805	XCIN	3.3579067	XPIN	2.6972863
XBALTY	25.050865	YBALTY	2.5630863	RSIM.	0.0	PSIK	0.0
VXM	134.60540	THETA0	5.3378350	AA0P	3.9493453	QSTR	0.0
VY0	12.670450	PHI0	0.0	AA1P	-5.1264332	RSTR	0.0
VZ0	12.577159	HEIAWF	4.6942014	BB1P	0.01200165E-1	TSTR	0.0
P	0.0	GANC	0.0	AA0L	-4.2899400	HTM	0.0
K	0.0	OMGRAT	1.0	BA1L	0.30030820	JSTR	0.0
ALPAP	0.44007700	PSI001	0.0	BA1L	0.35520411	MMSTR	0.0
CHITPP	81.447440	EXTX	1.4073010	CKMPX	0.91001679	LMSTR	0.0
ERTK	0.0	ERTZ	1.6000376	CKMP2	1.0008525	OMSTR	0.0
DMF	25.403003	EPSMT	0.49694201	YIGMT	0.02617400	XITM	0.0
MUXS	0.10631500	KUMT	0.67177979	KUVT	0.02610313	YITM	0.0
MUYS	0.10601050E-1	CISIG	0.02109790E-1	LTOT	2.3915002	ZITM	0.0
MUZS	0.070566724E-2	CHSIG	-0.59776573E-2	UTOT	24.510000	LITM	0.0
LAMMM	-0.11163602E-1	CHNSIG	0.65030592E-0	TIR	0.0017009	MITM	0.0
DASHMR	0.19749755E-1	NZ	0.94578244	MPMM	1162.6345	NITM	0.0
XIN	2303.0555	VC	-0.71325573E-5	KIRBLK	1.0	AXP	2.9002978
YMR	-519.59965	MBAM	-1507.0166	VX0001	-0.49460132E-2	AYP	0.21466639E-2
ZMR	-10470.570	JBAR	319.59960	VY0001	0.01907520E-4	AZP	-32.030120
LMM	-4954.5729	TDAM	14070.784	VZ0001	-0.57830071E-2	VXP	134.60540
MM	3150.3120	LEAMH	-1010.5172	PUOT	0.45116379E-3	VYP	12.078950
NMM	23000.315	MBAMH	-13492.761	QUOT	-0.37894720E-5	VZP	12.577139
YMP	-611.57015	QBAP	23603.767	RUOT	-0.51093098E-3	PSIMG	0.0
ZMP	-510.07200	XI	1.2539170	XIR	0.0	BTM	0.0
LMP	505.12475	YI	-142213050	YTR	700.10919	MADU	0.0
NMP	-2462.5270	ZI	502.93865	ZTR	-203.45000	XADD	0.0
XMI	5.1311051	LI	-318.20750	LTM	4765.0144	YADD	0.0
ZMI	302.61355	MT	8002.0505	MIR	-0797.9925	ZADD	0.0
		NT	3966.2674	NTH	-24172.239		
		XVT	-3.0771601	ALFMTI	-4.2022194		
		YVT	-140024907	ALFVTI	5.1038417		
		ZVT	0.52530441	AA001P	5.1270763		

MUN 24.

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UTIAS(S/N)

WEIGHT	179.27.0	150.0	100.0	PSIR2	0.0
IX	6800.0	246.2999	DEL5	VSIR2	0.0
IX	1500.0	0.2370000E-2	VSOUND	VSIR2	0.0
IX	3000.0	0.2000000E-1	VSOUND	VSIR2	0.0
UMCUM	27.01999	0.0	VSIR2	VSIR2	0.0
UMCUM	124.0000	0.0	VSIR2	VSIR2	0.0
KFR	15.0	500.0	VSIR2	VSIR2	0.0
FMT	700.0000	500.0	VSIR2	VSIR2	0.0
LATSTK	0.0000000	0.0	VSIR2	VSIR2	0.0
LOCSTK	0.0000000	0.0	VSIR2	VSIR2	0.0
CULSTK	17.00000	0.0	VSIR2	VSIR2	0.0
PEUL	10.00000	0.0	VSIR2	VSIR2	0.0
XAIN	4.000000	0.0	VSIR2	VSIR2	0.0
XBAL	20.00000	0.0	VSIR2	VSIR2	0.0
VXB	10.00000	0.0	VSIR2	VSIR2	0.0
VVB	11.00000	0.0	VSIR2	VSIR2	0.0
VZB	13.00000	0.0	VSIR2	VSIR2	0.0
P	0.0	0.0	VSIR2	VSIR2	0.0
R	0.0	0.0	VSIR2	VSIR2	0.0
ALP	0.000000	0.0	VSIR2	VSIR2	0.0
CHLIP	0.000000	0.0	VSIR2	VSIR2	0.0
ERK	0.0	0.0	VSIR2	VSIR2	0.0
OWP	0.000000	0.0	VSIR2	VSIR2	0.0
MUS	0.000000	0.0	VSIR2	VSIR2	0.0
MUS	0.000000	0.0	VSIR2	VSIR2	0.0
LAMOR	0.000000	0.0	VSIR2	VSIR2	0.0
OWM	0.000000	0.0	VSIR2	VSIR2	0.0
YK	2421.2217	0.0	VSIR2	VSIR2	0.0
YK	319.7174	0.0	VSIR2	VSIR2	0.0
ZK	1401.240	0.0	VSIR2	VSIR2	0.0
LK	2471.000	0.0	VSIR2	VSIR2	0.0
MM	1031.200	0.0	VSIR2	VSIR2	0.0
NK	2519.000	0.0	VSIR2	VSIR2	0.0
XK	310.0000	0.0	VSIR2	VSIR2	0.0
YK	300.0000	0.0	VSIR2	VSIR2	0.0
ZK	100.0000	0.0	VSIR2	VSIR2	0.0
WK	577.2500	0.0	VSIR2	VSIR2	0.0
MK	331.0000	0.0	VSIR2	VSIR2	0.0
NK	324.0000	0.0	VSIR2	VSIR2	0.0
XK	12.00000	0.0	VSIR2	VSIR2	0.0
YK	10.00000	0.0	VSIR2	VSIR2	0.0
ZK	10.00000	0.0	VSIR2	VSIR2	0.0

[illegible]



1-21-77 30-400-77 RUN 27.

UTLAS(S7A)

1-21-77

UTLAS(S7A)

WEIGHT	19400.0	FSCG	360.24000	V	150.0	PSIR2	0.0
IX	0.000.0	WLCG	246.29499	DELS	-5.0	VXSR.	0.0
IY	41587.0	RHO	0.23780200E-2	VSOUND	1117.0	VYSR.	0.0
IZ	56224.0	TIME	0.20002000E-1	DELSMR	0.0	VZSR.	0.0
ONEGR	27.014999	WSS	4.0	TASMR	-18.0	PSTR.	0.0
ONEGR	124.6200	NSS	5.0	TASMR	-18.0	MLVT	273.0
KFR	15.0	PASUNT	565.0	WHT	230.0	FST	695.0
FST	100.4000	SHI	45.0	SVT	32.500000	USTH.	0.0
LATSK	-1.7014538	AIS	-2.7680096	IHT	-5.6004066	XA	39.365913
LONGSK	13.00552	BIS	15.060911	S	-3.0	XB	1.2172113
CULSK	20.042670	THETA	20.042670	THSMR	10.762670	XC	64.766739
PEVAL	9.4193242	THETA	21.054542	THSMR	8.3543420	XP	55.490884
XAIN	3.9305913	XGIN	0.12172113	XGIN	6.4766739	XPIN	2.9964298
XBACIP	-0.00000002	XACTI	-0.00000002E-1	RSTH.	0.0	PSTR	0.0
VXH	253.09408	THETA	3.1010554	AAGP	4.0120304	QSTR	0.0
VYH	15.269734	PHIB	0.0	AALP	-8.0050206	RSTR	0.0
VZH	14.070379	RETA	3.3652540	RBIP	-0.48662349	TSTR	0.0
P	0.0	WMC	0.0	AACL	-8.0208362	HSTR	0.0
Q	0.0	OMGRAT	1.0	AIL	0.44932033	JSTR	0.0
K	0.0	PSIDOT	0.0	AIL	0.44932033	HMSTR	0.0
ALPMP	1.4507404	ERTX	1.5412333	ERAPX	2.84614260	LMSTR	0.0
CHLTPP	75.04333	ERT2	1.6497666	ERAP2	1.0103506	CMSTR	0.0
ERTM	0.0	ERT3	0.87365254	SGMT	0.59228487	XSTR	0.0
QW	60.532017	KMT	0.07177979	KGT	0.03231504	VSTR	0.0
MUX5	0.34962809	CTSIG	0.83352803E-1	LTOT	4.9574282	ZSTR	0.0
MUX5	0.21096244E-1	CHSIG	-0.09056100E-2	DTOT	24.688271	LSTR	0.0
MUX5	0.11799594E-2	CHSIG	0.64031969E-6	TTR	1615.1310	MSTR	0.0
LAMBMR	-0.44453757E-2	KZ	0.99893649	HPMR	2171.7298	NSTR	0.0
DMSHMR	0.16203716E-1	VL	0.71525573E-5	KIRBLK	1.0	AXP	1.7512933
XMR	507.07172	MBAR	-2066.3996	VXBDOT	-0.25609034E-1	AYP	-0.10429550
YMR	-466.54304	JBAR	466.54304	VYBDOT	-0.49032113E-1	AZP	-32.140161
ZMR	-14257.047	TBAR	19307.066	VZBDOT	-0.17732964E-1	VXP	253.09068
LPM	-5770.8875	LBARM	-4679.6183	POOT	-0.28210962E-1	VYP	15.289736
MPM	-10452.703	MBARM	-23058.565	QUOT	0.46496791E-2	VZP	14.070379
NMR	43127.213	QBARM	44206.196	RUOT	0.11705980E-2	NSTR.	0.0
XMP	-1934.4008	XT	-94.634451	XTR	0.0	PSIDMG	0.0
YMP	-711.07796	YT	-368.90397	YTR	1517.8399	BTR	0.0
ZMP	-443.61108	ZT	1184.2084	ZTR	-552.44448	MAUD	0.0
LXF	1125.7017	LT	53502.126	LTR	9272.0273	XADD	0.0
MPF	-5749.3304	MT	19294.347	MTR	-17116.726	YADD	0.0
NMF	-6204.0001	NT	-26.766145	NTR	-47027.720	ZADD	0.0
XMF	-0.00000001	XV	-0.00000001	ALFMT	-5.7593207	NADD	0.0
YMF	-0.00000001	YV	-0.00000001	ALFTT	3.434392	CAUD	0.0
ZMF	1104.1342	ZV	0.74287055E-1	ACDIP	8.8762639		



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UTIAS(970)

10-21-77

UTIAS(970)

WEIGHT	1920.0	PSCG	300.20000	V	1.00E+2	PSIAR	0.0
IX	6260.0	ALCG	246.29999	DELS	-5.0	VXIR.	0.0
IY	41501.0	RHO	0.1750000E-2	V SOUND	1077.0	VYIR.	0.0
IZ	30224.0	TIME	0.2000000E-1	DEL3MR	0.0	VZIR.	0.0
OMEGAR	27.01999	NOSS	4.0	TMSTR	-10.0	PSIR.	0.0
OMEGTR	124.00000	NSSS	5.0	TSIR	-10.0	MLVI	273.0
KFR	15.0	PASCNT	1112.0	MLMT	230.0	PSVI	995.0
FSMT	700.40000	SM	45.0	SVT	32.50000	QSTR.	0.0
LATSTR	-0.25335010	AIS	-1.5975005	INT	33.29053	XA	40.40000
LONGTR	2.9533516	BIS	1.5097903	IS	-3.0	X0	39.560120
COLSTR	21.179510	THETAB	21.179510	TH75MR	11.099510	XC	66.871990
PEDAL	21.402943	THETTR	34.242365	TH75TR	20.742365	XP	22.269520
XAIN	4.002006	XBIN	3.9564120	XCIR	6.5071909	XPIN	1.2025222
XOACTP	46.532057	XOACTI	4.6332057	PSIR.	0.0	PSIR	0.0
VIB	0.16036470E-1	THETAB	4.9177009	AAOF	4.3210444	QSTR	0.0
VIB	0.0	PHIO	-3.0202926	AAIF	-1.7407551	RSTR	0.0
VIB	0.14006977E-2	BETAMP	0.0	BBIF	-1.4489151	TSTR	0.0
P	0.0	GAMC	0.0	AAEL	-0.1515352	MITR	0.0
Q	0.0	OMGRAT	1.0	AAEL	-0.3168700E-1	JSTR	0.0
R	0.0	PSIDOT	0.0	BBIL	0.16550319	MMTR	0.0
ALPH	-13.192597	EKTX	-0.20396905	EKMPX	0.7995395E-3	LMTR	0.0
CHITTP	-1.7107535	EKTX	0.24629059	EKMPZ	0.11099360E-3	CMTR	0.0
EKTR	0.0	EPSMT	0.4499999	SIGMT	0.0	XSTR	0.0
QMF	0.27410154E-6	KQMT	0.07177979	KQVT	0.04052013	VSTR	0.0
MUX3	0.23295309E-4	CTSIG	0.18057778	CTOT	-20.002235	ZSTR	0.0
MUX3	0.2	CHSIG	-0.39705213E-2	DTOT	26.002217	LSTR	0.0
MUX3	0.7002050E-6	CHSIG	0.94317270E-6	TTR	1911.0063	MITR	0.0
LAMSTR	-0.60203924E-1	NZ	0.99401136	MPMR	2200.0252	NSTR	0.0
DMSTR	0.60204703E-1	VC	0.12701202E-3	KTRBLK	0.79599999	AXP	2.7039350
XMR	1607.5065	HDAR	-677.99109	VXDUOT	0.26265116E-1	AYP	1.7131147
YMR	-403.23119	JBAR	0.03.23119	VXDUOT	0.26265116E-1	AZP	-32.000749
ZMR	-10470.001	TBAR	10540.332	VZDUOT	-0.10057403E-2	VXP	0.16036470E-1
LMR	-0674.4494	LBARM	-3921.2577	POOT	0.99200373E-4	VYP	0.0
MMR	15046.545	MBARM	-4022.0445	QUOT	0.10910559E-3	VZP	0.14006977E-2
NMR	40009.009	GBAR	40945.001	ADOT	0.35000000E-3	RSTR.	0.0
YMP	-0.50075121E-5	XT	4.5320712	XTR	0.0	PSIDMG	0.0
ZMP	0.7170045E-5	ZT	5.0760797	YTR	1019.9870	BTR	4.0
MPF	0.0	LT	-0.77600327E-6	LTR	0074.2750	XADD	0.0
NMF	-0.14340742E-3	MT	171.23305	MTR	-10013.240	YADD	0.0
NMF	0.0	NT	2.97300013E-5	NTR	-43999.932	ZADD	0.0
XMT	4.5320713	XVT	-0.79060504E-7	ALFMTT	-7.6754474	MADD	0.0
YMT	0.0	YVT	-0.34903917E-6	ALPVT	0.0	LADD	0.0
ZMT	5.0760797	ZVT	0.60644250E-7	AA0BIF	2.20400504		

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WEIGHT	19900.0	PSCG	360.20000	V	40.0	PSITR2	0.0
IX	6200.0	MLCG	246.29999	DELS	-5.0	VXSTR.	0.0
IY	41507.0	RMO	0.17500000E-2	V SOUND	1077.0	VYSTR.	0.0
IZ	30224.0	TIME	0.20000000E-1	DELSHR	0.0	VZSTR.	0.0
OMEGMR	27.019999	NBS8	4.0	TMSTHM	-10.0	PSTR.	0.0
OMEGTR	124.62000	NBS5	5.0	TMSTR	-10.0	PLVT	273.0
KPR	13.0	PASCMT	900.0	MLMT	234.0	P3VT	045.0
PSMT	700.40000	9MT	45.0	SVT	32.30000	QSTR.	0.0
LATSTK	-2.1110904	A18	-3.0744206	IMT	31.50010	XA	30.000647
LONGSTK	4.2005735	B18	4.4329725	IS	-3.0	XB	34.000229
COLSTK	19.024095	THETA0	19.024095	TM75MH	9.7400953	XC	50.005596
PEDAL	14.592477	THETAH	25.006352	TM75TH	12.306352	XP	41.149706
XAIN	3.0000047	X01N	3.0000029	XCIM	3.000590	XPIM	2.2220203
XBACTP	41.459425	X0ACTI	4.1459425	RSTR.	0.0	PSTM	0.0
VXB	67.307914	THETA0	4.5009364	AA0P	4.3220095	QSTR	0.0
VYB	0.0	PHI0	-1.0793969	AA1F	-2.2701907	RSTR	0.0
VZB	5.3143365	02TAMP	0.0	001P	-0.34030161	TITM	0.0
P	0.0	GAMC	0.0	AA0L	-6.2970210	MITM	0.0
R	0.0	PMGRAT	1.0	AA1L	0.20227094	JITR	0.0
ALPMF	-10.001514	PMIDOT	0.0	B01L	0.03421005E-1	MMITR	0.0
CHITPP	62.503007	ERTX	0.97010370	ERMPX	0.69254940	LMITR	0.0
EXTR	0.0	EXTZ	2.0270011	EKMPZ	1.0349923	GMITR	0.0
DMF	7.9519971	EPST	0.44999999	SIGMT	0.0	XITM	0.0
MUXS	0.93204727E-1	KQMT	0.93491045	KGVT	0.04052013	YITR	0.0
MUYS	0.0	CT816	0.11159621	LTOI	-31.003029	ZITR	0.0
MUZS	0.24552929E-2	CH816	-0.30550043E-2	DTOT	30.001272	LITR	0.0
LAMBMR	-0.43902022E-1	CH816	0.94352743E-6	TTR	1162.0247	MITR	0.0
DW8MR	0.46357315E-1	NZ	0.99640052	MPHM	1706.5724	MITM	0.0
XMR	1020.6327	VC	0.10213562	KTRBLK	1.0	AXP	2.5326545
YMR	-245.09594	MBAR	-024.26542	VXBOOT	0.29740092E-2	AYP	0.91491704
ZMR	-10995.496	J0AR	545.09594	VYBOOT	-0.26200901E-1	AZP	-32.050373
LMR	-0650.2716	T0AR	19035.761	VZBOOT	0.52673799E-3	VXP	67.307914
MMR	15005.066	L0ARM	-1509.1654	PUOT	0.79995752E-3	VYP	0.0
NMR	33704.524	M0ARM	-6076.9490	QUOT	-0.20757559E-3	VZP	5.3143565
XMF	-150.67015	Q0AR	34737.701	RUOT	0.10929961E-3	RSTR.	0.0
YMF	0.0	XT	32.000064	XTR	0.0	PSIDMG	0.0
ZMF	300.20732	YI	-5.5032770	YTR	1092.7790	0TR	4.0
LMF	0.0	ZT	65.735507	ZTR	-397.73903	MADD	0.0
MMF	-5192.1344	LT	-12.422793	LTR	6675.4002	XADD	0.0
NMF	0.0	MT	1900.9407	MTR	-12323.305	YADD	0.0
XMT	33.004100	NT	155.77345	NTR	-33057.937	ZADD	0.0
YMT	0.0	XVT	-1.3902956	ALFMTT	-1.9713439	NAUD	0.0
ZMT	64.010140	YVT	-5.5032770	ALFVTT	0.0	LADU	0.0
		ZVT	0.92536707	AA001P	2.3214005		

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RUN 59.

HEIGHT	1922.8	PSCG	368.23322	V	62.2	PSITR2	2.2
IX	6260.6	WLCG	246.29999	DELS	-5.2	VISTR.	2.2
IY	1587.8	RMO	2.1752222E-2	VSDUND	1277.8	VISTR.	2.2
IZ	30224.8	TIME	8.2222222E-1	DELSM	2.2	VISTR.	2.2
OMEHR	27.81999	NBS	4.2	TASTM	-10.2	PSITR.	2.2
OMEHR	124.62000	NBS	5.2	TASTM	-10.2	PSITR.	2.2
KPR	15.8	PASCNT	1553.8	WLMH	234.2	PSITR.	2.2
FSMT	708.42020	SMT	45.8	SVT	32.50200	PSITR.	2.2
LATSTR	-1.1170111	AIB	-1.9963146	IMT	23.267562	PSITR.	2.2
LNGSTR	4.9373501	BIB	5.0766767	IS	-3.2	PSITR.	2.2
COLSTR	10.999452	TMETAB	10.999452	TMTSM	8.9194520	PSITR.	2.2
PEVAL	13.753000	TMETH	23.976342	TMTSM	12.476342	PSITR.	2.2
XAIN	4.3886102	XBIN	3.2553524	XBIN	5.3245576	PSITR.	2.2
XBACTP	37.114212	XBACTI	3.7114212	XBIN	2.2	PSITR.	2.2
VIB	101.25935	TMETAB	2.9332953	AAEP	4.1689293	PSITR.	2.2
VIB	16.670724	PHIO	0.2	AAIF	-1.4526229	PSITR.	2.2
VIB	5.1007104	BEAMP	7.7441839	BBIF	-2.2443444E-1	PSITR.	2.2
P	0.2	GAMC	0.2	AAEL	-5.2321924	PSITR.	2.2
R	0.2	DMGRAT	1.2	AAIL	2.23417631	PSITR.	2.2
ALPAP	-8.7549214	PSIDOT	2.2	BBIL	-2.12539813E-1	PSITR.	2.2
CHITAP	75.432079	EXTX	1.2497272	BBIL	2.64975206	PSITR.	2.2
EXTR	0.2	EXTZ	1.9255045	EXMPX	1.8145679	PSITR.	2.2
QMP	13.408374	EPST	0.52744183	EXMPZ	1.2222200	PSITR.	2.2
MUXS	0.1308200	KGMT	0.07177979	SGAT	2.76237277	PSITR.	2.2
MUXS	0.22995796E-1	CTSIG	0.11011818	LGOT	2.4598218	PSITR.	2.2
MUXS	-8.10297539E-3	CHSIG	-8.21122924E-2	DTOT	27.337912	PSITR.	2.2
LAMBHR	-8.32586347E-1	CHSIG	0.9899888E-6	TTR	936.73672	PSITR.	2.2
DMSHR	8.32425371E-1	NZ	0.9899888E-6	MPMR	1372.6902	PSITR.	2.2
IMR	1344.2279	VC	0.35762786E-5	KTRDLK	1.2	PSITR.	2.2
YMR	-505.48529	MBAR	-368.68732	VBDOT	-2.44624523E-2	PSITR.	2.2
ZMR	-18757.271	JBAR	505.48529	VBDOT	-2.44624523E-2	PSITR.	2.2
LHR	-5737.8062	TBAR	18003.377	VBDOT	-2.44624523E-2	PSITR.	2.2
MHR	18998.354	LBARM	-1261.9444	PDOT	2.15221422E-2	PSITR.	2.2
NHR	26908.184	MBARM	-3948.9629	CDOT	-2.44187189E-4	PSITR.	2.2
XMP	-311.31221	QBAR	27908.964	PDOT	-2.44187189E-4	PSITR.	2.2
YMP	-275.75058	XT	-58.815627	XTR	2.2	PSITR.	2.2
ZMP	162.67463	YT	-95.430404	YTR	602.31282	PSITR.	2.2
LMP	573.31927	ZT	-145.81911	ZTR	-322.40726	PSITR.	2.2
MMP	-4065.8771	LT	-285.43988	LTD	537.5522	PSITR.	2.2
NMP	-2334.7992	MT	-4207.6632	MTR	-9927.2049	PSITR.	2.2
XMT	-63.153215	NT	2663.6319	NTR	-27274.930	PSITR.	2.2
YMT	-2.1289010	XVT	4.3375808	ALFMTT	3.5482947	PSITR.	2.2
ZMT	-144.26142	YVT	-93.311442	ALFMTT	12.035836	PSITR.	2.2
		ZVT	-1.5376059	AABP	1.4526206	PSITR.	2.2

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UTIAS(1976)

WEIGHT	19920.0	PSCO	300.28222	V	02.2	PSITR2	2.2
IX	6260.0	MLC6	246.29990	DEL8	-5.2	VISTR.	0.0
IY	41587.0	PHO	0.1752822E-2	VSDUD	1277.2	VISTR.	0.0
IZ	30224.0	TIME	2.2020282E-1	DEL5M	0.2	VISTR.	0.0
OMEGMR	27.21999	NBS3	4.2	TOSTM	-10.2	PSITR.	3.0
OMEGTH	124.62620	NBS3	5.0	TOSTM	-10.2	PLVT	273.2
KPR	15.0	PASCMT	1190.0	MLMT	234.2	PSIT	093.2
PSMT	722.22222	8MT	45.0	SVT	32.32222	PSITM.	2.2
LATSTK	-1.2338148	AIS	-1.9874250	IMT	11.231011	XA	43.543057
LNGSTK	6.2627498	BIS	0.9193602	IS	-3.2	XB	27.872144
COLSTK	10.969427	THETAB	10.969427	TM2MM	0.0994270	XC	53.850920
PEDAL	11.060372	THETTH	22.255604	TM2STH	0.5556040	XP	49.721562
XAIN	4.3563057	XBIN	2.7072144	XCIN	5.3259919	XPIV	2.0290159
XOACTP	31.200071	XOACTI	3.1606271	ASIM.	0.2	PSIT	2.2
VXB	134.97011	THETAB	3.2209099	ASIP	4.1237046	PSITM	2.2
VYS	14.040855	PHIB	0.2	ASIF	-2.0435116	PSITM	0.2
VZB	7.6105747	DETAMP	5.2933397	OSIP	2.93127041E-1	YITM	0.2
P	0.2	GAMC	0.2	ASCL	-4.7915974	MITM	0.2
Q	0.2	OMGRAT	1.0	ASIL	2.2020295	JITR	0.2
R	0.2	PSIDOT	0.2	BSIL	2.00913994E-1	MMITR	0.2
ALFMP	-4.2302703	EXTX	1.3921097	EMEX	0.9210422	LMITR	0.2
CHITPP	82.141095	EXTZ	1.0047230	EMRZ	1.2290503	OMITR	0.2
EXTM	0.2	EPST	0.50293339	SIGT	0.91637412	XITR	0.2
QMF	28.306020	K2MT	0.87177979	KCVT	2.01819298	YITM	0.2
MUX3	0.10606744	CT816	0.11034024	LTOT	-1.7070262	ZITR	0.2
MUX3	0.19300330E-1	C4316	-0.34019237E-2	DTOT	24.756023	LITR	0.2
MUX3	0.73090330E-3	COM816	0.90211595E-6	YTR	929.93546	MITR	0.2
LAMBHR	-0.24252223E-1	NZ	0.99046366	MMHM	1325.3904	MITM	0.2
OMSHMR	0.24991104E-1	VC	0.0	K10BLK	1.0	ARP	1.0121001
XMR	1566.1062	MEAM	-502.92024	VSDUT	-2.17459512E-2	AVP	-2.04050562E-2
YMR	-459.42177	JBAR	459.42177	VSDUT	-2.59045469E-2	AZP	-32.126245
ZMR	-10703.610	TBAR	10641.296	VSDUT	-2.30497142E-2	VAP	134.97611
LWR	-5470.7069	LBARM	-1349.1199	PDUT	-2.25620308E-2	VAP	14.040855
MWR	15266.029	MBARM	-6591.0720	GDUT	-2.24476364E-3	VAP	7.6105747
MWR	25003.032	OBAR	20551.249	RDUT	-2.25762740E-3	ASTM.	0.0
XMF	-474.97709	XT	-17.677112	XTR	0.2	PSIDMG	0.2
YMF	-201.03292	YT	-117.37152	YTR	055.12321	STR	4.0
ZMF	69.922106	ZT	-33.743096	ZTR	-311.24200	MADD	0.2
LWF	490.08909	LT	-257.01745	LTR	5223.6917	XADD	0.0
MWF	-4464.2205	MT	-969.32766	MTR	-9603.2525	VADD	0.2
NWF	-2491.3348	NT	3275.1273	NTR	-26494.567	ZADD	0.0
XMT	-15.902419	XVT	-1.7146923	ALFMTT	0.61077900	MADD	0.2
YMT	-1.0250091	YVT	-116.34562	ALFVTT	6.1305936	MADD	0.0
ZMT	-34.059252	ZVT	0.31535472	ABBLF	2.4452932	LADD	0.0

UTTAB (876)

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RUN 01.

HEIGHT	19988.2	PSG	308.2222	Y	122.3	PSITP2	2.2
IX	6260.8	-LCC	206.2999	DEL8	-2.2	VSIR	2.2
IY	41507.8	RMC	8.17882222-2	VSOUND	1277.8	VSIR	2.2
IZ	30224.0	TIME	8.20222222-1	DEL3M	2.2	VSIR	2.2
CMGMR	27.01999	NR8	4.8	VSIR	-10.2	VSIR	2.2
CMGTR	124.6222	NR8	5.2	VSIR	-10.2	VSIR	2.2
KPR	13.8	PARCMT	1175.2	VSIR	234.8	VSIR	2.2
PSMT	728.4222	BT	45.8	VSIR	32.2222	VSIR	2.2
LATSTR	-1.1181328	A18	-2.0364713	VSIR	2.118075	VSIR	2.2
LGSTR	0.5963733	B18	9.6528767	VSIR	-3.8	VSIR	2.2
COLSTR	19.473597	THETAB	19.473597	VSIR	9.5335972	VSIR	2.2
PEUAL	18.959439	THETR	21.751756	VSIR	0.2517561	VSIR	2.2
XAIN	8.3861681	TRIN	1.9624122	VSIR	5.6229982	VSIR	2.2
XACTP	21.604106	XACT1	2.1604106	VSIR	8.2	VSIR	2.2
YB	160.5907	THETAB	4.2871815	VSIR	4.1174163	VSIR	2.2
YB	13.67693	PHIB	8.8	VSIR	-4.2822531	VSIR	2.2
YB	11.811597	SETAM	4.2915112	VSIR	2.1182172	VSIR	2.2
P	2.2	GMC	8.2	VSIR	-5.2224278	VSIR	2.2
Q	8.2	CMGRAT	1.2	VSIR	2.30234792	VSIR	2.2
ALPAP	-8.98473457	PSIDOT	8.2	VSIR	2.21642114	VSIR	2.2
CMITPP	0.938497	EXTR	1.3312193	VSIR	0.92522845	VSIR	2.2
EXTR	8.2	EXTR	1.7813254	VSIR	1.282614	VSIR	2.2
EXTR	29.228364	EXTR	8.49291512	VSIR	2.75352596	VSIR	2.2
EXTR	8.23328292	EXTR	8.1127992	VSIR	2.8282827	VSIR	2.2
EXTR	8.108657982-1	EXTR	8.1127992	VSIR	1.929228	VSIR	2.2
EXTR	8.48921372-2	EXTR	-8.614986292-2	VSIR	24.438382	VSIR	2.2
EXTR	-8.161876312-1	EXTR	8.490725982-6	VSIR	1225.0432	VSIR	2.2
EXTR	8.26295842-1	EXTR	8.99780522	VSIR	1415.3857	VSIR	2.2
EXTR	2241.1282	EXTR	8.71253735-5	VSIR	1.2	VSIR	2.2
EXTR	-8.05.02426	EXTR	-1849.9914	VSIR	8.182565932-1	VSIR	2.2
EXTR	-18085.179	EXTR	495.82426	VSIR	-2.31932822-2	VSIR	2.2
EXTR	-5958.2469	EXTR	1067.597	VSIR	8.173765922-1	VSIR	2.2
EXTR	7926.4675	EXTR	-1072.4788	VSIR	2.512961692-3	VSIR	2.2
EXTR	27918.784	EXTR	-11264.525	VSIR	2.981791722-3	VSIR	2.2
EXTR	-692.11721	EXTR	28828.362	VSIR	-2.311522222-3	VSIR	2.2
EXTR	-328.54356	EXTR	-4.2178311	VSIR	8.2	VSIR	2.2
EXTR	-34.814433	EXTR	-158.71235	VSIR	943.18813	VSIR	2.2
EXTR	531.13481	EXTR	238.92318	VSIR	-345.29234	VSIR	2.2
EXTR	-3809.9158	EXTR	-338.35132	VSIR	5761.8417	VSIR	2.2
EXTR	-2714.8.37	EXTR	6568.6182	VSIR	-12616.348	VSIR	2.2
EXTR	1.4734865	EXTR	4285.5646	VSIR	-2923.258	VSIR	2.2
EXTR	-1.5334375	EXTR	-5.4924377	VSIR	-2.9165212	VSIR	2.2
EXTR	238.42227	EXTR	-189.17091	VSIR	4.8779831	VSIR	2.2
EXTR		EXTR	8.52891392	VSIR	4.8915759	VSIR	2.2

UTTA9(1976) 1-21-77 30-AUG-77 RUN 62.

HEIGHT	1900.0	PSCG	300.20000	Y	122.0	PSTTR2	2.2
IX	6266.0	ALCG	246.29999	DEL3	-5.0	VSTTR.	2.2
IY	41507.0	RWD	0.17500000E-2	VROUND	1077.0	VSTTR.	2.2
IZ	30220.0	TIME	0.20000000E-1	DEL3MR	2.0	VSTTR.	2.2
OMEGFR	27.01999	NBS3	4.0	TWSTMR	-10.0	VSTTR.	2.2
OMEGTR	124.00000	NSS3	5.0	TWSTTR	-10.0	LVLT	273.0
KFR	15.0	PASCNT	1217.0	PLMT	230.0	PSTTR	095.0
FSMT	700.00000	3MT	45.0	3VT	32.30000	3TR.	2.2
LAT3TK	-1.300175	A13	-2.4150013	IMT	0.02705904	XA	41.500705
LGSTK	9.600124	B18	11.002034	IS	-5.0	XB	15.750045
COLSTK	20.093240	TMETAB	20.093240	TW5MM	10.013200	XC	02.500750
PEOAL	10.961510	TMETTH	22.977350	TW5TH	9.477301	XP	51.215595
XAIN	0.130705	XBIM	1.5750005	XCIM	0.2500750	XPIM	2.7055702
FBACTP	15.007390	XBACTI	1.5007309	RSTH.	2.0	PSTH	2.2
VIB	202.50000	TMETAB	2.7003003	AA0P	4.2003371	3STH	2.2
VTD	14.10720	PMIB	0.0	AA1P	-4.0715023	PSTH	2.2
VZB	9.0050300	BETAMP	3.7017001	BB1P	0.93369970E-1	TTH	2.2
P	0.0	GAMC	0.0	AA2L	-0.5910177	MTM	2.2
R	0.0	OMGRAT	1.0	AA1L	0.01004190	3TH	2.2
ALPMP	0.060000257	PSIDOT	0.0	BB1L	2.20209100	MTM	2.2
CHITPP	02.250050	EKTX	1.30000059	CKMPX	0.92933133	LMTM	2.2
EKTR	0.0	EP3MT	0.00701700	CKMPZ	1.02077437	2-MTR	2.2
GMP	40.233050	KGMT	0.07177979	Q1GMT	0.66557421	X1TR	2.2
MU3	0.27970301	CT310	0.11112723	AVT	2.03052972	V1TR	2.2
MU5	0.19510501E-1	CM310	-0.53930105E-2	LTOT	1.7100007	21TR	2.0
MU3	-0.10330017E-2	CM310	0.04003249E-6	DTOT	2.0336339	L1TR	2.2
LAMBMR	-0.17901310E-1	NZ	0.99007000	YTR	1.230.2972	MTM	2.2
OM3MR	0.16927050E-1	VC	0.71525573E-5	PMH	1730.5300	MTM	2.2
XMR	1912.0374	MCAP	-920.09073	MTBMR	1.0	ASP	1.5010070
YMR	-509.00059	JCAR	509.00059	VXDUOT	0.22600470E-1	AVP	-2.01027552E-2
ZMR	-1000.0000	TBAR	10975.000	VYDUOT	0.07739070E-5	AZP	-32.105350
LWR	-7317.0050	LDARM	-2000.0013	VZDUOT	0.21726290E-1	VAP	222.50562
MWR	0021.1002	MBARM	-10961.004	PDOT	0.63103010E-3	VTP	14.104726
NWR	30247.004	2BAR	35347.750	CDOT	0.25370410E-2	VLP	9.0050300
MP	-955.07042	XT	-15.010320	PDOT	0.24517190E-2	PSTH.	2.2
YMP	-390.59021	YT	-193.30005	YTR	2.0	P310MG	2.2
ZMP	-57.00030	ZT	329.30000	YTR	1101.0257	0TR	0.0
LMP	601.40127	LT	-026.30027	ZTR	-422.07002	MDO	2.2
MMP	-4970.1375	MT	9356.0009	LTP	7097.0059	XADU	0.0
NMP	-3534.2230	NT	5395.2002	MP	-13101.907	YADU	0.2
XMT	-4.2131005	XVT	-10.003375	MP	-35997.235	ZADU	2.2
YMT	-1.0000002	YVT	-191.50009	ALPMTT	-3.1245097	NADU	2.2
ZMT	320.00125	ZVT	0.70055207	ALPVT	4.0057215	LADU	2.0
				AA01P	4.02706320		

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UTTAB(876)

WEIGHT	1980.8	FSCG	V	140.0	PSIRZ	0.0
IX	6268.0	WLCG	DEL3	-5.0	VSTR.	0.0
IY	41587.0	RHO	VSUONO	1077.0	VSTR.	0.0
I2	30224.0	TIME	DEL3MR	0.0	VSTR.	0.0
OMEGRA	27.019999	N838	DEL3MR	-10.0	PLVT	273.0
OMEGTR	124.02200	N838	DEL3MR	-10.0	PLVT	273.0
KPR	15.0	PASCNT	DEL3MR	-10.0	PLVT	273.0
FSMT	700.00000	SMT	DEL3MR	-10.0	PLVT	273.0
LATSTK	-2.3040002	A18	DEL3MR	-10.0	PLVT	273.0
LNGSTK	11.3090004	B18	DEL3MR	-10.0	PLVT	273.0
COLSTK	22.003901	THETAB	DEL3MR	-10.0	PLVT	273.0
PEDAL	12.309947	THETTR	DEL3MR	-10.0	PLVT	273.0
IAIN	3.5300998	XOIN	DEL3MR	-10.0	PLVT	273.0
XBACTF	7.9204269	XOIN	DEL3MR	-10.0	PLVT	273.0
VXB	236.52902	XOIN	DEL3MR	-10.0	PLVT	273.0
VYB	16.027500	PHID	DEL3MR	-10.0	PLVT	273.0
VZB	4.6517224	PHID	DEL3MR	-10.0	PLVT	273.0
P	0.0	GAMC	DEL3MR	-10.0	PLVT	273.0
Q	0.0	OMGRAT	DEL3MR	-10.0	PLVT	273.0
R	0.0	PSIUOT	DEL3MR	-10.0	PLVT	273.0
ALPMP	-1.3009031	EKTX	DEL3MR	-10.0	PLVT	273.0
CHITPP	01.794446	EKTX	DEL3MR	-10.0	PLVT	273.0
EKTR	0.0	EP8MT	DEL3MR	-10.0	PLVT	273.0
QMP	53.330045	KOHT	DEL3MR	-10.0	PLVT	273.0
MUXS	0.32013428	CTSIG	DEL3MR	-10.0	PLVT	273.0
MUTS	0.22000401E-1	CHSIG	DEL3MR	-10.0	PLVT	273.0
MUZS	-0.10007037E-1	CHSIG	DEL3MR	-10.0	PLVT	273.0
LAMBHR	-0.25225756E-1	NZ	DEL3MR	-10.0	PLVT	273.0
DMBHR	0.1457910E-1	VC	DEL3MR	-10.0	PLVT	273.0
XMR	1657.1061	H0AR	DEL3MR	-10.0	PLVT	273.0
YMR	-055.09859	JBAR	DEL3MR	-10.0	PLVT	273.0
ZMR	-10970.019	TBAR	DEL3MR	-10.0	PLVT	273.0
LMR	-10300.103	LBARM	DEL3MR	-10.0	PLVT	273.0
MHR	11302.333	H0ARM	DEL3MR	-10.0	PLVT	273.0
NMR	49150.030	OBAR	DEL3MR	-10.0	PLVT	273.0
XMP	-1260.4914	XT	DEL3MR	-10.0	PLVT	273.0
YMP	-532.00071	YT	DEL3MR	-10.0	PLVT	273.0
ZMP	-15.010007	ZT	DEL3MR	-10.0	PLVT	273.0
LMP	077.33373	LT	DEL3MR	-10.0	PLVT	273.0
NMP	-7733.3000	MT	DEL3MR	-10.0	PLVT	273.0
NMT	-4729.8422	NT	DEL3MR	-10.0	PLVT	273.0
XMT	0.27100093	XVT	DEL3MR	-10.0	PLVT	273.0
YMT	-2.5010172	YVT	DEL3MR	-10.0	PLVT	273.0
ZMT	534.20471	ZVT	DEL3MR	-10.0	PLVT	273.0

UTIAS(376) 1-21-77 38-AUG-77 RUN 64.

WEIGHT	19900.0	PSCG	300.20000	V	150.0	PSTIM2	0.0
IX	6260.0	WLCG	246.29999	DELS	-5.0	VXSTR.	0.0
IY	41507.0	RMD	0.17500000E-2	VROUND	1077.0	VYSTR.	0.0
IZ	30224.0	TIME	0.20000000E-1	DELJMR	0.0	VZSTR.	0.0
OMEGMR	27.01999	NSS	4.0	TH31MR	-10.0	PSTR.	0.0
OMEGTR	124.62000	NSB	5.0	TH31TH	-10.0	WLVT	273.0
KFR	15.0	PASLMT	1703.0	WLMT	234.0	P3VT	093.0
PSMT	700.40000	SMT	45.0	SVT	32.30000	QSTR.	0.0
LATSTK	-2.2501305	AIS	-0.0457941	IMT	0.40409004	XA	29.001040
LNGSTK	12.37227	BIS	14.034737	IS	-3.0	XB	6.2010747
COLSTK	23.991239	THETAB	23.991239	TH75MM	13.911239	XC	04.405243
PEDAL	13.402227	THETTR	29.095714	TH75TH	16.195714	XP	44.227570
XAIN	2.9001000	XBIN	0.02010797	XCIN	0.40405243	XPIN	2.3002271
XOACTP	3.1116508	XOACTI	0.31116500	RSTR.	0.0	PSTR	0.0
VXB	253.49279	THETAB	-0.10007309	AAP	4.0499009	QSTR	0.0
VYB	10.527200	PHIO	0.0	AAIP	-3.4747201	RSTR	0.0
VZB	-0.47191204	DELAMP	4.0320177	BBIP	-0.20435743	TITR	0.0
P	0.0	GAMC	0.0	ABIP	-11.613063	MITR	0.0
R	0.0	OMGRAT	1.0	AAIL	0.00545010	JITR	0.0
ALFHF	-2.2750312	PSIDOT	0.0	BBIL	0.10719403	MMITR	0.0
CHITPP	01.100913	ERTX	1.3611159	EMFX	0.31545500	LMITR	0.0
ENTR	0.0	ERTZ	1.7420750	EMFZ	1.0000110	QMITR	0.0
QPF	0.0	EPMT	0.49032017	SICMT	0.70963513	XITR	0.0
MUX3	0.34913054	KOMT	0.07177979	KOVT	0.02930323	VITR	0.0
MUZ3	0.25550041E-1	CT916	0.11210004	L10T	-0.11021440	ZITR	0.0
LAMBMR	-0.10940031E-1	CH916	-0.22067932E-2	DTOT	24.386403	LITR	0.0
DMSHMR	0.13650000E-1	CM916	0.00390905E-6	TTR	2203.1753	MITR	0.0
YMR	1592.4000	NZ	1.0014097	MPHM	3111.4443	NITR	0.0
ZMR	-1096.0567	VC	0.44703403E-6	KTABLK	1.0	AXP	-0.66102769E-1
LMR	-12966.237	MBAR	-390.40443	VBDUOT	-0.21247699E-1	AYP	0.51950719E-1
MMR	15936.775	TBAR	19156.615	VBDUOT	0.135027130E-1	AZP	-32.230250
NMR	01270.410	LBARM	-3114.3240	VBDUOT	-0.46273110E-1	VXP	253.49279
YMP	-041.36970	MBARM	-9294.2006	QDOT	0.14509205E-1	VYP	10.527200
ZMP	64.434434	DBAR	63334.360	ROOT	-0.92496052E-2	VZP	-0.47191204
LWF	1003.9990	XT	-2.9063543	XTR	0.0	RSTR.	0.0
MWF	-10374.003	YT	-311.09039	YTR	2070.4615	P810MG	0.0
NWF	-5702.4020	ZT	602.60174	ZTR	-753.50703	BTR	4.0
XMT	12.920517	LT	-003.34276	LTR	12007.029	XADD	0.0
YMT	-3.2711310	MT	19401.907	MTR	-23340.662	YADD	0.0
ZMT	061.33000	NT	0703.4371	NTR	-64149.799	ZADD	0.0
		XVT	-15.034071	ALFMTT	-4.3625053	NADD	0.0
		YVT	-300.62125	ALFVTT	4.1053600	LADD	0.0
		ZVT	1.3429416	AAB01P	3.0007323		





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KUN 2.

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01105(510)

KLIGHT	10037.7	PSOB	300020000	1.2002	PSIM2	0.0
14	30000.0	ALG	251.10000	-3.0	VSIM	0.0
15	30000.0	MMO	2.23700000E-2	1117.0	VSIM	0.0
16	30000.0	TIME	0.20000000E-1	0.2	VSIM	0.0
17	30000.0	TIME	0.0	-10.0	PSIM	0.0
18	30000.0	TIME	0.0	-10.0	PSIM	0.0
19	30000.0	TIME	0.0	-10.0	PSIM	0.0
20	30000.0	TIME	0.0	-10.0	PSIM	0.0
21	30000.0	TIME	0.0	-10.0	PSIM	0.0
22	30000.0	TIME	0.0	-10.0	PSIM	0.0
23	30000.0	TIME	0.0	-10.0	PSIM	0.0
24	30000.0	TIME	0.0	-10.0	PSIM	0.0
25	30000.0	TIME	0.0	-10.0	PSIM	0.0
26	30000.0	TIME	0.0	-10.0	PSIM	0.0
27	30000.0	TIME	0.0	-10.0	PSIM	0.0
28	30000.0	TIME	0.0	-10.0	PSIM	0.0
29	30000.0	TIME	0.0	-10.0	PSIM	0.0
30	30000.0	TIME	0.0	-10.0	PSIM	0.0
31	30000.0	TIME	0.0	-10.0	PSIM	0.0
32	30000.0	TIME	0.0	-10.0	PSIM	0.0
33	30000.0	TIME	0.0	-10.0	PSIM	0.0
34	30000.0	TIME	0.0	-10.0	PSIM	0.0
35	30000.0	TIME	0.0	-10.0	PSIM	0.0
36	30000.0	TIME	0.0	-10.0	PSIM	0.0
37	30000.0	TIME	0.0	-10.0	PSIM	0.0
38	30000.0	TIME	0.0	-10.0	PSIM	0.0
39	30000.0	TIME	0.0	-10.0	PSIM	0.0
40	30000.0	TIME	0.0	-10.0	PSIM	0.0
41	30000.0	TIME	0.0	-10.0	PSIM	0.0
42	30000.0	TIME	0.0	-10.0	PSIM	0.0
43	30000.0	TIME	0.0	-10.0	PSIM	0.0
44	30000.0	TIME	0.0	-10.0	PSIM	0.0
45	30000.0	TIME	0.0	-10.0	PSIM	0.0
46	30000.0	TIME	0.0	-10.0	PSIM	0.0
47	30000.0	TIME	0.0	-10.0	PSIM	0.0
48	30000.0	TIME	0.0	-10.0	PSIM	0.0
49	30000.0	TIME	0.0	-10.0	PSIM	0.0
50	30000.0	TIME	0.0	-10.0	PSIM	0.0
51	30000.0	TIME	0.0	-10.0	PSIM	0.0
52	30000.0	TIME	0.0	-10.0	PSIM	0.0
53	30000.0	TIME	0.0	-10.0	PSIM	0.0
54	30000.0	TIME	0.0	-10.0	PSIM	0.0
55	30000.0	TIME	0.0	-10.0	PSIM	0.0
56	30000.0	TIME	0.0	-10.0	PSIM	0.0
57	30000.0	TIME	0.0	-10.0	PSIM	0.0
58	30000.0	TIME	0.0	-10.0	PSIM	0.0
59	30000.0	TIME	0.0	-10.0	PSIM	0.0
60	30000.0	TIME	0.0	-10.0	PSIM	0.0
61	30000.0	TIME	0.0	-10.0	PSIM	0.0
62	30000.0	TIME	0.0	-10.0	PSIM	0.0
63	30000.0	TIME	0.0	-10.0	PSIM	0.0
64	30000.0	TIME	0.0	-10.0	PSIM	0.0
65	30000.0	TIME	0.0	-10.0	PSIM	0.0
66	30000.0	TIME	0.0	-10.0	PSIM	0.0
67	30000.0	TIME	0.0	-10.0	PSIM	0.0
68	30000.0	TIME	0.0	-10.0	PSIM	0.0
69	30000.0	TIME	0.0	-10.0	PSIM	0.0
70	30000.0	TIME	0.0	-10.0	PSIM	0.0
71	30000.0	TIME	0.0	-10.0	PSIM	0.0
72	30000.0	TIME	0.0	-10.0	PSIM	0.0
73	30000.0	TIME	0.0	-10.0	PSIM	0.0
74	30000.0	TIME	0.0	-10.0	PSIM	0.0
75	30000.0	TIME	0.0	-10.0	PSIM	0.0
76	30000.0	TIME	0.0	-10.0	PSIM	0.0
77	30000.0	TIME	0.0	-10.0	PSIM	0.0
78	30000.0	TIME	0.0	-10.0	PSIM	0.0
79	30000.0	TIME	0.0	-10.0	PSIM	0.0
80	30000.0	TIME	0.0	-10.0	PSIM	0.0
81	30000.0	TIME	0.0	-10.0	PSIM	0.0
82	30000.0	TIME	0.0	-10.0	PSIM	0.0
83	30000.0	TIME	0.0	-10.0	PSIM	0.0
84	30000.0	TIME	0.0	-10.0	PSIM	0.0
85	30000.0	TIME	0.0	-10.0	PSIM	0.0
86	30000.0	TIME	0.0	-10.0	PSIM	0.0
87	30000.0	TIME	0.0	-10.0	PSIM	0.0
88	30000.0	TIME	0.0	-10.0	PSIM	0.0
89	30000.0	TIME	0.0	-10.0	PSIM	0.0
90	30000.0	TIME	0.0	-10.0	PSIM	0.0
91	30000.0	TIME	0.0	-10.0	PSIM	0.0
92	30000.0	TIME	0.0	-10.0	PSIM	0.0
93	30000.0	TIME	0.0	-10.0	PSIM	0.0
94	30000.0	TIME	0.0	-10.0	PSIM	0.0
95	30000.0	TIME	0.0	-10.0	PSIM	0.0
96	30000.0	TIME	0.0	-10.0	PSIM	0.0
97	30000.0	TIME	0.0	-10.0	PSIM	0.0
98	30000.0	TIME	0.0	-10.0	PSIM	0.0
99	30000.0	TIME	0.0	-10.0	PSIM	0.0
100	30000.0	TIME	0.0	-10.0	PSIM	0.0

HUN 3.

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1-21-77

UT145(370)

HEIGHT	10457.7	RSCG	302.27202	V	02.2	PSIR2	2.2
LA	3099.0	ALC	251.10002	DEL	-5.2	VSIR2	0.2
LY	34945.2	END	0.23700212E-2	V50040	1117.2	VYSIR	0.2
LZ	31255.2	TIME	0.20000000E-1	DEL3M	0.7	VZSIR	0.2
U-5M	27.01444	NOSS	0.0	TASIR	-10.2	PSIR	2.2
DEL3M	124.00000	N355	5.0	T-5174	-10.0	LV1	273.2
RPL	15.2	PASLMT	225.2	ALMT	225.2	PSVT	095.2
PSVT	7.00000	SM	0.0	SVT	32.30000	OSTM	0.2
LAISTK	-1.35002	AIS	-1.9400279	IMT	25.30597	YA	41.095057
LA3STK	3.001075	BIS	3.0674397	IS	-3.2	XS	36.210410
COLSTK	15.000344	THEIAR	16.00039	TH75M	3.9003991	XC	36.082495
PEVAL	12.761400	THEITM	19.00339	TH75TH	5.943591	XP	46.225714
XALC	4.103587	XAIN	3.6210817	XCIR	3.0002095	XPIR	2.0001236
XALCUP	0.20000	XOALTI	0.2000000	OSTM	2.0	PSIR	0.2
VAC	67.35500	THEIAB	3.7537955	AAZP	3.1762742	OSTR	0.2
VPO	7.0	PRID	-1.0730554	AAIP	-0.1663592	OSTM	0.2
VLO	0.0222722	DETAMP	0.2	MBIP	-0.59771222E-1	TITR	0.2
P	0.2	GAMC	0.0	AAZL	-1.9062449	MITM	0.2
G	2.2	DMGRAT	1.2	AXIL	2.17669637	JITR	2.2
R	0.2	PSIOUT	0.2	MBIL	0.93042653E-1	PHIR	0.2
ALPAP	-11.006777	EXTR	1.1075013	EXKRX	2.79900259	LMIR	0.2
CHITPP	7.000015	EXTL	2.0463325	EXKXZ	1.0191017	UMIR	0.2
EATH	2.2	EPSAT	0.0099999	SIGKT	2.0	XITM	0.2
GRP	0.0075000	ALMT	0.0717794	KAVI	2.34052015	VITM	0.2
MU3	0.93233623E-1	CTSIG	2.67221225E-1	LTOI	-17.253200	ZITM	0.2
MU2	0.0	CHSIG	-0.10075725E-2	DIOT	25.077360	LITM	0.2
LAMCH	0.12000000E-2	CUMSIG	0.51217517E-0	MM	750.55921	MITM	0.2
DASHW	0.20000000E-1	NZ	0.94735012	MM	1099.5961	MITM	0.2
XP	100.00000	VC	0.12390000	XIMBLK	1.2	AXP	2.0000007
YMP	0.31400001	MDAM	-419.41507	VABOOI	-0.15525200E-1	ATP	0.79304147
ZMP	-13.000001	JDMR	319.00001	VABOOI	-0.15525200E-1	ATP	-32.0000007
LMP	-0.000001	TDMR	15551.121	VZOOI	2.36002779E-2	VXP	67.055000
MM	1310.0001	LDAM	-1112.0000	PUOI	-0.10112553E-2	VYP	0.0
NMP	2170.0001	MDAM	-5010.0000	SOOI	0.12012360E-3	VZP	4.4000007
XMP	-140.00001	DMR	22370.531	MUOI	0.00359572E-0	PSIR	0.0
YMP	2.2	XT	-01.000001	XIR	0.0	PSIUG	0.0
ZMP	195.00000	ZT	-07.300000	YIM	709.10025	STR	0.2
LMP	0.0	LT	-26.900000	ZIR	-250.00007	MADU	0.2
NMP	-0.000001	MT	-13.000000	LTW	0.000000	XADD	0.0
XMP	-17.000000	MT	-100.75000	MTW	-1996.6105	YADD	0.0
YMP	-17.000000	XVT	-0.000000	MTW	-21970.075	ZADD	0.0
ZMP	-01.000000	YVT	-07.300000	ALMTI	1.0222573	MADU	0.0
		ZVT	0.90170050	ALPVT	2.2	LADD	0.0



MUN 5.

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1-21-77

UTIAS (5175)

WEIGHT	16457.2	FSC6	562.22023	V	80.0 *	PSIR2	0.0
IA	5024.0	ALC6	231.10702	UELS	-5.0	VXSIM.	0.0
IV	3944.0	RMD	8.23760020E-2	VSDUUD	1117.4	VSTR.	0.0
IZ	3700.0	TIME	0.20000000E-1	UFL3MM	0.0	VZSIM.	0.0
ORPUAR	27.01494	WSS	4.0	TASIMM	-18.0	PSIM.	0.0
ORPULM	12.02000	WSS	5.0	TASIMM	-18.0	MLVT	273.0
RPR	15.0	PASUNT	1272.2	FLMT	250.0	PSVT	0.0
FSMT	702.00000	SMT	45.0	SVT	32.30000	USTM.	0.0
LAI3TK	0.05342077	AIS	-1.1745910	IMT	-2.47450734	XA	46.357332
LAI3TK	7.0002244	BIS	7.4064132	IS	-5.4	XB	22.852208
COL3TK	15.507016	THEIAT	15.007016	IM73MM	5.7270163	XC	33.290052
PEUAL	11.700434	THEITM	11.700434	IM73MM	4.0763108	XP	40.938002
TAIR	0.057332	XDIM	2.2052228	XCIM	3.3298852	YPIR	2.6426052
XDAUTP	0.0513407	XDACTI	0.0613407	ADDP	0.0	PSIM	0.0
VIM	134.73965	THEIAD	4.5362799	ADDP	3.2093926	OSTM	0.0
VIM	11.070372	FMID	0.0	AAIP	-4.9204211	HSTM	0.0
VZ0	10.420304	MEIAMP	0.4539273	BBIP	0.10209245	TITR	0.0
V	0.0	GAUC	0.0	AAVL	-3.6530274	MITM	0.0
Q	0.0	DEGRAT	1.7	RAIC	2.22108371	JITR	0.0
R	0.0	PSIUDT	0.0	BEIL	0.20619540	MMITR	0.0
ALPAP	0.17034058	ERIX	1.0041026	EAHX	0.92513126	UMITR	0.0
CHITAP	0.1453173	EATZ	1.0735235	EAPZ	1.0020660	UMITR	0.0
ERIM	0.0	EMST	0.044033927	SIGMT	0.70037124	XITM	0.0
QAT	25.012501	KMT	0.07177974	KQVI	0.02736242	YITM	0.0
MUS	0.10654921	CTSIG	0.07400003E-1	LTOT	2.9619329	ZITR	0.0
MUS	0.10654935E-1	CM516	-0.40096060E-2	DTOT	24.460705	LITM	0.0
MUS	0.03047050E-2	CM516	0.44025111E-6	TTM	715.97046	MITM	0.0
LAMPAR	0.10000000E-1	WZ	0.94696325	MPMK	994.75765	NITM	0.0
DeShap	0.10000000E-1	VC	0.71525373E-3	KTRBLK	1.0	AXP	2.0010130
ATA	1000.4172	MDAM	-1046.3482	VHUOT	0.11368335E-2	ATP	-0.46706579E-2
YMR	227.03335	J0AM	247.00345	VHUOT	-0.25091043E-2	AZP	-32.077005
ZMR	-1000.130	T0AM	15054.578	V200U1	-0.90000000E-2	VAP	134.74965
LPM	-4100.0000	L9AM	-1745.7020	PUOT	-0.70000000E-3	VAP	11.250372
MPM	200.0000	MDAM	-13400.397	UUOT	-0.19000000E-3	VZP	10.920009
NPM	1910.000	Q0AR	20000.571	UUOT	0.45209100E-3	PSIM.	0.0
KAF	-0.0010007	RI	-5.0746026	XIM	0.0	PSIUMG	0.0
YAF	-292.00000	YI	-134.15084	YIR	0.72.00702	BTM	4.0
ZAF	-60.707434	ZI	249.31175	ZIR	-249.09705	MADG	0.0
LAF	570.55014	LI	-234.48934	LIR	364.10000	XADU	0.0
KAF	-0.0010007	MI	6495.0505	MIR	-1507.7269	YADU	0.0
NAF	-2000.0000	NI	3745.0599	NIR	-2000.0000	ZADU	0.0
XMI	0.0010007	XVI	-4.3943014	ALFMTI	-4.3943014	NAUL	0.0
YMI	0.0000000	YVI	-132.51270	ALFMTI	-4.3943014	LROD	0.0
ZMI	0.0000000	ZVI	0.31515441	AA001P	4.9294950		



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UN 7.

UTIAS(S/E)

WEIGHT	15450.0	FSCG	367.20000	V	120.0	PSIR2	0.0
IX	5024.0	ALC	251.10000	UCLS	-5.0	VSIR.	0.0
IV	57440.0	RHO	0.23700000E-2	VBOUND	1117.0	VSTR.	0.0
IZ	37220.0	TIME	0.00000000E-1	DEL3MM	0.0	VZSTR.	0.0
OMEGH	27.11999	NHSS	4.0	TASIR	-10.0	PSTR.	0.0
OMEGH	124.00000	NSSS	5.0	TNSIR	-10.0	FLVI	273.0
RFR	15.0	PASST	402.0	PLMT	234.0	FSVT	695.0
FSH	107.00000	SHI	45.0	SVT	32.50000	QSTR.	0.0
LATSTK	-0.6757000	AIS	-1.4210533	IMT	-4.5067430	XA	45.770196
LNGSTK	16.504197	HIS	11.197095	IS	-3.0	XB	12.741350
CULSTK	17.770000	TMETAR	17.706066	TM75MM	7.6200660	XC	45.162914
PEUAL	16.500974	IMELT	19.240254	TM75TK	5.7402541	XP	52.503795
XAIN	0.3772156	XJIN	1.2741350	XCIN	4.5102915	XPIN	2.8243314
XALIP	12.444583	XMACIL	1.2994383	XSIN	4.0	PSTR	0.0
VXB	202.45461	TMETAB	5.1160607	ASOP	5.1500043	QSTR	0.0
VVB	10.270000	PHIB	0.0	AAIP	-6.4089694	HSIN	0.0
VZB	11.026503	BCATAP	5.3497433	BBIP	-0.51151017E-1	HTIN	0.0
P	0.0	GAMC	0.0	AAOL	-5.0076570	HTIN	0.0
Q	0.0	ORGRAT	1.0	AAIC	2.27798430	JITH	0.0
H	0.0	PSIDUT	0.0	BBIL	0.50007981	MMTH	0.0
ALPAP	0.40950001	EXTX	1.0750521	EXKTX	0.91299096	LMITH	0.0
CHITPP	0.4945025	EXTZ	1.0050107	EXKTX	1.0090006	UMITH	0.0
ERIN	0.0	EPST	0.00549743	SIGMT	0.50955484	XITH	0.0
GPF	57.350244	KWHI	0.0717794	KJVI	0.05208756	YITH	0.0
MUAS	0.27970122	CTSIG	0.68356389E-1	LTOT	3.9771569	ZITH	0.0
MUYS	0.10426504E-1	CHSIG	-0.256734839E-2	U101	24.522825	LITH	0.0
MUZS	0.37054993E-3	CHSIG	0.30452904E-0	TTR	1030.0700	MITM	0.0
LAMBHM	-0.49452409E-2	NZ	0.99949057	MPHM	1392.5929	NITH	0.0
DASHMR	0.10515009E-1	VC	0.14505114E-4	KTRBLK	1.0	AXP	1.7330175
YMK	2104.5629	MAAM	-1310.4382	VXBUOT	-0.19047693E-1	AYP	0.26002307E-1
YMK	-270.41793	J0AM	270.41793	VXBUOT	0.17904924E-1	AZP	-32.100001
ZMK	-1574.473	T0AM	15056.330	VZBUOT	-0.21033093E-1	VXP	202.40401
LMM	-0.2201350	L0AM	-3020.2713	PUOT	0.00040100E-2	VYP	12.270055
MMK	-4095.1479	M0AM	-18959.971	QUOT	-0.25200209E-2	VZP	11.026503
NMK	27050.764	W0AM	20300.630	KUOT	0.10035456E-3	WSTM	0.0
NMK	-1255.4040	XT	-40.236324	XTH	0.0	PSIUMG	0.0
YAF	4002.12191	YT	-230.00078	YTR	970.11009	BTM	0.0
ZAF	-220.21700	ZI	724.06531	ZIR	-355.27592	MAUO	0.0
LMP	910.03799	LI	-423.01341	LIM	5572.3236	XADD	0.0
MPF	-4411.4547	MT	20513.092	MTR	-11007.632	YADD	0.0
NMP	-4067.2525	NI	6609.2769	NTR	-30243.162	ZADD	0.0
XMT	-31.155046	XVT	-17.002427	ALFMTI	-5.3600431	NAUU	0.0
YMT	-2.5371134	YVT	-230.19167	ALPVTI	3.4503545	LADD	0.0
ZMT	723.70053	ZVT	0.30470071	AABDIP	6.9694309		







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UTIAS(376)

RUN 12:

WEIGHT	1980.0	PSCU	300.20000	140.0	140.0	PSTRZ	0.0
IX	6200.0	WLCU	246.29999	-5.0	-5.0	VXSIR	0.0
IY	41507.0	AMO	0.23780000E-2	VSOUND	1117.0	VYSIR	0.0
IZ	30224.0	TIME	0.20000000E-1	DELJMH	0.0	VZSTR	0.0
OMEGMR	27.019999	NOSS	4.0	TWSIMH	-10.0	PSTR	0.0
OMEGTR	124.62000	NSSS	5.0	TWSITH	-10.0	MLVI	273.0
KPR	15.0	PASCNT	1910.0	MCMT	234.0	PSVT	695.0
FSMT	700.40000	SMT	45.0	SVT	32.500000	USTH	0.0
LATSTR	-1.3798829	AIS	-2.3487000	IMT	-4.9080073	XA	41.375731
LANGSTR	15.968756	BIS	14.179321	IS	-5.0	XB	14.244676
COLSTR	14.006008	THETA0	19.006008	TH7SMH	9.0060087	XC	50.787930
PEDAL	14.418970	THETA1	25.706253	TH7STM	12.206253	XP	41.630700
XAIN	4.1375731	XBIN	1.4248076	XBIN	9.0707930	XPM	2.2479997
XBACTP	15.163044	XBACTI	1.3163444	RSTM	0.0	PSTM	0.0
VXB	250.10613	THETA0	3.4211264	AAWF	3.9774003	QSTR	0.0
VYB	14.006250	PHIB	0.0	AAIF	-0.0690840	RSTR	0.0
VZB	14.119190	BETAWF	3.3094763	BWIF	-0.24999690	TSTR	0.0
P	0.0	GAMC	0.0	AAOL	-7.0130896	MTH	0.0
R	0.0	ORGMAT	1.0	AAIL	0.41012052	JTM	0.0
ALFWF	1.4442033	EATX	1.5164054	ERMPX	0.75937691	MHTR	0.0
CHITPP	0.0.446062	EKTZ	1.6779347	EKMPZ	0.90500910	LMTR	0.0
EKTR	0.0	EP3MT	0.00309476	SIGMT	1.0095531	QHTR	0.0
QWF	70.667645	KOMT	0.07177979	KQVT	0.50240783	XTR	0.0
MUXS	0.52631796	CT916	0.03109924E-1	LTOI	0.03270099	YTR	0.0
MUYS	0.19430742E-1	CHS16	0.03109924E-1	DTOT	4.9271002	ZTR	0.0
MUZS	0.23989400E-2	CUMS16	0.63847310E-6	TTR	24.675700	LITR	0.0
LAMBMR	-0.04744056E-2	NZ	0.99927145	MPHM	1415.4938	MITH	0.0
UMSMR	0.10075906E-1	VC	0.14305114E-4	KTRMLK	1906.7465	NITH	0.0
XMR	2900.5003	MBAN	-1094.0922	VXDUOT	1.0	AXP	1.90442943
YMR	-397.76794	JBAR	397.76794	VYDUOT	-0.29005149E-1	AYP	-0.14610363E-1
ZMR	-19157.233	TBAN	19204.285	VZDUOT	-0.51372307E-3	AZP	-32.112627
LMR	-0.026.0007	LBAMH	-0.026.6037	PUOT	-0.35536930E-1	VXP	236.16613
MMR	-7416.0105	MBAMH	-21727.105	QUOT	-0.30901322E-2	VYP	14.006250
NMR	37008.056	QBAM	30012.303	RUOT	-0.03603008E-2	VZP	14.119190
XWF	-1701.6451	XT	-77.246506	XTR	0.0	RSTR	0.0
YWF	-614.24034	YT	-310.46049	YTR	1330.2200	PSIUMG	0.0
ZWF	-341.30724	ZT	950.69202	ZTR	-0.04.16434	BTM	2.0
LMF	970.13007	LT	-697.51570	LTR	8125.9047	MADU	0.0
NMF	-5106.3505	MT	27176.264	MTR	-15001.025	XADU	0.0
NMT	-5422.0009	NT	8006.0323	NTR	-41214.897	YADU	0.0
XMT	-53.604132	XVT	-23.562374	ALFMTT	-5.2875001	ZADU	0.0
YMT	-3.4697249	YVT	-314.49076	ALFVIT	3.3911209	NADU	0.0
ZMT	958.57240	ZVT	0.11954006	AABVIT	8.0735554	LADU	0.0

RUN 13.

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UTIAS(8/0)

WELGHT	1982.2	FSC	302.2222	A	152.2	PSITW2	2.2
IX	655.2	ALCB	246.29999	DEL3	-5.2	PSITW2	2.2
IY	4197.2	RMO	2.2378222E-2	VSOUND	1117.2	VSITW2	2.2
IZ	30224.2	TIME	0.2044222E-1	DEL3M	2.2	VSITW2	2.2
OMEGAR	27.21999	MS3	4.4	VSITW2	-15.2	VSITW2	2.2
OMEGTA	124.6222	MS3	5.4	VSITW2	-15.2	VSITW2	2.2
RFR	15.2	PASANT	652.2	VSITW2	252.2	VSITW2	2.2
FMT	722.4222	SMT	45.2	VSITW2	32.12222	VSITW2	2.2
LATSTR	-1.7212238	MS	-2.7604971	VSITW2	-5.25294292	VSITW2	2.2
LN6STR	15.322231	MS	15.642292	VSITW2	-5.2	VSITW2	2.2
COLSTR	22.522231	THETA2	22.842292	VSITW2	12.762231	VSITW2	2.2
PEDAL	14.772232	THETA2	27.229231	VSITW2	15.722231	VSITW2	2.2
IAIN	3.932231	THETA2	2.932231	VSITW2	6.772231	VSITW2	2.2
IBACTP	7.032231	THETA2	6.732231	VSITW2	2.2	VSITW2	2.2
VIB	253.2231	THETA2	3.122231	VSITW2	4.212231	VSITW2	2.2
VIB	15.2231	THETA2	2.2	VSITW2	-2.251231	VSITW2	2.2
VIB	14.2231	THETA2	3.322231	VSITW2	-2.251231	VSITW2	2.2
P	2.2	THETA2	4.2	VSITW2	-2.251231	VSITW2	2.2
Q	2.2	THETA2	1.2	VSITW2	2.251231	VSITW2	2.2
R	2.2	THETA2	2.2	VSITW2	2.251231	VSITW2	2.2
ALPMP	1.422231	THETA2	1.522231	VSITW2	2.251231	VSITW2	2.2
CHITP	74.222231	THETA2	1.522231	VSITW2	2.251231	VSITW2	2.2
EXTP	8.2	THETA2	0.422231	VSITW2	2.251231	VSITW2	2.2
QMP	82.222231	THETA2	0.422231	VSITW2	2.251231	VSITW2	2.2
MUS3	2.322231	THETA2	2.322231	VSITW2	2.251231	VSITW2	2.2
MUS3	2.212222E-1	THETA2	-2.212222E-1	VSITW2	2.251231	VSITW2	2.2
MUS3	2.112222E-1	THETA2	-2.112222E-1	VSITW2	2.251231	VSITW2	2.2
LAMPB	-2.922222E-2	THETA2	-2.922222E-2	VSITW2	2.251231	VSITW2	2.2
DMSMB	2.122222E-1	THETA2	2.122222E-1	VSITW2	2.251231	VSITW2	2.2
YMR	441.2122	THETA2	441.2122	VSITW2	2.251231	VSITW2	2.2
ZMR	-1922.2122	THETA2	-1922.2122	VSITW2	2.251231	VSITW2	2.2
LMR	-9622.2122	THETA2	-9622.2122	VSITW2	2.251231	VSITW2	2.2
PMR	-1632.2122	THETA2	-1632.2122	VSITW2	2.251231	VSITW2	2.2
NMR	4312.2122	THETA2	4312.2122	VSITW2	2.251231	VSITW2	2.2
IMF	-1432.2122	THETA2	-1432.2122	VSITW2	2.251231	VSITW2	2.2
YMF	-711.2122	THETA2	-711.2122	VSITW2	2.251231	VSITW2	2.2
ZMF	-441.2122	THETA2	-441.2122	VSITW2	2.251231	VSITW2	2.2
LMF	1123.2122	THETA2	1123.2122	VSITW2	2.251231	VSITW2	2.2
PMF	-522.2122	THETA2	-522.2122	VSITW2	2.251231	VSITW2	2.2
NMF	-622.2122	THETA2	-622.2122	VSITW2	2.251231	VSITW2	2.2
IMT	-67.1222	THETA2	-67.1222	VSITW2	2.251231	VSITW2	2.2
YMT	44.2222	THETA2	44.2222	VSITW2	2.251231	VSITW2	2.2
ZMT	1165.222	THETA2	1165.222	VSITW2	2.251231	VSITW2	2.2



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ULIAS(15/1)

ALIGHT	179000.2	PSGB	398.22322	Y	42.7	PSIR2	P.0
IX	6400.0	MLCB	246.29944	DELS	-5.0	VASIM.	0.0
IV	4157.5	WMO	7.25780222E-2	VSCURD	1117.8	VYSTH.	0.0
IZ	30224.0	TIME	0.00000000E-1	DELSTM	0.0	VZSTM.	0.0
OPRGMK	27.214479	WSS	4.0	TXSTM	-10.0	PSIM.	0.0
OPRGMK	124.00000	WSS	5.0	TXSTM	-10.0	PLVT	273.0
KFM	150.0	PSURST	17047.0	SVT	254.0	PSVT	695.0
FSM1	700.0	SMI	45.0	SVT	32.36000	USTH.	0.0
LATSK	-1.7050571	AIS	-2.4317423	IMT	27.095343	XA	34.215040
LNGSK	5.2703300	PIS	4.1503410	IS	-5.0	XB	31.305533
CULSK	17.357019	TMETAV	17.357019	TMZSM	7.2570195	XC	42.000122
PEVAL	17.000000	TMETTH	24.911405	TMZSTM	11.411405	XP	35.350113
XAIR	3.921077	XPR	3.150533	XLST	0.2000121	XPM	1.3091004
XOALIP	37.000000	XOAL11	3.7000425	USTH.	0.0	PSIM	0.0
VXO	07.347203	TMETAB	4.4101392	AACP	4.7000203	USTH	0.0
VYC	0.0	PHIB	-1.4479620	AAIP	-2.5902430	USTH	0.0
VZB	5.0710417	METANT	5.0	MOIP	-4.10730043	TITM	0.0
P	0.0	UANC	0.0	AAEL	-5.1002034	MITM	0.0
Q	0.0	DRUMAT	1.0	AAIC	7.25352309	JITM	0.0
K	0.0	PSIU01	0.0	BUIL	0.13468700	MMITR	0.0
ALPAP	-13.071009	EXAT	1.1112937	EXMKA	0.70130401	MMITR	0.0
CHITPA	67.102710	KATZ	2.2432155	EXATZ	1.2204146	MMITR	0.0
EXTH	0.0	EPST	2.40999949	SLGT	0.0	XITM	0.0
QAF	9.5531703	KMT	0.41177979	KLVT	0.04052013	XITM	0.0
MUXS	2.9307773E-1	CI910	0.00132007E-1	LIUT	-21.025470	ZITM	0.0
MUTS	0.0	CMS10	-0.29517450E-2	DIUT	26.039905	LITM	0.0
MUZS	0.25772007E-2	CMS10	0.055534170E-6	TIM	900.77001	MITM	0.0
LAMPMP	-0.51515154E-1	NZ	0.99685525	MPM	1406.1050	MITM	0.0
UMSMMP	0.55025300E-1	VL	0.11070330	KTHOLK	1.0	AXP	2.5120026
XMK	1001.2774	MSAM	-684.90300	VXU01	0.3204005E-1	AYP	0.70547506
YMK	-43.035993	MSAM	0.3303943	VXU01	-0.50155167E-2	AYP	-32.073034
ZMK	-10494.110	TSAM	19257.502	VZU01	-0.73471720E-2	VXP	67.397243
MMK	-5504.7012	LPAMH	-1423.6270	PDU1	0.69370100E-3	VYP	0.0
MMK	14501.405	MOAMH	-6937.1763	QDU1	-0.20397170E-3	VZP	5.2076017
NMK	27740.730	UBAM	20621.696	QDU1	-0.75201041E-3	RSTH.	0.0
XAF	-149.41154	TI	0.0025415	XIP	0.0	PSIUMH	0.0
YAF	0.0	VI	-7.0006345	VIM	904.77514	BITR	2.0
ZAF	202.07417	ZI	32.703026	ZIM	-329.31185	MAUU	0.0
LAF	0.0	LI	-16.000000	LIP	5527.0004	MAUU	0.0
MAF	-5137.0001	MT	943.69649	MTM	-12243.170	YAUU	0.0
NAF	0.0	NT	211.00710	NTM	-20032.949	ZAUU	0.0
XMI	12.071500	XAT	-1.9951300	ALFMT	-0.00001371	MAUU	0.0
YMI	0.0	VAT	-7.5006345	AFVAT	0.0	LAUU	0.0
ZMI	51.000000	ZAT	1.00949344	ABOIF	2.6249910		

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0110313107

17922.0

HEIGHT	17922.0	PSG	300.20202	V	62.7	PSIR2	0.0
IX	6255.2	WLCB	246.29999	UCLS	-5.0	VXSTR	0.0
IY	41507.0	WMO	2.237620002-2	VROUND	1117.0	VZSTR	0.0
I2	35228.0	TIME	W.24000000E-1	UCLSAM	0.0	VZSTR	0.0
OPERA	27.21944	ROSS	4.0	TSIMM	-14.0	PSIR	0.0
OPERM	124.00000	ROSS	5.0	TSIMM	-10.0	MLVT	273.0
KPR	13.2	PASST	1077.0	MLMT	234.0	PSVT	0.0
FSMT	12.00000	SM	45.0	SVT	52.50000	QSTR	0.0
LAISTR	-1.711590	AIS	-1.0552692	IMT	14.517045	XA	43.061450
LAISTR	6.204550	DIS	5.1234212	IS	-5.0	XD	20.059561
CULSTR	14.71372	TMETAN	18.713972	1475PM	6.5334722	XC	30.962327
PEVAL	15.70113	TMELIM	23.247080	1475PM	9.7470004	XP	37.893361
XAIR	0.501050	XDIR	2.0059961	XDIR	5.2762327	XPRM	2.2001072
XOACTP	30.431150	XOACTI	3.2430730	XSTR	2.0	PSIR	0.0
XVS	101.15302	TMETAB	3.7511125	ASOP	3.9477367	QSTR	0.0
VVB	12.451407	PMLO	2.0	AAIP	-2.0161533	HSTR	0.0
VZB	6.5303025	PMETAP	6.5055176	BBIP	2.42100005E-1	YSTR	0.0
P	2.0	GANC	0.0	AAOL	-4.5049324	MITH	0.0
Q	0.2	UMGRAT	1.2	AAIL	0.20007037	JSTR	0.0
ALPHA	0.0	PSIDOT	0.0	BBIL	0.11004274	MMTR	0.0
CHITIM	10.21101	EXTX	1.3053120	EMTX	0.00033079	LMTR	0.0
EXTX	0.0	EXTZ	1.0474976	EXTZ	1.0117001	UMTR	0.0
EPSMT	0.0	EPSMT	0.51305517	SIMT	1.02010041	XIM	0.0
KMT	0.0	KMT	0.0	ACVT	2.74501501	YIM	0.0
CISIG	0.0	CISIG	0.0	L101	-5.5549270	ZIM	0.0
CHSIG	0.0	CHSIG	0.0	L101	25.2515201	LIM	0.0
CHSIG	0.0	CHSIG	0.0	TIM	0.1471354	MIM	0.0
NZ	0.0	NZ	0.0	MPHM	1175.6359	NIM	0.0
VC	0.0	VC	0.0	MTBLK	1.0	ARP	2.0900001
MDAM	0.0	MDAM	0.0	VBDUT	-0.13364507E-1	AYP	-2.59639441E-3
MDAM	0.0	MDAM	0.0	VBDUT	0.124000420E-2	ADP	-32.040456
MDAM	0.0	MDAM	0.0	VBDUT	0.02022023E-2	VXP	101.10302
MDAM	0.0	MDAM	0.0	PUUT	-0.25570157E-3	VYP	12.950007
MDAM	0.0	MDAM	0.0	CUUT	0.24400000E-3	VZP	6.6343025
MDAM	0.0	MDAM	0.0	RUUT	0.07003605E-3	RSTR	0.0
MDAM	0.0	MDAM	0.0	XTM	0.0	PSIML	0.0
MDAM	0.0	MDAM	0.0	YTM	765.63704	BTM	2.0
MDAM	0.0	MDAM	0.0	ZTM	-270.66962	MAOD	0.0
MDAM	0.0	MDAM	0.0	LTM	4677.0472	XADU	0.0
MDAM	0.0	MDAM	0.0	MTM	-0.634.1136	YADU	0.0
MDAM	0.0	MDAM	0.0	NTM	-23721.986	ZADU	0.0
MDAM	0.0	MDAM	0.0	ALFMTT	2.02752224	NAUD	0.0
MDAM	0.0	MDAM	0.0	ALFMTT	7.0490203	LAUD	0.0
MDAM	0.0	MDAM	0.0	AAADIT	2.0164931	LAUD	0.0

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UTIA (576)

WEIGHT	19907.0	FSCG	362.20222	V	03.2	PSIR2	0.0
IX	6299.0	ULL	246.23999	UCLS	-5.0	VISTR.	0.0
IY	41347.0	RHD	0.2370220VE-2	VSDUD	1117.0	VISTR.	0.0
IZ	30224.0	TIME	0.2000000DE-1	UPLSM	0.0	VSTR.	0.0
OMEGM	27.21999	NBS	4.0	TASTM	-10.0	PSTR.	0.0
OMEGH	124.62000	NBS	5.0	TASTM	-10.0	PLVT	273.0
RPR	15.0	PASCHT	1322.0	WMT	290.0	PST	695.0
FSMT	720.40000	SMT	43.0	SVT	52.50000	USTH.	0.0
LATSTR	0.59374108	AIS	-1.3039529	INT	0.50292289	XA	44.410115
LNSTK	0.4120291	BIS	0.1439054	IS	-3.0	XB	10.577201
CULSTK	10.012109	TMETAB	16.012149	TW5MR	0.7321094	XC	39.575934
PEUAL	14.402647	TMETW	22.003226	TW5TR	0.5012266	XP	41.454101
XAIN	4.4413115	XBIN	1.8577201	XBIN	3.9575932	XPIR	2.2380675
XBACIP	22.011420	XBACTI	2.2011920	WSTM.	0.0	PSTM	0.0
VXN	133.62519	TMETAB	5.3392774	AAOF	3.9490476	OSTR	0.0
VYN	12.070534	PHID	0.0	AAIF	-5.1259021	RSTM	0.0
VZB	12.500529	DETAMF	4.6932903	BOIF	2.82351620E-1	TITR	0.0
P	0.0	GAMC	4.0	AAOL	-4.2469659	MITR	0.0
Q	0.0	DIGRAT	1.0	AAIL	2.29804330	JITR	0.0
R	0.0	PSUDOT	0.0	BOIL	0.3502232	MMILK	0.0
ALP>F	0.40492242	EKTZ	1.4071622	ERMPX	0.9100409	LMITR	0.0
CHITPH	01.443415	EKTZ	1.6799061	EKAP2	1.0005500	UMITR	0.0
EFTK	0.0	EP3MT	0.4903297	SIGMT	0.82002050	XITM	0.0
WFF	25.400504	KUMT	0.0717794	KUVI	0.02610750	YITM	0.0
MUXS	0.10531531	CTSIG	0.02170997E-1	LTOT	2.3030110	ZITM	0.0
MUTS	0.10650513E-1	CHSIG	-0.59944204E-2	UIUT	24.510659	LITM	0.0
MUZS	0.70113044E-2	UMSIG	0.5433840E-0	TTR	0.24.07250	MITM	0.0
LAMHMK	0.11150401E-1	NZ	0.99553440	MPHM	1163.7512	NITM	0.0
DASHMR	0.10767000E-1	VC	0.71525573E-5	KTRBLA	1.0	AXP	2.9000327
KMK	2504.4904	MBAM	-1300.5877	VXBUOT	-0.51760114E-2	AYP	-0.10300309E-1
YIM	4323.1059	JBAM	325.10009	VYBUOT	0.10203010E-1	AZP	-32.020099
ZMK	-10467.441	TBAM	19000.195	VZBUOT	0.21246470E-2	VXP	154.60519
LW	-4959.2070	LBAM	-1011.5192	PUOT	-0.49494570E-2	VYP	12.070333
MM	3104.0002	MBAM	-13433.217	WUOT	0.11635551E-2	VZP	12.500529
NM	2502.007	QBAM	25000.000	KUOT	-0.24702910E-3	PSIR.	0.0
XK	-011.50014	XT	1.5413011	XTH	0.0	PSIUNG	0.0
YK	-310.55095	YT	-102.51030	YTH	779.00313	PTR	0.0
ZK	-55.90357	ZT	304.95174	ZTR	-203.05479	MAUU	0.0
LW	500.00000	LT	-310.23209	LTH	0700.0725	XADD	0.0
MM	-0001.1050	MT	0059.5000	MTH	-0794.7677	YADD	0.0
NK	-2005.2973	NT	5955.0176	NTH	-20105.370	ZADD	0.0
XMT	5.2140707	XVT	-3.0705139	ALFMTT	-4.2306754	NAUU	0.0
YMT	0.1037077	YVT	0102.27095	ALFVTT	5.1027095	LADD	0.0
ZMT	3.4005004	ZVT	0.32504053	AA001P	5.1027095		



UTIAS(S/O) 1-21-77 30-AUG-77

MUN 31.

REL(M)	1993-2	FSCG	307.20000	V	120.0	PSIR2	0.0
IA	6000.0	ALLO	246.29999	DELS	-5.0	VASIR	0.0
IV	41507.0	RHU	0.25782002E-2	VSOUDU	1117.0	VYSIR	0.0
12	30024.0	TIME	0.20000000E-1	DELSMR	0.0	VZSMR	0.0
OMEGP	27.019494	WSS	4.0	TSSTM	-10.0	PSTM	0.0
OMEGH	124.00000	WSS	5.0	TSSTM	-10.0	HLVT	213.0
KPR	15.0	PASCT	650.0	ALMT	234.0	FST	695.0
FST	700.00000	SMT	450.0	SVT	30.00000	USTM	0.0
LATSTK	-0.00154072	AIS	-1.00000000	IMT	-3.70000000	XA	43.027020
LANGSTK	11.0101021	BIS	11.3070000	IS	-3.0	XB	0.9514927
CULSTK	10.310001	THEAD	10.375001	TM75M	0.2430010	XC	49.336750
PEDAL	13.000000	THEAD	23.000000	TM75M	9.9040010	XP	42.013004
XAIR	0.000000	XAIR	0.000000	XCM	0.0	XPIN	2.3110053
XOACTP	0.000000	XOACTI	0.000000	ASIM	0.0	ASTM	0.0
VXB	200.00000	THEAD	3.000000	AAVP	3.9300000	OSTM	0.0
VTH	10.0101021	PHID	0.0	AAIP	-6.6270000	RSTM	0.0
VZM	15.000000	MTAMP	3.200000	BBIP	0.4100000	TITM	0.0
P	0.0	GAUC	0.0	AAOL	-5.5720000	MITM	0.0
Q	0.0	DMONAT	1.0	AAIL	0.3500000	JTM	0.0
R	0.0	PSUOT	0.0	BPIL	0.5400000	MMTH	0.0
ALFAP	1.000000	ERTX	1.400000	ERAPX	0.9210000	LMTR	0.0
CHLAP	0.100000	ERTZ	1.600000	ERAPZ	1.0000000	CHTR	0.0
ERTM	0.0	TPST	0.000000	SIGAT	0.5700000	XITM	0.0
QAF	55.014500	KMTI	0.01777779	KLVI	0.8320000	VITM	0.0
MUS	0.000000	CTSIG	2.000000	LTOT	0.5220000	ZITM	0.0
MUS	0.101500	CHSIG	-0.000000	DTOT	24.000000	LITM	0.0
MUS	0.000000	CHSIG	0.000000	TIR	1115.0000	MITM	0.0
LANEKA	0.000000	NZ	0.900000	MPMK	1505.0000	NITM	0.0
DASHKE	0.100000	VC	0.715000	KTPBLK	1.0	AXP	2.172000
KW	2615.0000	MDAK	-1617.0000	VABUOT	0.5596000	AYP	-0.55913172E-1
YPM	500.00000	JBAR	303.00000	VABUOT	-0.1025000	AP	-32.000000
ZPM	-10.51000	LBAR	1915.0000	VABUOT	0.1091400	VXP	202.34200
LPM	-0011.9000	LBARM	-2901.5000	WUOT	-0.1170000	YPM	12.14700
MPM	-2011.0000	MPARM	-1700.0000	WUOT	0.5050000	VZP	15.72500
NPM	2400.0000	DBAR	3000.0000	WUOT	-0.2270000	WSTM	0.0
XPM	-10.0000	XI	-47.0000	XIM	0.0	PSIUMG	0.0
YPM	0.000000	YI	-235.0000	YIM	1000.7000	UTM	2.0
ZPM	-200.0000	ZI	641.0000	ZIM	-301.0000	MADD	0.0
LPM	100.0000	LI	-515.0000	LIM	0.500.0000	XADD	2.2
MPM	-400.0000	MI	1000.0000	MIM	-1100.0000	YADD	0.0
NPM	-4000.0000	NI	000.0000	NIM	-5200.0000	ZADD	0.0
XPM	-50.0000	XI	-17.0000	ALFMTI	-4.671000	NAUU	0.0
YPM	-20.0000	YI	-232.0000	ALFMTI	-4.671000	NAUU	0.0
ZPM	600.0000	ZI	0.271000	AAABIP	6.627000	LAUU	0.0







[illegible]

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ALIGHT	104000	PSUB	507.4000	V	00.0	PSIR2	0.0
IX	50000	PLCB	451.1000	VELS	-5.0	VXSTR.	0.0
IV	50000	PLCB	451.1000	VSOUD	1117.0	VYSTR.	0.0
12	50000	TIME	0.20000000E-1	DEL3MM	0.0	VZSTR.	0.0
OMEGM	27.81999	ROSS	4.0	1-STM	-10.0	PSIR.	0.0
OMEGM	104.0000	ROSS	5.0	1-STM	-10.0	WLVT	273.0
KFR	15.0	PSSENT	1196.0	KLMT	230.0	FSVT	695.0
FSMT	104.0000	SMT	45.0	SVT	32.50000	USIR.	0.0
LATSTR	-0.1705209	AIS	-1.5046502	INT	13.105316	XA	45.132297
LONGSTR	5.0000000	AIS	4.2277621	IS	-3.0	XB	30.470793
CULSTR	15.0000000	THE1A	15.505026	TH7MM	5.505262	XC	31.906414
FEUAL	15.0000000	THE1M	21.404067	TH7STM	7.9046870	XP	39.025002
XALC	4.5152296	XBIN	3.0472793	XCIN	3.1926414	XPIR	2.1073320
XALCIP	35.041000	XBACTI	3.5041000	XCIN.	0.0	PSIR	0.0
VXB	101.25004	THE1AB	2.9602903	AAEP	3.0000109	QSTR	0.0
VVB	11.000000	PHIB	0.0	AAIP	-2.1070001	HSIR	0.0
VZB	5.2500000	ACTAMP	5.94005193	BDIP	0.00043504E-1	TITR	0.0
P	0.0	GMLC	0.0	AAVL	-3.4000591	MITR	0.0
Q	0.0	QCRAT	1.0	RAIL	0.16300091	JITR	0.0
R	0.0	PSUBOT	0.0	BDIL	0.94350420E-1	MMIR	0.0
ALPMP	-4.710700	ERAT	1.3790324	ERATX	0.09527561	LMIR	0.0
LMITPP	74.570511	ERATZ	1.0205009	ERATZ	1.0104294	UMIR	0.0
ERAT	0.0	ERAT	0.00040510	SIGMT	0.99002441	XITR	0.0
QMP	15.000000	KUMI	0.07177479	KUMI	0.00302914	VITR	0.0
MUXS	2.13985265	CTSIG	2.06511802E-1	LTOI	-2.5004282	ZITR	0.0
MUTS	2.10000000E-1	CHSIG	-0.16781210E-2	DIOI	25.144311	LITR	0.0
MUZS	-0.00000000E-4	CHSIG	0.00259199E-6	TTR	671.01545	MITR	0.0
LAFMR	-0.00000000E-1	NZ	0.94852628	MPM	959.27262	NITR	0.0
QKSMR	0.0019730E-1	VC	0.71525373E-5	KIRBLK	1.0	AXP	1.6530000
KMR	1100.0000	MDAM	-307.50026	VXBDUT	-0.79001090E-2	AYP	0.55300103E-3
ZMR	-205.05003	MDAM	205.05003	VXBDUT	0.12010900E-2	AZP	0.52120002
LMR	-13500.0000	MDAM	13502.903	VXBDUT	0.20245234E-2	VXP	101.25000
MMR	12400.0000	MDAM	-1350.2233	POOT	-0.31420000E-3	VYP	11.930227
NMR	10400.0000	MDAM	-5045.5029	QUOI	2.90001257E-4	VZP	5.2305291
KMP	-504.00000	KI	1920.274	WUOI	0.31234734E-4	NSIR.	0.0
YMP	-200.00000	YI	-22.003525	XIR	0.0	PSIUMG	0.0
ZMP	71.00000	ZI	-00.524726	YIR	0.0	BTM	0.0
LMR	500.00000	LI	-170.52101	ZIR	-229.12205	MAUU	0.0
MMR	-5051.0000	MI	-1912.6530	LIM	3005.0070	XADU	0.0
NMR	-2100.0000	KI	2751.2039	MIR	-7117.5197	YADU	0.0
XMI	-0.00000000E-1	XVI	-0.92003049E-1	NIR	-19555.351	ZADU	0.0
YMI	-1.1113025	YVI	-97.002344	ALFMIT	1.4701450	NAUU	0.0
ZMI	-0.00000000E-1	ZVI	0.10054725E-1	ACFYI	7.1200240	LRDU	0.0
				AA00IA	2.1000942		

404 11.

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0110010101

WEIGHT	10-21-77	30-000-77	0110010101	10-21-77	30-000-77	0110010101	10-21-77	30-000-77	0110010101
1A	10000.0	251.1442	282.2222	PCS	100	100	100	100	100
1B	30000.0	2.237022222E-2	282.2222	PCS	100	100	100	100	100
1C	30000.0	4.227022222E-1	282.2222	PCS	100	100	100	100	100
1D	30000.0	4.2	282.2222	PCS	100	100	100	100	100
1E	30000.0	5.2	282.2222	PCS	100	100	100	100	100
1F	30000.0	12.2	282.2222	PCS	100	100	100	100	100
1G	30000.0	42.4	282.2222	PCS	100	100	100	100	100
1H	30000.0	11.1791534	282.2222	PCS	100	100	100	100	100
1I	30000.0	7.440345	282.2222	PCS	100	100	100	100	100
1J	30000.0	15.25032	282.2222	PCS	100	100	100	100	100
1K	30000.0	22.012572	282.2222	PCS	100	100	100	100	100
1L	30000.0	2.222222	282.2222	PCS	100	100	100	100	100
1M	30000.0	2.4616224	282.2222	PCS	100	100	100	100	100
1N	30000.0	2.222222	282.2222	PCS	100	100	100	100	100
1O	30000.0	2.222222	282.2222	PCS	100	100	100	100	100
1P	30000.0	2.222222	282.2222	PCS	100	100	100	100	100
1Q	30000.0	2.222222	282.2222	PCS	100	100	100	100	100
1R	30000.0	2.222222	282.2222	PCS	100	100	100	100	100
1S	30000.0	2.222222	282.2222	PCS	100	100	100	100	100
1T	30000.0	2.222222	282.2222	PCS	100	100	100	100	100
1U	30000.0	2.222222	282.2222	PCS	100	100	100	100	100
1V	30000.0	2.222222	282.2222	PCS	100	100	100	100	100
1W	30000.0	2.222222	282.2222	PCS	100	100	100	100	100
1X	30000.0	2.222222	282.2222	PCS	100	100	100	100	100
1Y	30000.0	2.222222	282.2222	PCS	100	100	100	100	100
1Z	30000.0	2.222222	282.2222	PCS	100	100	100	100	100





RUN 14.

U1143(5/5) 1-21-77 30-AUG-77

HEIGHT	10000.0	FSCG	367.22700	V	142.0	PSIR2	0.0
1A	5627.0	ALG	251.10000	DELS	-5.0	VXSR	0.0
1Y	39395.0	RMD	0.23700000E-2	VSOUDU	1117.0	VYSR	0.0
1Z	37220.0	TIME	4.20000000E-1	DELJRM	0.0	VZSR	0.0
DMGWR	27.21399	NESS	4.0	TASMR	-10.0	PSTR	0.0
DMGTR	120.62700	NESS	5.0	TASMR	-10.0	ALVI	273.0
KFR	15.0	PASANT	524.0	HEHT	234.0	PST	0.0
FMT	100.40000	SMY	43.0	IMT	32.300000	ASTM	0.0
LATSTK	0.00000000E-1	ALB	-1.00000000E-1	IS	-3.0	XA	0.013922
LONGSTK	14.01723	DIS	14.092000	TH75M	9.3339032	XB	0.46917517
COLSTK	17.41593	THETA0	19.013903	TH75M	11.62568	XC	55.037146
PEUAL	14.40335	THETK	25.124508	XCIN	3.5037146	XP	41.672664
XAL	0.3015922	XBL	0.8917517E-1	ASTM	0.0	ASTM	0.0
XACIP	-0.00000000E-1	THETA0	0.00000000E-1	AAIP	3.2257503	ASTM	0.0
VIM	230.34101	PMID	2.0139001	BBIP	-0.0623431	ASTM	0.0
VIB	14.124404	BEYAP	3.3330075	AAEL	-2.31170425	ASTM	0.0
VZO	12.749002	GAEL	0.0	AAEL	-6.5747609	ASTM	0.0
D	0.0	DMGTR	1.0	AAEL	0.3250018	ASTM	0.0
R	0.0	PSI00T	1.0	AAEL	0.69611372	ASTM	0.0
ALPWR	0.00000000E-1	EAIX	1.5330333	EAIX	0.09200000	ASTM	0.0
CHLTPH	74.55335	EAIZ	1.7001000	EAIX	1.0100000	ASTM	0.0
EAIX	0.0	EPSAT	0.0033300	EAIX	0.5900000	ASTM	0.0
QAP	10.000000	QAP	0.0177979	QAP	0.5320000	ASTM	0.0
MUXS	0.00000000E-1	CTSIG	0.00000000E-1	CTSIG	0.00000000E-1	ASTM	0.0
MUS	0.00000000E-1	CHSIG	0.00000000E-1	CHSIG	0.00000000E-1	ASTM	0.0
MUS	0.00000000E-1	CHSIG	0.00000000E-1	CHSIG	0.00000000E-1	ASTM	0.0
LANDMR	0.00000000E-1	VC	0.00000000E-1	VC	0.00000000E-1	ASTM	0.0
DSHMR	0.00000000E-1	VC	0.00000000E-1	VC	0.00000000E-1	ASTM	0.0
KFR	15.0	MDAM	0.00000000E-1	MDAM	0.00000000E-1	ASTM	0.0
YMR	0.00000000E-1	YMR	0.00000000E-1	YMR	0.00000000E-1	ASTM	0.0
ZMR	0.00000000E-1	ZMR	0.00000000E-1	ZMR	0.00000000E-1	ASTM	0.0
LWR	0.00000000E-1	LWR	0.00000000E-1	LWR	0.00000000E-1	ASTM	0.0
MWR	0.00000000E-1	MWR	0.00000000E-1	MWR	0.00000000E-1	ASTM	0.0
NWR	0.00000000E-1	NWR	0.00000000E-1	NWR	0.00000000E-1	ASTM	0.0
YMR	0.00000000E-1	YMR	0.00000000E-1	YMR	0.00000000E-1	ASTM	0.0
ZMR	0.00000000E-1	ZMR	0.00000000E-1	ZMR	0.00000000E-1	ASTM	0.0
LWR	0.00000000E-1	LWR	0.00000000E-1	LWR	0.00000000E-1	ASTM	0.0
MWR	0.00000000E-1	MWR	0.00000000E-1	MWR	0.00000000E-1	ASTM	0.0
NWR	0.00000000E-1	NWR	0.00000000E-1	NWR	0.00000000E-1	ASTM	0.0
YMR	0.00000000E-1	YMR	0.00000000E-1	YMR	0.00000000E-1	ASTM	0.0
ZMR	0.00000000E-1	ZMR	0.00000000E-1	ZMR	0.00000000E-1	ASTM	0.0
LWR	0.00000000E-1	LWR	0.00000000E-1	LWR	0.00000000E-1	ASTM	0.0
MWR	0.00000000E-1	MWR	0.00000000E-1	MWR	0.00000000E-1	ASTM	0.0
NWR	0.00000000E-1	NWR	0.00000000E-1	NWR	0.00000000E-1	ASTM	0.0
YMR	0.00000000E-1	YMR	0.00000000E-1	YMR	0.00000000E-1	ASTM	0.0
ZMR	0.00000000E-1	ZMR	0.00000000E-1	ZMR	0.00000000E-1	ASTM	0.0
LWR	0.00000000E-1	LWR	0.00000000E-1	LWR	0.00000000E-1	ASTM	0.0
MWR	0.00000000E-1	MWR	0.00000000E-1	MWR	0.00000000E-1	ASTM	0.0
NWR	0.00000000E-1	NWR	0.00000000E-1	NWR	0.00000000E-1	ASTM	0.0
YMR	0.00000000E-1	YMR	0.00000000E-1	YMR	0.00000000E-1	ASTM	0.0
ZMR	0.00000000E-1	ZMR	0.00000000E-1	ZMR	0.00000000E-1	ASTM	0.0
LWR	0.00000000E-1	LWR	0.00000000E-1	LWR	0.00000000E-1	ASTM	0.0
MWR	0.00000000E-1	MWR	0.00000000E-1	MWR	0.00000000E-1	ASTM	0.0
NWR	0.00000000E-1	NWR	0.00000000E-1	NWR	0.00000000E-1	ASTM	0.0
YMR	0.00000000E-1	YMR	0.00000000E-1	YMR	0.00000000E-1	ASTM	0.0
ZMR	0.00000000E-1	ZMR	0.00000000E-1	ZMR	0.00000000E-1	ASTM	0.0
LWR	0.00000000E-1	LWR	0.00000000E-1	LWR	0.00000000E-1	ASTM	0.0
MWR	0.00000000E-1	MWR	0.00000000E-1	MWR	0.00000000E-1	ASTM	0.0
NWR	0.00000000E-1	NWR	0.00000000E-1	NWR	0.00000000E-1	ASTM	0.0
YMR	0.00000000E-1	YMR	0.00000000E-1	YMR	0.00000000E-1	ASTM	0.0
ZMR	0.00000000E-1	ZMR	0.00000000E-1	ZMR	0.00000000E-1	ASTM	0.0
LWR	0.00000000E-1	LWR	0.00000000E-1	LWR	0.00000000E-1	ASTM	0.0
MWR	0.00000000E-1	MWR	0.00000000E-1	MWR	0.00000000E-1	ASTM	0.0
NWR	0.00000000E-1	NWR	0.00000000E-1	NWR	0.00000000E-1	ASTM	0.0
YMR	0.00000000E-1	YMR	0.00000000E-1	YMR	0.00000000E-1	ASTM	0.0
ZMR	0.00000000E-1	ZMR	0.00000000E-1	ZMR	0.00000000E-1	ASTM	0.0
LWR	0.00000000E-1	LWR	0.00000000E-1	LWR	0.00000000E-1	ASTM	0.0
MWR	0.00000000E-1	MWR	0.00000000E-1	MWR	0.00000000E-1	ASTM	0.0
NWR	0.00000000E-1	NWR	0.00000000E-1	NWR	0.00000000E-1	ASTM	0.0
YMR	0.00000000E-1	YMR	0.00000000E-1	YMR	0.00000000E-1	ASTM	0.0
ZMR	0.00000000E-1	ZMR	0.00000000E-1	ZMR	0.00000000E-1	ASTM	0.0
LWR	0.00000000E-1	LWR	0.00000000E-1	LWR	0.00000000E-1	ASTM	0.0
MWR	0.00000000E-1	MWR	0.00000000E-1	MWR	0.00000000E-1	ASTM	0.0
NWR	0.00000000E-1	NWR	0.00000000E-1	NWR	0.00000000E-1	ASTM	0.0
YMR	0.00000000E-1	YMR	0.00000000E-1	YMR	0.00000000E-1	ASTM	0.0
ZMR	0.00000000E-1	ZMR	0.00000000E-1	ZMR	0.00000000E-1	ASTM	0.0
LWR	0.00000000E-1	LWR	0.00000000E-1	LWR	0.00000000E-1	ASTM	0.0
MWR	0.00000000E-1	MWR	0.00000000E-1	MWR	0.00000000E-1	ASTM	0.0
NWR	0.00000000E-1	NWR	0.00000000E-1	NWR	0.00000000E-1	ASTM	0.0
YMR	0.00000000E-1	YMR	0.00000000E-1	YMR	0.00000000E-1	ASTM	0.0
ZMR	0.00000000E-1	ZMR	0.00000000E-1	ZMR	0.00000000E-1	ASTM	0.0
LWR	0.00000000E-1	LWR	0.00000000E-1	LWR	0.00000000E-1	ASTM	0.0
MWR	0.00000000E-1	MWR	0.00000000E-1	MWR	0.00000000E-1	ASTM	0.0
NWR	0.00000000E-1	NWR	0.00000000E-1	NWR	0.00000000E-1	ASTM	0.0
YMR	0.00000000E-1	YMR	0.00000000E-1	YMR	0.00000000E-1	ASTM	0.0
ZMR	0.00000000E-1	ZMR	0.00000000E-1	ZMR	0.00000000E-1	ASTM	0.0
LWR	0.00000000E-1	LWR	0.00000000E-1	LWR	0.00000000E-1	ASTM	0.0
MWR	0.00000000E-1	MWR	0.00000000E-1	MWR	0.00000000E-1	ASTM	0.0
NWR	0.00000000E-1	NWR	0.00000000E-1	NWR	0.00000000E-1	ASTM	0.0
YMR	0.00000000E-1	YMR	0.00000000E-1	YMR	0.00000000E-1	ASTM	0.0
ZMR	0.00000000E-1	ZMR	0.00000000E-1	ZMR	0.00000000E-1	ASTM	0.0
LWR	0.00000000E-1	LWR	0.00000000E-1	LWR	0.00000000E-1	ASTM	0.0
MWR	0.00000000E-1	MWR	0.00000000E-1	MWR	0.00000000E-1	ASTM	0.0
NWR	0.00000000E-1	NWR	0.00000000E-1	NWR	0.00000000E-1	ASTM	0.0
YMR	0.00000000E-1	YMR	0.00000000E-1	YMR	0.00000000E-1	ASTM	0.0
ZMR	0.00000000E-1	ZMR	0.00000000E-1	ZMR	0.00000000E-1	ASTM	0.0
LWR	0.00000000E-1	LWR	0.00000000E-1	LWR	0.00000000E-1	ASTM	0.0
MWR	0.00000000E-1	MWR	0.00000000E-1	MWR	0.00000000E-1	ASTM	0.0
NWR	0.00000000E-1	NWR	0.00000000E-1	NWR	0.00000000E-1	ASTM	0.0
YMR	0.00000000E-1	YMR	0.00000000E-1	YMR	0.00000000E-1	ASTM	0.0
ZMR	0.00000000E-1	ZMR	0.00000000E-1	ZMR	0.00000000E-1	ASTM	0.0
LWR	0.00000000E-1	LWR	0.00000000E-1	LWR	0.00000000E-1	ASTM	0.0
MWR	0.00000000E-1	MWR	0.00000000E-1	MWR	0.00000000E-1	ASTM	0.0
NWR	0.00000000E-1	NWR	0.00000000E-1	NWR	0.00000000E-1	ASTM	0.0
YMR	0.00000000E-1	YMR	0.00000000E-1	YMR	0.00000000E-1	ASTM	0.0
ZMR	0.00000000E-1	ZMR	0.00000000E-1	ZMR	0.00000000E-1	ASTM	0.0
LWR	0.00000000E-1	LWR	0.00000000E-1	LWR	0.00000000E-1	ASTM	0.0
MWR	0.00000000E-1	MWR	0.00000000E-1	MWR	0.00000000E-1	ASTM	0.0
NWR	0.00000000E-1	NWR	0.00000000E-1	NWR	0.00000000E-1	ASTM	0.0
YMR	0.00000000E-1	YMR	0.00000000E-1	YMR	0.00000000E-1	ASTM	0.0
ZMR	0.00000000E-1	ZMR	0.00000000E-1	ZMR	0.00000000E-1	ASTM	0.0
LWR	0.00000000E-1	LWR	0.00000000E-1	LWR	0.00000000E-1	ASTM	0.0
MWR	0.00000000E-1	MWR	0.00000000E-1	MWR	0.00000000E-1	ASTM	0.0
NWR	0.00000000E-1	NWR	0.00000000E-1	NWR	0.00000000E-1	ASTM	0.0
YMR	0.00000000E-1	YMR	0.00000000E-1	YMR	0.00000000E-1	ASTM	0.0
ZMR	0.00000000E-1	ZMR	0.00000000E-1	ZMR	0.00000000E-1	ASTM	0.0
LWR	0.00000000E-1	LWR	0.00000000E-1	LWR	0.00000000E-1	ASTM	0.0
MWR	0.00000000E-1	MWR	0.00000000E-1	MWR	0.00000000E-1	ASTM	0.0
NWR	0.00000000E-1	NWR	0.00000000E-1	NWR	0.00000000E-1	ASTM	0.0
YMR	0.00000000E-1	YMR	0.00000000E-1	YMR	0.00000000E-1	ASTM	0.0
ZMR	0.00000000E-1	ZMR	0.00000000E-1	ZMR	0.00000000E-1	ASTM	0.0
LWR	0.00000000E-1	LWR	0.00000000E-1	LWR	0.00000000E-1	ASTM	0.0
MWR							



RUN 15.

30-AUG-77

1-21-77

UNITAS (316)

WEIGHT	16452.0	PSCG	367.20000	Y	130.0	PSIR2	0.0
IX	5624.3	ALC6	251.10000	DELS	-5.0	VXSTR	0.0
IY	39436.0	RHO	0.23780000E-2	VROUND	1117.0	VYSTR	0.0
IZ	31226.4	TIME	0.20000000E-1	DELSMR	0.0	VZSTR	0.0
OMEGMR	27.01949	MBSS	4.0	TOSTMR	-16.0	PSTR	0.0
OMEGTM	124.02000	NSSS	5.0	TWSTR	-10.0	MLVT	273.0
KFR	15.0	PASCNT	2030.0	KMT	238.0	PSVT	695.0
FSM	700.40000	SMT	45.0	SVT	32.500000	USTN	0.0
LAT..K	-1.2109364	AIS	-2.2362224	IMT	-5.9730025	XA	42.394147
LONGTA	14.143444	HIS	14.452325	IS	-3.0	XB	0.0
CULSTK	20.375400	TMETAW	20.375960	TM75MR	10.295960	XC	61.049755
PEUAL	14.544221	TMETTR	20.474374	TM75TH	12.974374	XP	41.131011
XAIR	0.2393136	XGIN	0.0	XGIN	0.1049733	XPIN	2.2210100
XBALTP	-2.5643120	XHAUT1	-0.25643120	XSTM	0.0	PSIN	0.0
VXB	293.40020	THETAB	1.4773135	AA0P	3.3300018	QSTM	0.0
VYB	14.040410	PHID	0.0	AA1P	-0.2157770	RSTM	0.0
VZB	0.5334400	BTAMP	3.2245004	BB1P	-0.400000300	TITN	0.0
P	0.0	GAMC	0.0	AA0L	-7.4034654	HITN	0.0
R	0.0	OMGRAT	1.0	AA1L	0.33227022	JITR	0.0
ALPWF	0.040000750E-1	PSIUOT	0.0	BB1L	0.09740340	MMITR	0.0
CHITPP	74.025034	EATX	1.5206000	EAPFX	0.00700196	LMITR	0.0
ERTH	0.0	EATZ	1.7193591	EAPFZ	1.0111743	QMITR	0.0
QKT	00.047013	CSMT	0.40224506	SIGMT	0.50752371	XITN	0.0
MUXS	0.34950049	KUMT	0.07177479	KQVT	0.03318073	YITN	0.0
MUS	0.20131710E-1	CTB6	0.71559172E-1	LTOT	2.3330423	ZITN	0.0
MUZS	0.20131710E-1	CHSIG	-0.04942716E-2	UTOT	24.232115	LITN	0.0
LAMHMY	-0.72910043E-2	CHMS16	0.53953460E-6	TTR	1505.2019	NITN	0.0
OMSMY	0.01947531E-2	NZ	1.0013401	MPMK	2004.9661	NITN	0.0
XMM	2373.5720	VE	0.33762700E-5	KTR0LA	1.0	AXP	0.43562390
ZMM	-350.30445	MBAR	-1506.8004	VABUOT	-0.15019201E-1	ATP	0.74062321E-1
LMH	-0044.3245	JBAM	356.54745	VABUOT	0.49338694E-1	APR	-31.541790
MMH	-7401.2022	LBAMH	-4522.0175	P0UT	0.23911131E-1	VTP	253.40020
NMH	34422.024	MBAMH	-22160.087	W0UT	0.26742863	VZP	6.5354040
XMP	-1404.5046	QBAR	40011.672	KUOT	0.30045154E-2	RSTM	0.0
YMP	-070.02903	XT	-73.294600	XTR	0.0	PSIOMG	0.0
ZMP	-107.40321	YI	-550.44000	YTR	1414.6074	0TR	2.0
LMF	1334.1402	ZI	1504.5410	ZTR	-514.07601	MADU	0.0
MMF	-9122.4000	LI	-636.00902	LTR	0075.5704	XADD	0.0
NMF	-3440.3450	MI	43712.000	MTR	-15952.575	YADD	0.0
XMT	-45.622444	NT	9491.0063	NTR	-43029.254	ZADD	0.0
YMT	-5.1107345	XVT	-27.676710	ALFMT1	-7.5906131	MADU	0.0
ZMT	1543.7534	YVT	-552.93215	ALFVT1	3.2762203	LADD	0.0
		ZVT	0.70500331	AA001F	0.2254461		

UTIAS(S76) 1-21-77 30-AUG-77 RUN 16.

WEIGHT	16050.0	FSCG	362.20000	V	150.0	PSITR2	0.0
IX	5624.0	MLCG	251.10000	DELS	-5.0	VASIR.	0.0
IY	39996.0	RMO	0.23780000E-2	V SOUND	1117.0	VZSTR.	0.0
IZ	3720.0	TIME	0.20000000E-1	DELSM	0.0	VZSTR.	0.0
ONEGMR	27.01999	NBS5	4.0	TMSTR	-18.0	PSTR.	0.0
ONEGTR	124.6200	NBS5	5.0	TMSTR	-16.0	MLVT	273.0
RFR	15.0	PASCT	3524.0	MLMT	234.0	PSVT	695.0
FSMT	700.00000	SMT	45.0	SVT	32.30000	USVM.	0.0
LATSTK	-1.4020172	AIS	-2.4751901	IMT	-8.0	XA	42.90092
LN6STA	19.14999	BIS	15.794999	IS	-3.0	AB	0.0
CULSTK	20.500920	THEIAB	20.500920	TH/SMR	10.42020	XC	52.660250
PEUAL	7.745170	THEITM	19.779001	TH/STM	0.270015	XP	40.127600
XAIN	4.000000	IBIN	0.0	XCIN	0.2550250	XPI.	3.2468111
XBACTP	-2.01.12010	XBACTI	-4.01012016	HSTM.	0.0	PSITP	0.0
VXB	253.20054	THEIAB	2.6700756	AA7F	3.3631001	GSTR	7.0
VVB	0.0	PHIO	-3.0700091	AA1F	-4.7505700	HSTM	0.0
VZB	11.426510	BETAMF	0.0	MB1F	-0.25602053	TITR	0.0
P	0.0	OMGRAT	0.0	AAVL	-7.5713495	MITM	0.0
R	0.0	PSIDUT	0.0	AXIL	0.3013042	JITR	0.0
ALPWF	1.1053970	ERTX	1.5121000	HAIL	0.8370000	MMTR	0.0
CHITPP	10.400007	ERTZ	1.7270333	ERKFX	0.00333333	LMITR	0.0
ERIN	0.0	EPSMT	0.0000000	ERKFX	1.0105133	UMITR	0.0
QMF	73.607007	KUMT	0.07177979	SIGMT	0.0	XITR	0.0
MUTS	0.33932004	CTSIG	0.71003972-1	KUVI	0.04052013	VITR	0.0
MUTS	0.0	CTSIG	-0.01625965E-2	LTOT	3.1300150	ZITR	0.0
LMBMK	-0.10700100E-1	CTSIG	0.50021024E-0	DTOT	23.935769	LITR	0.0
DMSMR	0.07900100E-2	VC	0.90015561	TIR	1504.0001	MITR	0.0
XW	270.0097	MDAN	-1093.9956	MPMK	2041.5004	NITM	0.0
YMR	500.27101	JMAN	303.27101	KTRBLK	1.0	AXP	1.1007903
ZMR	-10443.540	TMAN	16571.450	VXBUOT	0.15241701E-1	AYP	1.9002304
LMR	-0001.0200	LDANM	-3909.0001	VZBUOT	0.20443094E-1	ZXP	-31.071220
MMK	-10234.024	MDANM	-26103.517	PUOT	-0.37497759E-1	VXP	253.20054
NNK	4010.900	MDANM	41557.272	QUOT	0.23930309	VZP	11.026510
XMP	-1002.0141	XI	-119.20514	RUOT	-0.00477920E-2	HSTR.	0.0
YMP	0.0	YI	-100.20000	XIR	0.0	PSIUMG	0.0
ZMP	-209.50530	ZI	1674.2927	ZIR	1.13.0070	ZIR	0.0
LMP	0.0	LI	-194.33001	LIM	-514.40030	MADU	0.0
MPF	-7050.5050	MI	47349.750	MIR	-15934.904	XADD	0.0
NMP	0.0	NI	2973.9003	NIR	-43790.253	YADD	0.0
XMT	-07.524534	XVI	-31.975007	ALFMTI	-8.2950316	MADU	0.0
YMT	0.0	YVI	-100.20000	ALFMTI	0.0	LADD	0.0
ZMT	1074.1270	ZVI	0.10500250	AA001P	9.7534000		

UN 19.

UTIAS(3/0) 1-21-77 30-000-77

HEIGHT	1007.0	FSCU	30020000	Y	1-00-2	PSIRE	0.0
IX	5027.4	MLCG	251.14000	UELS	-5.0	VXSTR	0.0
IY	3996.0	RMO	0.23780000E-2	VSDUO	1117.0	VYSTR	0.0
IZ	3725.0	TIME	0.20000000E-1	UELJRM	0.0	VZSTR	0.0
ORCUM	27.01494	NOSS	4.0	TMSIM	-10.0	PSIR	0.0
ORCUM	124.62000	NSSS	5.0	TASIM	-10.0	MLVT	273.0
KPR	15.0	PASCT	965.0	ALMT	234.0	PSVT	0.0
FMT	700.00000	SMT	45.0	SVT	32.30000	USTM	0.0
LATSK	0.13915020	ALS	0.00000000	IMT	27.291733	XA	0.0
LNSTK	0.70000001	OLS	2.1156757	IS	-5.0	XB	33.079601
COLSK	17.070070	TMETAB	17.070070	TWJRM	7.5909703	XC	0.0
PEUAL	22.000000	TMETAB	31.000000	TWJRM	17.5909703	XP	19.340724
XALN	0.000000	XOIN	3.000000	XCIN	0.000000	XPIN	1.000000
XBALP	34.000000	XOACTI	3.000000	RSIM	0.0	PSIR	0.0
VXB	0.10027120E-1	TMETAB	5.2019950	AAOP	3.2090005	QSTR	0.0
VVB	0.0	PHIB	-2.7172532	AAIP	-2.2552740	RSTR	0.0
VZB	0.13557530E-2	DETAMP	0.0	DDIP	-1.0000000	TITM	0.0
P	0.0	GALC	0.0	AAUL	-5.0143962	MITH	0.0
Q	0.0	OMGRAT	1.0	AAUL	0.0000000	JITR	0.0
R	0.0	PSIUOT	0.0	AAUL	0.1420000	MITH	0.0
ALFAP	0.00000000	ERTX	-0.24000000	EMTX	0.79900000E-5	LMITH	0.0
CMITPP	-2.2200750	ERTZ	0.20000000	EMTX	0.11000000E-3	OMITH	0.0
ERTM	0.0	EPSMT	0.00000000	SIGMT	0.0	XITR	0.0
QAP	0.35000000E-6	KUMT	0.0717799	KUMT	0.00000000	VITM	0.0
MU25	0.00000000E-6	GTSIG	0.00000000E-1	LTOI	-11.500000	ZITR	0.0
MU25	0.00000000E-6	CHSIG	0.00000000E-2	UTOI	24.780000	LITR	0.0
LARDM	-0.55000000E-1	NZ	0.52000000E-6	TIM	1052.0000	MITH	0.0
ORCUMH	0.35000000E-1	VC	0.90000000	MPHM	1533.0000	NITH	0.0
XRM	1001.0000	MBAM	-0.00000000E-3	KIMOLK	0.79500000	AKP	2.9737004
YRM	-0.35000000E-1	MBAM	-0.00000000E-3	VXUOT	0.12015914E-1	AYP	1.5520023
ZRM	-0.35000000E-1	MBAM	-0.00000000E-1	VXUOT	0.12015914E-1	AYP	-31.997351
LMH	0.00000000	LOAMH	15253.712	VZUOT	-0.17000000E-3	VXP	0.16027120E-1
MMH	0.00000000	LOAMH	-0.00000000E-3	DUOI	-0.24000000E-3	VYP	0.0
NMH	0.00000000	LOAMH	-0.00000000E-3	DUOI	0.34140150E-4	VZP	0.15557353E-2
XAP	0.00000000	XT	3.00000000	XTM	0.0	PSIDMG	0.0
YAP	0.00000000	YI	0.00000000	YITR	0.0	BTM	0.0
ZAP	0.00000000	ZI	0.00000000	ZITR	-359.0000	MAUU	0.0
LMF	0.00000000	LI	-0.00000000E-6	LITR	5644.0000	XADD	0.0
MMF	0.00000000	MI	164.000000	MITR	-11149.0000	YADD	0.0
NMF	0.00000000	NI	0.15236000E-4	NITR	-30632.0000	ZADD	0.0
XMT	0.00000000	XVI	-0.15000000E-6	ALFMTI	-11.565600	NADD	0.0
YMT	0.00000000	YVI	-0.15000000E-6	ALFMTI	-11.565600	NADD	0.0
ZMT	0.00000000	ZVI	0.00000000E-7	ALFMTI	-11.565600	LADD	0.0

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WEIGHT	16932.0	FSCG	360.22000	V	00.0	PSIR2	0.0
IX	5629.0	WLCU	251.10300	UELS	-5.0	VXSTR	0.0
IY	54995.0	RMU	0.2570000E-2	VUUND	1117.0	VZSTM	0.0
IZ	37225.0	TIME	0.2600000E-1	DELSM	0.0	VZSTM	0.0
OMEGMR	27.01999	NOSS	4.0	TKSTM	-10.0	PSIR	0.0
OMEGTK	124.02000	NSS	5.0	TKSTM	-10.0	MLVT	273.0
KPR	15.0	PASCENT	001.0	MLMT	238.0	PSVT	693.0
FSMT	700.00000	SMT	45.0	SVT	32.50000	USTH	0.0
LATSTK	-1.5300000	AIS	-1.9331970	IMT	20.600257	XA	41.506922
LANGSTK	4.7000000	BIS	3.4650076	IS	-5.0	XB	53.392050
CULSTK	16.059207	TMETAG	16.059207	TM7SM	5.9752077	XC	34.045549
PEUAL	15.022117	TMETM	22.512402	TM7STM	8.8124620	XP	30.295304
XAIN	4.1570977	XBIN	3.3392030	XCM	3.4045540	XPIN	2.0670926
XDACIP	34.700254	XBALTI	3.9705254	XSTM	0.0	PSIM	0.0
VX0	67.451625	TMETAB	3.7109304	AAP	3.1779036	USTM	0.0
VY0	0.0	PHIB	-1.3755022	AAIP	-2.1609907	RSTM	0.0
VZM	4.5009944	BETAMP	0.0	BBIP	-0.57040507E-1	TSTM	0.0
P	0.0	GAMC	0.0	AAOL	-3.9097695	MITR	0.0
Q	0.0	OMGRAT	1.0	AAIL	0.17702203	JTR	0.0
R	0.0	PSIDOT	0.0	BBIL	0.93903679E-1	MMTR	0.0
ALPAP	-11.710045	ERIX	1.1067570	EMPA	0.74902454	LMTR	0.0
CHITPP	76.020015	ERIZ	2.0471702	EMFZ	1.0191791	OMTR	0.0
ERTH	0.0	EPSWT	0.44999994	SIGMT	0.0	XSTM	0.0
QAP	0.0000000	KGMT	0.87177979	KVIT	0.84852013	YSTM	0.0
MUS	0.9323029E-1	CTSIG	0.67043795E-1	LTOT	-17.125224	ZSTM	0.0
MUTS	0.0	CMSIG	-0.10135049E-2	UTOT	25.091920	LSTM	0.0
LAMBDM	0.11701057E-2	CMMSIG	0.51040109E-0	TIR	753.10004	MITK	0.0
OMSMH	0.20527250E-1	NZ	0.94759151	MPMM	1094.0931	MITK	0.0
MM	1234.5000	MOAN	0.90019500E-1	KTMOLK	1.0	AXP	2.0930740
YMN	-312.07112	YMAN	312.07112	VIBOUT	0.44303659E-2	AYP	0.74567910
ZMN	-13512.517	YMAN	15556.069	VIBOUT	0.20990700E-1	AZP	-32.094502
LMN	-4024.7051	LBARM	-1106.5054	PUOT	0.20230100E-2	VXP	67.457605
MMN	15096.007	MOARM	-5025.9296	QUOT	0.6320447E-3	VYP	0.0
NNN	21778.505	MOARM	22500.000	RUOT	0.16542000E-2	VZP	4.3044944
KPP	-194.03527	XI	-21.439400	XTK	0.0	PSIMG	0.0
YPP	0.0	YI	0.75039330	YTR	707.79963	BTR	2.0
ZPP	195.74430	ZI	-24.106270	ZTR	-257.61049	MADU	0.0
MP	0.0	LT	-13.000715	LTR	0.000.0101	XADD	0.0
NP	-0322.0019	MT	-766.70034	MTR	-7901.0797	YADD	0.0
NPP	0.0	NI	211.54230	NTM	-21424.991	ZADD	0.0
XMT	-14.507154	XVT	-2.0517255	ALFMTI	0.94644004	NADD	0.0
YMT	0.0	YVT	0.75039330	ALFMTI	0.0	LADD	0.0
ZMT	-27.159405	ZVI	0.90319204	AAADDI	2.1697700		



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UTIAS(S75)

EIGHT	19422.7	F5C6	347.0	Y	02.0	PS1RZ	0.2
ALC6	246.29999	UCLD	-5.0			VS1R.	0.0
PMO	0.1750002PE-2	VSOUND	1077.0			VS1R.	0.0
TIME	4.20000000E-1	VELSHM	0.0			VS1R.	0.0
WSS	4.0	TAS1M	-10.0			VS1R.	0.0
NSS	5.0	TAS1M	-10.0			VS1R.	0.0
PASCT	1135.0	WMT	234.0			VS1R.	0.0
SM	45.0	SVT	52.500000			VS1R.	0.0
AT1SK	-1.0040701	IMT	11.251416			VS1R.	0.0
PLS	3.6427600	IS	-3.0			VS1R.	0.0
ULSTK	19.120320	TM7SHM	9.0003200			VS1R.	0.0
UEAL	10.476215	TM7SHM	13.500260			VS1R.	0.0
AFIN	3.5072558	XCIN	3.0002000			VS1R.	0.0
ADALTI	3.7000950	PS1M.	0.0			VS1R.	0.0
TMETAB	-0.11521810	AAAP	4.1900279			VS1R.	0.0
PHIO	0.0	AAIP	1.1215078			VS1R.	0.0
RETAAP	0.4136710	BBIP	0.20230413			VS1R.	0.0
GAML	0.0	AAUL	-4.0543329			VS1R.	0.0
CEGFAT	1.0	AAUL	0.1773500			VS1R.	0.0
PS1001	0.0	BBIL	-0.10569161			VS1R.	0.0
ERTX	1.2437349	ERAPX	0.90007703			VS1R.	0.0
ERTZ	1.9312140	ERAPZ	1.0096001			VS1R.	0.0
EP9MT	0.49413072	SIGMT	0.77000012			VS1R.	0.0
KMT	0.07177979	KQVI	0.62746034			VS1R.	0.0
CT816	0.11220029	L10T	-0.53000004			VS1R.	0.0
CM516	0.54612701E-2	O10I	25.000002			VS1R.	0.0
CM510	0.91597212E-0	TIR	920.00009			VS1R.	0.0
MC	1.00000794	MPHM	1324.2941			VS1R.	0.0
VC	0.44723005E-0	KTMELK	1.0			VS1R.	0.0
MBAM	551.05517	VADUOI	0.10556100E-1			VS1R.	0.0
JBAM	525.05020	VADUOI	-0.17707092E-2			VS1R.	0.0
TOAM	19100.390	VADUOI	-0.55434591E-2			VS1R.	0.0
LOAMM	-979.72601	POUT	0.12001001E-2			VS1R.	0.0
MOAMM	3059.1022	MOUI	-0.12110305E-3			VS1R.	0.0
UOAR	20956.594	MOUI	-0.003400703E-3			VS1R.	0.0
XT	55.701045	XIR	0.0			VS1R.	0.0
YT	-105.31015	YIR	0.00003038			VS1R.	0.0
ZI	200.50904	ZIR	-314.70322			VS1R.	0.0
LI	-225.49591	LIR	5201.0107			VS1R.	0.0
MI	5950.9072	MIR	-10096.720			VS1R.	0.0
NI	2900.7753	NIR	-27702.479			VS1R.	0.0
AVT	-0.0000000	ALFMT	-5.4000123			VS1R.	0.0
VVT	-0.0000000	ALFMT	-5.4000123			VS1R.	0.0
ZVT	0.7400000	AA001P	1.1515974			VS1R.	0.0



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RUN 40.

WEIGHT	19900.0	FSCG	347.0	V	120.0	PSITR2	0.0
IX	6268.0	MLCG	246.29999	DEL3	-5.0	VXSTR.	0.0
IY	41587.0	RMO	0.17500000E-2	VROUND	1077.0	VYSTR.	0.0
IZ	50224.0	TIME	0.20000000E-1	DELSHM	0.0	VZSTR.	0.0
OMECHR	27.01999	NRSS	4.0	THSTMR	-10.0	PSTR.	0.0
OMEGR	124.62000	NRSS	5.0	THSTTR	-10.0	WLVT	273.0
KPR	15.0	PASCNT	1426.0	WLMT	234.0	PVST	695.0
FSMT	700.40000	SWT	45.0	SVT	32.50000	OSTR.	0.0
LATSTR	-1.4515740	AIS	-2.5100297	IS	1.0064000	XA	40.927602
LNGSTR	0.7152465	BIS	0.2150732	IS	-3.0	XB	19.204075
COLSTR	20.033939	THETAB	20.033939	TH7MR	10.753939	XC	64.712119
PEUAL	17.907529	THETTR	30.372256	TH7STR	16.072256	XP	31.040719
XAIN	4.0927662	XBIN	1.9200075	XCIN	6.4712119	XPIN	1.7197061
XBACTP	10.199071	XBACTI	1.0190071	RSTR.	0.0	PSTR	0.0
VX0	202.79070	THETAB	-0.17211994	AA0P	4.1757097	OSTR	0.0
VY0	13.033174	PHI0	0.0	AA1P	-0.64405510	RSTR	0.0
VZ0	-0.00915195	BETAMP	3.4670001	BB1P	0.24050512	TSTR	0.0
P	0.0	GAMC	0.0	AA0L	-6.9727763	MITR	0.0
Q	0.0	OMGRAT	1.0	AA1L	0.33900220	JSTR	0.0
R	0.0	PSIDOT	0.0	BB1L	-0.12796733	MMTR	0.0
ALPMP	-3.5290074	ERTX	1.1530915	EKMPX	0.93457266	LMTR	0.0
CHITPP	82.659437	EKTZ	1.7061266	EKMP2	1.0073405	OMTR	0.0
EKTR	0.0	EPST	0.4607000	SIGMT	0.01033204	XSTR	0.0
OMF	40.503635	KOHT	0.0717799	KOVT	0.03202010	YSTR	0.0
MUX3	0.27920204	CT810	0.11394292	LTOT	-1.0470007	ZSTR	0.0
MUY3	0.17978117E-1	CHS10	0.95150750E-3	DTOT	24.273359	LSTR	0.0
MUZ3	-0.15070049E-1	COMS10	0.91104967E-6	TTR	1329.0072	MITR	0.0
LAMBHR	-0.3271971E-1	NZ	0.99998516	MPMR	1073.0374	NSTR	0.0
DM3HR	0.17293321E-1	VC	0.15411045E-3	KTRBLK	1.0	AXP	-0.11447095
XMR	0.56.00106	HBAR	162.47593	VX8DOT	-0.15454646E-1	AYP	0.36919009E-2
YMR	-0.90.50306	JBAR	0.96.50306	VY8DOT	0.26540090E-2	AZP	-32.100502
ZMR	-19436.003	TBAR	19456.476	VZ8DOT	-0.99792160E-3	VXP	202.79070
LMR	-7000.0420	LBARM	-1735.7143	POOT	-0.4002445E-3	VYP	13.833174
MMR	3217.4670	HBARM	-1467.5361	QOOT	0.14413370E-2	VZP	-0.60915195
NMR	37045.441	QBAR	30142.510	ROOT	-0.53617964E-3	RSTR.	0.0
XMP	-957.00477	XT	35.104295	XTR	0.0	PSIDMG	0.0
YMP	-306.44471	YT	-103.59337	YTR	1249.7701	STR	2.0
ZMP	134.10066	ZT	609.70173	ZTR	-454.00293	MADD	0.0
LMP	049.70003	LT	-399.30505	LTR	7634.5206	XADD	0.0
MP	-0362.0562	MT	19700.090	MTR	-14594.160	YADD	0.0
NMP	-2001.5333	NT	5313.7570	NTR	-60097.848	ZADD	0.0
XMT	46.097096	XVT	-11.792000	ALPMTT	-6.4000007	MADD	0.0
YMT	-2.5550059	YVT	-100.03970	ALPYTT	3.0040720	LADD	0.0
ZMT	660.24057	ZVT	1.5331025	AAB1F	0.69030341		



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UTIAS(876)

HEIGHT	1900.0	PSCG	347.0	Y	140.0	PSIR2	0.0
IX	6260.0	HLCG	246.29999	DELS	-5.0	VXSTR.	0.0
IY	41507.0	RMO	0.1750000E-2	VROUND	1077.0	VYSTR.	0.0
IZ	30224.0	TIME	0.2000000E-1	DEL3MR	0.0	VZSTR.	0.0
OMEGMR	27.01999	MS3	4.0	TMSTR	-10.0	PSIR.	0.0
OMEGTR	124.62000	MS3	5.0	TMSTR	-10.0	HLVT	273.0
KPR	15.0	PASCNT	5335.0	MLMT	234.0	PSVT	0.0
PSMT	700.40000	BMT	45.0	SVT	32.30000	QSTM.	0.0
LATSTR	-5.0977994	A10	-7.3700114	INT	-2.5045345	XA	13.157503
LNGSTR	14.14999	B10	11.596751	IS	-3.0	XB	0.0
COLSTR	24.000271	THETAB	24.000271	TM75MR	10.720271	XC	0.0
PEDAL	29.430000	THETTR	37.5	TM75TR	24.0	YP	0.0
XAIR	1.3137303	XBIN	0.0	XCIN	0.9551599	XTN	0.0
XBACTP	-2.9932616	XBACTI	0.0	RSTR.	0.0	PSIR	0.0
VXB	236.50000	THETAB	-1.5777704	AAOF	4.1633709	OSTR	0.0
VYS	-30.033740	PHIO	-7.2900511	AAIF	-1.4350900	RSTR	0.0
VZB	-6.5145040	BETAMP	-7.1350002	BBIF	0.22234500	TSTR	0.0
P	0.0	GAMC	0.0	AAEL	-13.660769	MSTR	0.0
Q	0.0	UMGRAT	1.0	AXIL	0.79103796	JSTR	0.0
R	0.0	PSIDOT	0.0	BBIL	-0.05519365E-1	MMSTR	0.0
ALPMP	-4.0327025	EKTX	1.2669090	EKMPX	0.91012247	LMSTR	0.0
CHITPP	01.59030	EKTZ	1.0045203	EKMFX	1.0006059	OMSTR	0.0
EKTR	0.0	EPBMT	0.39140500	SIOMT	-1.1445599	XSTR	0.0
QMP	54.211793	KOMT	0.6717799	KQVI	0.04474472	YSTR	0.0
MUXB	0.3250902	CT810	0.1149000	LTOI	-0.55910022	ZSTR	0.0
MUYB	-0.42015195E-1	CH81G	0.23110274E-2	DTOT	25.660120	LSTR	0.0
MUZB	-0.20040417E-1	COM810	0.90073004E-0	TTR	2355.2705	MSTR	0.0
LAMBMR	-0.40900902E-1	NZ	0.99247031	MAPH	3617.7676	NSTR	0.0
DMSMR	0.14030404E-1	VC	-230.00007	KTRBLK	1.0	AXP	-1.1709210
XMR	632.74963	MBAR	394.62250	VXBDOF	-0.3755442E-1	AYP	4.0036740
YMR	-1140.1504	JOAR	1140.1504	VYBDOF	-0.34430007E-2	AZP	-31.042940
ZMR	-19612.246	TBAR	19620.006	VZBDOF	-0.34134000E-1	VAP	230.50060
LMR	-12303.712	LBARM	-1079.3044	PDOT	-0.53451592E-3	VVP	-30.093740
MMR	3064.0991	MBARM	-3041.3592	ODOT	0.13654170	VZP	-6.5145040
NMR	72067.030	QBAR	73040.719	RDOT	0.13637000E-2	RSTR.	0.0
XMP	-1277.2057	XT	96.603241	XTR	0.0	PSIDMG	0.0
YMP	1041.2901	YT	319.07490	YTR	2213.0026	OSTR	0.0
ZMP	120.07104	ZT	1352.9633	ZTR	-005.61410	MADD	0.0
LMP	-1022.0229	Lt	070.07309	LTR	13921.012	XADD	0.0
MPF	-11472.569	MT	39953.217	MTR	-25046.707	YADD	0.0
NMP	7474.0097	NT	-9275.0505	NTR	-71013.320	ZADD	0.0
XMT	93.500147	XVT	3.3350944	ALFMTT	-9.7356432	MADD	0.0
YMT	9.9701075	YVT	309.70075	ALFVTT	-7.007470	LADD	0.0
ZMT	1353.3017	ZVT	-0.41062602	AAB01F	1.4522203		

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UTIAS(876)

WEIGHT	1988.0	PSC6	347.0	V	148.0	P81TR2	0.0
IX	6260.0	WLCG	246.20999	DELS	-5.0	VXSTR.	0.0
IY	41567.0	RMO	0.17500000E-2	V8OUND	1077.0	VYSTR.	0.0
IZ	30220.0	TIME	0.20000000E-1	DELJMH	0.0	VZSTR.	0.0
OMEGMR	27.019999	N883	4.0	TMSTR	-10.0	PSTR.	0.0
OMEGTR	124.02000	N883	5.0	TMSTR	-10.0	MLVT	273.0
KFR	15.0	PASCNT	3300.0	NCMT	234.0	PSVT	095.0
FSMT	700.00000	8MT	45.0	SVT	32.300000	QSTR.	0.0
LATSTR	-2.7937071	A18	-4.1207063	IMT	1.3654796	XA	32.530030
LANGTK	13.317537	B18	10.350337	IS	-3.0	XB	2.9415645
COLSTR	23.403344	THETA5	23.403344	TH75MR	13.321344	XC	00.759654
PEDAL	29.430000	THETTR	37.5	TH75TR	24.0	XP	0.0
XAIN	3.2530030	XBIN	0.2943044	XCIN	0.0759034	XPIN	0.0
XBACTP	-0.27001334	XBACTI	-0.27001334E-1	RSTR.	0.0	PSTR	0.0
VXD	236.43033	THETAB	-2.1040332	AADP	4.1463573	QSTR	0.0
VY0	14.601174	PHIO	0.0	AAIP	-0.36072520E-2	RSTR	0.0
VZ0	-0.9309413	DETAMP	3.3951360	BBIP	0.23010071	TITR	0.0
P	0.0	GAMC	0.0	AACL	-11.040039	HITH	0.0
0	0.0	OMGRAT	1.0	AAIC	0.5451592	JITR	0.0
R	0.0	P81UOT	0.0	BBIL	-0.27500045	MHITR	0.0
ALFMP	-0.5900224	EXTX	1.1571344	EMFX	0.92904707	LHITR	0.0
CHITPP	02.23452	EKTZ	1.0295311	EKMF2	1.0077656	QHITR	0.0
EXTR	0.0	EP8MT	0.40355136	8IGMT	0.59754000	XITR	0.0
OWP	53.607619	KQMT	0.07177979	KQVT	0.03230945	VITR	0.0
MUX9	0.3250240	CT910	0.11401401	LIOI	-3.1595724	ZITR	0.0
MUY0	0.20231307E-1	CH810	0.3121903E-2	DTOI	24.259027	LITR	0.0
MUZ9	-0.29370511E-1	CGM810	0.94504301E-6	TIR	1966.9571	MITR	0.0
LAMBHR	-0.4427296E-1	NZ	0.99871239	MPHM	2926.9025	NITR	0.0
DW8MHR	0.14090704E-1	VC	0.14305114E-4	KTR0LK	1.0	AXP	-1.2240703
XMR	491.07795	H0AR	533.13370	V8UOT	0.10355520E-1	AYP	-0.23140060
YMR	-1120.0393	JUAR	1120.0393	VYUOT	0.13010041E-1	AZP	-32.133720
ZMR	-19570.629	T0AR	19571.070	VZUOT	0.1944039E-1	VXP	236.43033
LMR	-11725.000	LBARM	-1925.0091	PDOT	0.11060001E-1	VYP	14.601174
HMR	7327.2340	H0ARM	402.20029	QDOT	-0.17022060E-2	VZP	-0.9369413
NMR	50027.744	0BAR	59579.100	RDOT	0.74430744E-1	RSTR.	0.0
XMP	-1250.5901	XT	56.611196	XTR	0.0	P81DMG	0.0
YMP	-477.01494	YT	-242.02099	YTR	1040.4725	0TR	2.0
ZMP	271.39555	ZT	900.60250	ZTR	-672.79027	MADD	0.0
LMP	060.05097	LT	-529.09778	LTR	11291.745	XADD	0.0
MPF	-12602.717	MT	26069.543	MTR	-21505.354	YADD	0.0
NMP	-3747.5035	NT	7043.5014	NTR	-59305.159	ZADD	0.0
XMT	73.230040	XVT	-16.62052	ALFMTT	-6.6312555	MADD	0.0
YMT	-3.310021	YVT	-239.750439	ALFVT?	3.5440033	LADD	0.0
ZMT	906.20735	ZVT	2.3351552	AAB0IF	0.23022003		

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UTIAS(S76)

MEIGHT	19400.0	FSCG	360.20000	V	1.0E-2	PSITR2	0.0
IX	6200.0	RLCG	246.29999	DELS	-5.0	VXSTR.	0.0
IY	41507.0	RLC	0.17500000E-2	VSOUND	1077.0	VYSTR.	0.0
IZ	30225.0	TIME	0.20000000E-1	DEL3MM	0.0	VZSTR.	0.0
OMEGMR	27.019994	NDSS	4.0	TMSTM	-18.0	PSTR.	0.0
OMEBTR	124.02240	MSSS	5.0	TMSTTR	-10.0	PLVT	273.0
KFR	15.0	PASLMT	1955.0	ALMT	234.0	FST	645.0
FSMT	700.00000	SMT	45.0	IS	34.0	QSTR.	0.0
LATSTR	-0.31014607E-1	AIS	-1.1332193	IMT	-3.0	XA	49.006127
LONGSTR	5.4019007	BIS	2.3931239	IS	-3.0	XB	20.002329
COLSTR	21.237270	THETA	21.237270	TM75MR	11.157270	XC	67.232993
PEDAL	29.030000	THETR	37.5	TM75TR	24.0	XP	0.0
XAIN	4.9006120	XBIN	2.0006230	XCM	6.7232992	XPIN	0.0
XOACTP	35.904103	XOACTI	3.5906103	RSTR.	0.0	PSTR	0.0
VXB	0.10015904E-1	THETAB	5.7941446	AAIF	4.3546563	RSTR	0.0
VYB	0.0	PMIB	-2.0021572	AAIF	-2.0074254	RSTR	0.0
VZB	0.17062107E-2	BETAMF	0.0	AAIF	-1.2010031	YSTR	0.0
P	0.0	GAML	0.0	AAEL	-7.9267669	YSTR	0.0
Q	0.0	DMGRAT	1.0	AAEL	0.10031475E-1	YSTR	0.0
R	0.0	PSIDOT	0.0	AAEL	0.21602560	YSTR	0.0
ALTRF	-12.444623	EXTA	-0.22019296	AAEL	0.79599999	YSTR	0.0
CHITPP	-2.50304750	EXTZ	0.16975012	AAEL	0.22517277E-2	YSTR	0.0
EXTM	0.0	EPSMT	0.44999999	AAEL	-2.23705512E-3	YSTR	0.0
QWF	0.27101449E-6	KUMT	0.07177979	AAEL	0.90533240E-3	YSTR	0.0
MUS	0.23202900E-4	CTSIG	0.10930117	AAEL	0.19530034E-4	YSTR	0.0
MUS	0.0	CHSIG	-0.55720034E-2	AAEL	0.26190063	YSTR	0.0
MUS	0.11303509E-5	CUMSIG	0.95050930E-6	AAEL	0.0	YSTR	0.0
LABMR	-0.00420450E-1	NZ	0.99002036	AAEL	0.16665292	YSTR	0.0
DM3MR	0.00420450E-1	VC	0.91734233E-4	AAEL	-300.10566	YSTR	0.0
XMR	1420.4540	MDAR	-951.57102	AAEL	6515.1079	YSTR	0.0
YMR	-269.23567	JBAR	269.23567	AAEL	-12027.205	YSTR	0.0
ZMR	-10207.040	TBAR	10663.067	AAEL	-33244.031	YSTR	0.0
LMR	-7100.6069	LBARM	-3213.6656	AAEL	-2.9223661	YSTR	0.0
MMR	11900.504	MDARM	-7191.7030	AAEL	0.0	YSTR	0.0
NMR	43000.751	QBAR	43732.609	AAEL	0.0	YSTR	0.0
XMP	-0.50000340E-5	XT	0.00140039	AAEL	0.0	YSTR	0.0
YMP	0.0	YT	-6.3037330E-6	AAEL	0.0	YSTR	0.0
ZMP	0.00007010E-5	ZT	1.3650773	AAEL	0.0	YSTR	0.0
LMP	0.0	LT	-0.77735500E-6	AAEL	0.0	YSTR	0.0
MPF	-0.13596191E-3	MT	39.594299	AAEL	0.0	YSTR	0.0
NMP	0.0	NT	0.97475174E-5	AAEL	0.0	YSTR	0.0
XMT	0.00140040	XVT	-0.03705925E-7	AAEL	0.0	YSTR	0.0
YMT	0.0	YVT	-0.34937330E-6	AAEL	0.0	YSTR	0.0
ZMT	1.3050773	ZVT	0.62959520E-7	AAEL	0.0	YSTR	0.0

UTIAS(S76) 1-21-77 16-SEP-77 JUN 29.

WEIGHT	19902.0	FSCG	300.20002	V	DEL8	62.0	PSITR2	0.0
IX	6200.0	MLC6	246.24999	DEL8	VSOUND	-5.0	VXSTR.	0.0
IY	41507.0	KMD	0.17500000E-2	VSOUND	1077.2	1077.2	VYSTR.	0.0
IZ	30224.0	TIME	0.20000000E-1	DEL3MH	0.0	0.0	VZSTR.	0.0
OMELMH	27.01999	NDS	0.0	TSSTM	-10.0	-10.0	PSTR.	0.0
OMESTR	124.62002	NDS	5.0	TSSTM	-10.0	-10.0	PLVT	273.0
KFM	15.0	PASCT	755.0	PLMT	234.0	234.0	PSVT	695.0
FSMT	700.00000	SMT	45.0	SVT	32.30000	32.30000	USTR.	0.0
LATSTK	-1.115414	AIS	-1.9950204	IMT	25.092047	25.092047	XA	43.825365
LNSTK	6.5124020	SIS	5.0023202	IS	-3.0	-3.0	XB	27.692642
COLSTK	19.014024	THETA0	19.014024	TH75MH	0.9340240	0.9340240	XC	55.342655
PEDAL	10.077509	THETM	20.919299	TH75TH	15.419299	15.419299	XP	24.025044
XAIN	4.5025365	XBIN	2.7092942	XCIN	5.3342655	5.3342655	XPIN	1.6105105
XOACTP	32.220000	XOACTI	3.2200000	RBTH.	0.0	0.0	PBTM	0.0
YB	101.26533	THETA0	2.0007927	AA0F	4.1725906	4.1725906	USTM	0.0
YB	15.075009	PHI0	0.0	AA1F	-1.4466630	-1.4466630	RSTM	0.0
VZB	5.0747045	DELTA0F	7.0365960	BB1F	-0.5140017E-1	-0.5140017E-1	TITR	0.0
P	0.0	GAC	0.0	AA0L	-5.0546674	-5.0546674	MITM	0.0
Q	0.0	OMGAT	1.0	AA1L	0.25339599	0.25339599	JITR	0.0
R	0.0	PBI00T	0.0	BB1L	-0.13486923E-1	-0.13486923E-1	MMITR	0.0
ALPWF	-0.0060320	ERTX	1.2401020	EMPFX	0.04913022	0.04913022	LMITR	0.0
CHITTP	75.575059	ERTZ	1.9573018	EMPTZ	1.0146241	1.0146241	CHITR	0.0
ERTH	0.0	EPST	0.52036595	SIGMT	1.2317370	1.2317370	XITR	0.0
QMF	13.415935	KUMT	0.07177979	KGV	0.76010505	0.76010505	YITR	0.0
MUS	0.1595000	CT916	0.11017923	LTOI	-0.5255324	-0.5255324	ZITR	0.0
MUY8	0.2527530E-1	CH916	-0.21221149E-2	DTOT	27.409134	27.409134	LITR	0.0
MUZS	-0.3203307E-3	CH916	0.91072714E-6	TIR	942.75573	942.75573	MITM	0.0
LAMBMR	-0.52745455E-1	NZ	0.99000731	MPMH	1376.4220	1376.4220	NITR	0.0
DMSMR	0.5202312E-1	VC	0.0	KTRBLK	1.0	1.0	AXP	1.6003302
XMR	1500.4004	MBAR	-562.56457	VX00T	0.36540016E-1	0.36540016E-1	ATP	0.12004232E-1
YMR	-500.95903	JBAR	506.95963	VY00T	0.5733206E-2	0.5733206E-2	AAP	-32.140595
ZMR	-10767.593	TBAR	10013.002	VZ00T	-0.12719076E-1	-0.12719076E-1	VBP	101.20533
LMM	-5770.6350	LBMM	-1200.4014	PUOT	0.20935727E-2	0.20935727E-2	VTP	16.073409
MM	19011.970	MBMM	-3931.1303	QUOT	-0.59425504E-3	-0.59425504E-3	VZP	5.0747045
NM	27073.000	QBAR	20017.474	RUOT	-0.11440112E-2	-0.11440112E-2	PSTR.	0.0
XMF	-511.53042	XT	-50.130310	XTP	0.0	0.0	PSIDMG	0.0
YMF	-274.20342	YT	-96.322052	YTM	005.96640	005.96640	BTR	2.0
ZMF	103.95705	ZT	-140.09450	ZTR	-522.46005	-522.46005	MADD	0.0
LMF	501.70795	LT	-287.50297	LTR	5412.1039	5412.1039	XADD	0.0
MMF	-4006.9006	MT	-4150.6244	MTR	-9991.0731	-9991.0731	VADD	0.0
NMF	-2501.6120	NT	2600.3500	NTR	-27450.194	-27450.194	ZADD	0.0
XT	-62.040032	XVT	4.5105143	ALFMTT	3.5041153	3.5041153	NADD	0.0
YMT	-2.1057220	YVT	-94.176329	ALFVTT	10.796405	10.796405	LADD	0.0
ZMT	-142.40053	ZVT	-1.0079760	AAB01F	1.4470307	1.4470307		



WEIGHT	1900.0	FSCG	360.20000	V	100.0	PSIIR2	0.0
IX	6260.0	MLCG	246.29999	DELS	-5.0	VXSIR.	0.0
IY	41507.0	RMO	0.17500000E-2	VROUND	1077.0	VYSTR.	0.0
IZ	30224.0	TIME	0.20000000E-1	DELJMK	0.0	VZSTR.	0.0
OMEGM	27.019999	NBS3	4.0	TMJMK	-10.0	PSTR.	0.0
OMEGTR	124.62000	NBS3	5.0	TMSTR	-10.0	WLVI	273.0
KFR	15.0	PASCNT	1230.0	MLHI	234.0	F3VT	695.0
FSMT	700.40000	SHT	43.0	SVT	32.500000	USTM.	0.0
LATSTK	-1.110497	AIS	-2.0366959	IM1	2.1731706	XA	43.059609
LNGSTK	9.9605309	BIS	9.6520607	IS	-3.0	XB	14.775487
COLSTK	19.472601	THETA0	19.472601	TH7MK	9.3926010	XC	56.204257
PEUAL	15.074932	THET1R	26.666149	TH7STR	13.16149	XP	37.594443
XAIN	4.3059000	XBIN	1.4775487	XCIN	5.6204257	XPIN	2.0308471
XBACTP	16.036392	XBACTI	1.6036392	RSTM.	0.0	PSTR	0.0
VXB	160.54012	THETAB	4.8093331	AARF	4.1181395	OSTM	0.0
VYB	13.675936	PHIB	0.0	AALF	-4.0935119	RSTR	0.0
VZB	11.017919	BETAMF	4.2912516	BRIF	0.11079506	TITH	0.0
P	0.0	GANC	0.0	AABL	-5.2246011	MITH	0.0
Q	0.0	OMGRAT	1.0	AAIL	0.36149302	JITR	0.0
R	0.0	PSIDOT	0.0	BBIL	0.21530410	MNITR	0.0
ALPWF	-0.94351625	EATX	1.3321035	EMFX	0.92517276	LM1R	0.0
CHITPP	01.936367	EKTZ	1.7012676	EKMZ	1.0006636	OMITR	2.0
EKTH	0.0	EPST	0.49291251	SIGT	0.7526032	XITH	0.0
OMF	29.220740	KMT	0.07177979	KOVI	0.82085192	VITH	0.0
MUXS	0.25308261	CT816	0.11111695	LTOI	1.5002809	ZITH	0.0
MUYS	0.10860779E-1	CH316	-0.60613351E-2	DTOT	24.430250	LITR	0.0
MUZS	0.41069016E-2	CUM316	0.09080370E-6	TIR	1003.6709	MITR	0.0
LAMBMR	-0.16102195E-1	NZ	0.99770940	MPMK	1417.8943	NITR	0.0
DM8MR	0.20209157E-1	VC	0.71525573E-5	KTRBLK	1.0	AXP	2.2410316
XMR	2020.5010	HBAR	-1035.0113	VXUOT	-0.02040769E-2	AYP	-0.17539004E-1
YMR	-469.30570	JBAR	409.30570	VYUOT	-0.09308123E-2	AZP	-32.102576
ZMR	-10092.201	TBAR	10973.924	VZUOT	-0.20110525E-2	VXP	160.59012
LMW	-5909.0019	LBARM	-1600.7003	PUOT	-0.42076809E-2	VYP	13.675950
MMR	0011.0939	MBARM	-11070.905	QUOT	-0.20944970E-3	VZP	11.017919
NMR	27937.223	QBAR	20001.655	RUOT	0.39144494E-3	RSTR.	0.0
XMF	-692.12701	XT	-4.4013164	XTR	0.0	PSIDMG	0.0
YMF	-320.52011	YT	-150.69340	YTR	943.21235	BTR	2.0
ZMF	-34.009306	ZT	226.17545	ZTR	-343.30108	MADD	0.0
LMF	531.00015	LT	-330.35104	LTR	5761.0010	XADD	0.0
NMF	-3000.9194	MT	6425.7517	NTR	-10636.636	YADD	0.0
XMT	-2913.0706	NT	4205.0324	ALFMTT	-2.0559512	ZADD	0.0
YMT	1.2098772	XVT	-5.0911936	ALFVTT	4.6777553	MAUD	0.0
ZMT	-1.5203625	YVT	-149.17312	AAB5IF	4.0950111	LADD	0.0
	225.67400	ZVT	0.50005064				

UT1AS(S76) 1-21-77 16-SEP-77 RUN 32.

WEIGHT	19900.0	FSCG	360.20000	V	120.0	PS1TR2	0.0
IX	6260.0	MLCG	246.29999	DEL3	-5.0	VXSTR.	0.0
IY	41507.0	RHO	0.17500000E-2	V50UND	1077.0	VYSTR.	0.0
IZ	38224.0	TIME	0.20000000E-1	DEL3MM	0.0	VZSTR.	0.0
OMEGMR	27.019994	NBSS	4.0	TWSTR	-10.0	PS1M.	0.0
OMEGTR	124.62000	NSS	5.0	TWSTR	-10.0	MLVT	273.0
KFM	15.0	PASCNT	1217.0	MLMT	234.0	FST	695.0
FSMT	70P.40000	SMT	45.0	SVT	32.500000	QSTM.	0.0
LATSTK	-1.5059633	AIS	-2.4175206	IMT	0.75663007	XA	41.537729
LNOSTK	11.529501	BIS	11.042752	IS	-3.0	XC	9.9671332
COLSTK	20.495119	THETA0	20.495119	TH75MR	10.415119	XP	62.594495
PEUAL	16.032439	THETM	20.051002	TH75TR	15.351002	XPIN	34.930623
XAIN	4.1537724	XBIN	0.99671332	XCIN	6.2594494	PS1M	1.0866365
XOACTP	10.097036	XOACTI	1.0097035	RSTM.	0.0	QSTR	0.0
VXB	202.54593	THETA0	2.7066535	AA0P	4.0824927	RSTR	0.0
VYM	14.137591	PHI0	0.0	AA1P	-0.0765376	TSTR	0.0
VZB	9.0591917	SELTAMF	3.7703400	BB1P	0.91237400E-1	MITR	0.0
P	0.0	GAMC	0.0	AA0L	-6.5077339	JSTR	0.0
O	0.0	OMGNAT	1.0	AA1L	0.41411603	MMSTR	0.0
R	0.0	PSIUOT	0.0	BB1L	0.19071790	MMSTR	0.0
ALFMF	-0.67202079	EXTX	1.3092301	EMPMX	0.92921540	MMSTR	0.0
CHITPP	02.247306	EXTZ	1.6934372	EMPMZ	1.0077526	OMSTR	0.0
EKTR	0.0	EPST	0.40770300	SIGMT	0.66490797	XITM	0.0
OMF	40.235629	KOMT	0.07177979	KOVT	0.83052590	YITM	0.0
MUXS	0.2797041	CT91G	0.11120060	LTOI	1.7044262	ZITR	0.0
MUTS	0.19501502E-1	CH91G	-0.52454093E-2	DTOT	24.535660	LITR	0.0
MUZS	-0.10417322E-2	CH91G	0.09110301E-6	TTR	1236.4301	MITR	0.0
LAMBMR	-0.17900590E-1	NZ	0.99941705	MPMM	1735.0914	NITR	0.0
DMSHMR	0.16930050E-1	VC	0.14305114E-4	KTRDLK	1.0	AXP	1.5400303
XMR	1000.2110	MBAR	-0.95.70056	VIBUOT	-0.10202100E-1	AYP	-0.24905395E-1
YMR	-576.20406	JBAR	576.20406	VIBUOT	-0.96359550E-2	AZP	-32.161700
ZMR	-10415.212	TBAR	10909.500	VZBUOT	-0.21577739E-1	VXP	202.54593
LMR	-7364.0712	LBARM	-2000.0999	PUOT	-0.76190140E-2	VYP	14.137591
MMR	0971.6537	MBARM	-10901.604	QOUI	-0.13460500E-2	VZP	9.0591917
NMR	34162.719	OBAR	35293.067	ROUI	0.63290020E-3	RSTM.	0.0
XMF	-955.70425	XT	-15.340053	XTR	0.0	PSIDMG	0.0
YMF	-398.25090	YT	-193.20360	YTR	1161.9506	BTR	2.0
ZMF	-57.305424	ZT	310.50605	ZTR	-422.91629	MADD	0.0
LMF	640.9011	LT	-424.11270	LTR	7090.0009	XADD	0.0
MMF	-4975.2402	MT	9051.0401	MTR	-13103.350	YADD	0.0
NMF	-3531.2426	NT	5591.1011	NTR	-36001.105	ZADD	0.0
XMT	-4.5205406	XVT	-10.015509	ALFMTT	-5.0211777	NADD	0.0
YMT	-1.770013	YVT	-191.42968	ALFVTT	4.0022339	LADD	0.0
ZMT	317.07043	ZVT	0.71041911	AABHIF	4.0775504		

UTIAS(S/P) 1-21-77 16-SEP-77 RUN 33.

WEIGHT	19900.0	FSLG	360.20000	V	140.0	PSIR2	0.0
IX	6268.0	WLCG	246.29999	DEL3	-5.0	VSTR.	0.0
IY	91507.0	RMU	0.17500000E-2	VSDUN	1077.0	VSTR.	0.0
IZ	50224.0	TIME	0.20000000E-1	DELJMR	0.0	VSTR.	0.0
OMEGMR	27.01999	NBS	4.0	TMSTR	-18.0	PSTR.	0.0
OMEGTR	124.62000	NSS	5.0	TMSTR	-18.0	PSTR.	0.0
KFM	15.0	PASCT	1511.0	MLMT	234.0	FLVT	273.0
FSMT	700.40000	SMT	45.0	MLMT	234.0	FLVT	695.0
LATSTK	-2.5536269	AIS	-3.5076137	IMT	0.22549525	QSTR.	0.0
LGSTK	15.630475	BIS	12.094850	IS	-3.0	XA	35.289031
COLSTK	20.460454	THEIAC	22.460454	TMSTR	12.500454	XB	1.0145745
PEDAL	20.505540	THEIAC	34.002005	TMSTR	21.502005	XC	74.077839
XAIN	5.5209031	XBIN	0.10145745	XCIN	7.4077039	XP	24.757316
XBACTP	-0.16057375	XBACTI	-0.16057374E-1	RSTR.	0.0	XPIN	1.3360602
VXB	236.53006	THEIAB	1.1100015	AAAP	4.0504062	PSIR	0.0
VVB	14.463121	PHIB	0.0	AAIP	-3.7852726	QSTR	0.0
VZB	4.5034004	REIAMP	5.8215155	BBIP	-0.41644849E-1	RSTR	0.0
P	0.0	GAMC	0.0	AAWL	-9.3189593	MITR	0.0
G	0.0	OMGHAT	1.0	AAIL	0.57340779	JITR	0.0
R	0.0	PSIOUT	0.0	BBIL	0.15021995	MMTR	0.0
ALFMP	-1.4063310	ERTX	1.3318751	EMPA	0.92306154	LMTR	0.0
CHITPP	0.1.775465	ERTZ	1.7159271	EMPAZ	1.0002260	GMTR	0.0
GMT	0.0	EPSMT	0.40021515	SIGMT	0.67258676	XITR	0.0
GMP	53.540606	KMT	0.87177479	KGT	0.85031793	YITR	0.0
MUXS	0.32613079	CTSIG	0.11162011	LTOI	0.04100902	ZITR	0.0
MUYS	0.22709427E-1	CHSIG	-0.36940166E-2	DIOT	24.344302	LIIR	0.0
MUZS	-0.10761099E-1	CUMSIG	0.00411602E-6	TIR	1700.1776	MITR	0.0
LAMBMR	-0.25329201E-1	NZ	1.0005003	MPMR	2498.0073	NITR	0.0
DASHMR	0.14507302E-1	VC	0.7152573E-5	KTRBLK	1.0	AXP	0.59273494
XMM	1027.4197	MBAM	-630.77676	VXDUOT	-0.59691521E-1	AYP	0.35010003E-1
YMM	-067.01197	JBAR	067.01197	VYDUOT	0.1650572E-1	AZP	-32.199134
ZMR	-14007.594	TBAR	19061.208	VZDUOT	-0.25867362E-1	VXP	236.53006
LMM	-10473.540	LBARM	-2641.5031	PUOT	0.77547262E-2	VYP	16.463121
MMH	11495.240	MBARM	-10155.432	QDOT	-0.48353222E-2	VZP	4.5034004
NMM	69206.254	QBAR	50849.299	RUOT	-0.96696602E-3	RSTR.	0.0
XMF	-1264.5110	XT	-14.677223	XTR	0.0	PSIDMG	0.0
YMF	-534.01967	YT	-262.07274	YTR	1672.9441	BTR	2.0
ZMF	-15.009266	ZT	525.40245	ZTR	-600.90306	MADD	0.0
LMF	874.70045	LT	-574.77540	LTR	10219.515	XADD	0.0
MMF	-7760.4756	MT	14929.965	MTR	-10065.046	YADD	0.0
NMF	-0740.4320	NT	7312.9030	NTR	-51033.306	ZADD	0.0
XMT	0.10766533	XVT	-14.785000	ALFMTT	-3.0121306	NADD	0.0
YMT	-2.5050640	YVT	-259.50767	ALFVTI	3.9404995	LADD	0.0
ZMT	524.43875	ZVT	1.0437009	AA001P	3.7055016		



RUN 34.

1-21-77 16-SEP-77

UTIAS(S16)

WEIGHT	19900.0	FSCB	360.20000	V	150.0	PSITH2	0.0
IX	6260.0	WLCG	246.29999	DELS	-5.0	VXSTR.	0.0
IY	41507.0	NMO	0.17500000E-2	VOUNU	1077.0	VYSTR.	0.0
IZ	30220.0	TIME	0.20000000E-1	DELJMR	0.0	VZSTR.	0.0
OMEGMR	27.019999	NBS	4.0	TMSTMM	-18.0	PSHM.	0.0
OMEGTK	124.86000	NSS	5.0	TMSTTM	-18.0	MLVT	273.0
KFM	15.0	PASLNT	1060.0	WMT	254.0	F8VT	695.0
FSMT	700.80000	SMT	45.0	SVT	32.30000	QSTR.	0.0
LAISTK	-5.4004343	AIS	-4.9100241	IMT	2.1306094	XA	20.497205
LGSTK	14.109999	BIS	11.001750	IS	-3.0	XB	0.0
CULSTK	24.025531	THETAB	24.025531	TM75MM	14.745531	XC	09.659573
PEUAL	24.036000	THETTR	37.5	TM75TM	24.0	XP	0.0
XAIN	2.0497204	XOIN	0.0	XCIN	0.9659572	XPIN	0.0
XBACTP	-4.2440414	XOALTI	-0.4240414	RSTM.	0.0	PSIR	0.0
VXB	253.15072	THETAB	-2.9740592	AAUP	4.1307400	QSTR	0.0
VYB	12.924004	PHIB	0.0	AAIP	0.05937304E-1	RSTM	0.0
VZB	-13.155667	BETAMP	2.0030507	BAIP	0.30070046	TITM	0.0
P	0.0	GAMC	0.0	BAOL	-12.920078	MTR	0.0
Q	0.0	OMGNAT	1.0	AAIL	0.6330445	JITH	0.0
R	0.0	PSIDOT	0.0	SEIL	-0.29419435	MHIR	0.0
ALFHF	-5.0004299	EXTX	1.1017009	EMPX	0.92365205	LMTR	0.0
CHITPP	01.019390	EXTZ	1.0430036	EMFZ	1.0001006	QMITR	0.0
EXTR	0.0	EPSMT	0.47003058	SIGMT	0.49347914	XITR	0.0
UNP	0.914500	KUMT	0.07177979	KQVI	0.03520003	VITR	0.0
MUXS	0.34712120	CTSIG	0.11409720	LTOI	-4.0199445	ZITR	0.0
MUYS	0.17020415E-1	CHSIG	0.43700200E-2	DTOT	24.166946	LITM	0.0
MUZS	-0.30395057E-1	CUMSIG	0.90163432E-6	TTR	2020.0024	MTR	0.0
LAMBMR	-0.30307754E-1	NZ	0.99502696	MPHM	3411.7000	NITM	0.0
DSMMR	0.13972047E-1	VL	0.14305114E-4	KTRBLK	1.0	AXP	-2.8793936
XMM	200.21903	MBAM	747.51467	VXBOOT	-0.15755469	AYP	-0.74397554
YMM	-1232.1342	JBAR	1032.1342	VYBOOT	-0.27055690E-1	AZP	-30.734137
ZMM	-19030.152	TBAR	19019.440	VZBOOT	0.11415029	VXP	253.13872
LMH	-12009.005	LBARM	-1623.5700	PUOT	-0.29019137E-2	VYP	12.924649
MMH	31002.931	MBARM	652.50000	QUOT	0.51500024	VZP	-13.155067
NMH	67226.702	GBAM	67446.167	RUOT	0.28619001	RSTM.	0.0
XMF	-1424.4340	XT	60.093732	XTR	0.0	PSIDMG	0.0
YMF	-447.26325	YT	-243.02430	YTR	1905.9157	BTM	2.0
ZMF	372.64093	ZT	950.12723	ZTR	-693.69795	MAUU	0.0
LMF	029.11904	LT	-531.33030	LTR	11642.000	XADU	0.0
NMF	-15729.350	MT	27293.413	MTR	-21493.074	YADU	0.0
XMT	-4010.3709	NT	6701.6704	NTR	-59051.023	ZADU	0.0
YMT	01.734501	XVT	-21.640040	ALFMTT	-6.1673489	NADU	0.0
ZMT	-2.0094506	YVT	-240.13405	ALFVTT	2.8900779	LADU	0.0
	954.90794	ZVT	3.1502999	AABRIF	0.30642756		

WEIGHT	1900.0	FSCG	300.20000	V	150.0	PSI1R2	0.0
IX	6260.0	WLCW	246.29999	DEL3	-5.0	VXSTR.	0.0
IY	41507.0	RMU	0.17500000E-2	V SOUND	1077.0	VYSTR.	0.0
IZ	50224.0	TIME	0.20000000E-1	DEL3MK	0.0	VZSTR.	0.0
OMEGMR	27.014999	NSS	4.0	TMSTR	-10.0	PSM.	0.0
OMEGTR	124.62000	NSS	5.0	TMSTR	-10.0	MLVT	273.0
KFR	15.0	PASUNT	1357.0	WLMT	234.0	FSVT	695.0
FSMT	700.40000	SMT	45.0	IS	1.3540781	QSTM.	0.0
LATSTK	-3.430055	AIS	-4.8659000	IMT	-3.0	XA	20.500402
LONGTK	10.0	BIS	15.31000	TM75MR	14.250749	XC	0.0
COLSTK	24.336749	THETA0	24.336749	TM75TR	24.0	XP	0.0
PEUAL	29.436000	THETR	37.5	XCIN	0.6604604	XPIN	0.0
XAIN	2.0500402	XBIN	0.0	RSTR.	0.0	PSTR	0.0
XBACTP	-2.9570585	XBACTI	-0.29570544	AAVP	4.0205314	QSTR	0.0
VXB	253.46405	THETAB	0.44956497	AAIP	-4.7300915	RSTR	0.0
VYB	10.549714	PHIB	0.0	BBIP	-0.14074197	TITH	0.0
VZB	1.9000267	BETAMF	3.0053156	AAOL	-12.037575	HITH	0.0
P	0.0	GAMC	0.0	AAIL	0.75640594	JITH	0.0
Q	0.0	UMGMAT	1.0	MMIL	0.24300257	MMITH	0.0
R	0.0	PSIUOT	0.0	ERMPX	0.90654006	LMITH	0.0
ALP4F	-1.7260323	ENTX	1.4005106	EKMP2	1.0094962	GMITH	0.0
CHITPP	00.503760	EKT2	1.7107020	SIGMT	0.63453555	XITH	0.0
EMT	0.0	EPMT	0.40005315	KQVI	0.03135001	VITH	0.0
OMT	00.531632	KQMT	0.07177979	LTOI	0.36992740	ZITH	0.0
MUXS	0.54927631	CTSIG	0.11127502	DTOT	24.301063	LITH	0.0
MUYS	0.22020000E-1	CHSIG	-0.39601074E-2	TIR	2040.2770	MITH	0.0
MUZS	-0.15550703E-1	CHMSIG	-0.07932465E-6	MPMN	3201.4266	NITH	0.0
LAMBMR	-0.29113717E-1	NZ	1.0047190	KTRBLK	1.0	AXP	0.72012703
OMSHMR	0.13552014E-1	VC	0.09406967E-6	VXBUOT	0.99083665E-1	AYP	-0.34380090
XMR	1609.6352	MBAR	-0.76.21344	VYBUOT	0.50820017E-1	AZP	-32.924960
YMR	-1031.7110	JBAN	1031.7110	VZBUOT	-0.15370704	VXP	253.46965
ZMR	-10430.010	TBAR	19000.915	PUOT	0.11054068E-1	VYP	16.549719
LAR	-12395.365	LBAMH	-2031.2354	RUOT	-0.24323001	VZP	1.9800267
MMR	0510.6291	MBAMH	-12775.023	XTR	0.17076605	RSTR.	0.0
NMR	63220.401	QBAM	65165.975	YTR	0.0	PSIDMG	0.0
WMF	-571.66152	XT	-23.279671	ZTR	1924.0947	BTR	2.0
ZWF	21.061179	YT	-206.62103	LTR	-700.60574	MADD	0.0
LWF	953.00930	ZT	439.46363	NTR	11750.605	XADD	0.0
MMF	-9421.0754	MT	-629.97055	ALFMTT	-21707.101	YADD	0.0
XMT	-5070.0000	XVT	7997.0013	ALFVIT	-59639.654	ZADD	0.0
YMT	-4.9906504	ZVT	-10.709021	AABMIP	-2.7002592	NAUD	0.0
ZMT	-2.5000779		-204.23295		3.7295165	LADD	0.0
	430.13070		1.3240900		4.7320046		

UTAS(376) 1-21-77 9-DEC-77 RUN 13.

WEIGHT	19900.0	FSCG	360.20000	V	40.0	PSITR2	0.0
IX	6260.0	MLCG	245.99999	DELS	-5.0	VXSTR.	0.0
IY	41587.0	RHO	0.17520000E-2	VOUNO	1077.0	VYSTR.	0.0
IZ	30224.0	TIME	0.20000000E-1	NEL3MR	0.0	VZSTR.	0.0
OMEGMR	29.72000	NBS8	4.0	TMSTR	-10.0	PSSTR.	0.0
OMEGTR	137.07999	NBS8	5.0	TMSTR	-10.0	HLVT	273.0
KFR	15.0	PASCT	1574.0	WLMT	234.0	PSVT	695.0
P8MT	700.40000	SMT	45.0	SVI	32.30000	QSTR.	0.0
LATSTK	-1.6645184	AIS	-2.6500000	INT	20.452054	XA	30.346704
LONGTK	A.5750306	BIS	4.1443951	IS	-3.0	XB	33.030950
COLSTK	10.106151	THETA	10.106151	TM75MR	0.0261315	XC	47.663444
PEDAL	14.069022	THETR	24.021204	TM75TR	10.521204	XP	40.300042
XAIN	3.0346704	XBIN	3.3030950	XCIN	4.7663447	XPIN	2.1005087
X9ACTP	40.587456	X9ACTI	4.0587456	ASTR.	0.0	PSSTR	0.0
VXB	67.349219	THETAB	4.085227	AAOF	3.4930566	QSTR	0.0
VYB	0.0	PMIB	-1.7132399	AAIF	-2.6241740	QSTR	0.0
VZB	5.7569621	DETAWF	0.0	BBIF	-0.30731454	TSTR	0.0
P	0.0	GMC	0.0	AAPL	-5.0087476	MSTR	0.0
Q	0.0	OMGRAT	1.0	AAIL	0.22559690	JSTR	0.0
R	0.0	PSIDOT	0.0	BBIL	0.12570405	MHSTR	0.0
ALP-F	-17.070022	EKTZ	0.97024706	EKWF	0.69015035	LMSTR	0.0
CHITPP	62.319074	EKTZ	2.0165237	EKWF2	1.03553602	QMSTR	0.0
EATH	0.0	EPST	0.44999999	SIGMT	0.0	XISTR	0.0
Q-F	7.9436076	KOMT	0.93225064	KQVT	0.04052013	VISTR	0.0
MUXS	0.0	CTSIG	0.92667451E-1	LTOT	-30.741646	ZISTR	0.0
MUXS	0.0	CTSIG	-0.33423794E-2	DTOT	29.091491	LISTR	0.0
MUXS	0.0	CTSIG	0.63020404E-6	TTR	1141.9651	MISTR	0.0
LAMBMR	-0.39600741E-1	NZ	0.99506406	MPMR	1039.6475	NISTR	0.0
D-SMR	0.42397701E-1	VC	0.13498790	KTRBLK	1.0	AXP	2.7434510
XMR	1691.3700	MBAR	-690.49346	VXDOOT	0.34102150E-2	AYP	0.95412731
YMR	-501.21399	JBAR	501.21399	VYDOOT	-0.37110795E-2	AZP	-32.041112
ZMR	-1900.005	TBAR	19143.925	VZDOOT	-0.93619450E-3	VXP	67.349219
LMR	-6504.4505	LOARM	-1796.4220	PDOT	-0.11164289E-2	VYP	0.0
MMR	12741.703	MBARM	-8599.6012 <td>QDOT</td> <td>0.12460200E-3</td> <td>VZP</td> <td>5.7569621</td>	QDOT	0.12460200E-3	VZP	5.7569621
NMR	33073.957	QBAR	3404.421	RUOT	-0.61171596E-3	RSTR.	0.0
XMF	-151.03022	XY	07.254710	XTR	0.0	PSIDMG	-150.0
YMF	0.0	YT	-5.5044320	YTR	1073.1760	BTR	0.0
ZMF	305.29710	ZT	156.30481	ZTR	-390.60000	MAND	0.0
LMF	0.0	LT	-12.611510	LTR	6591.4035	XADD	0.0
MMF	-5156.1065	MT	4521.9060	MTR	-12102.241	YADD	0.0
NMF	0.0	NT	155.40567	NTR	-33250.569	ZADD	0.0
XMT	00.654954	XVT	-1.4002439	ALFMTT	-4.0430697	NADD	0.0
YMT	0.0	YVT	-5.5044320	ALFVTT	0.0	NADD	0.0
ZMT	155.30520	ZVT	0.91961704	AA0BIF	2.6421309	LADD	0.0

UTIAS(S76) 1-21-77 9-DEC-77 RUN 14.

WEIGHT	19000.0	FSCG	360.26000	V	42.0	PSITR2	P.P
IX	6260.0	WLCG	245.49999	DEL3	-5.0	VXSTR.	P.P
IY	41507.0	RMD	0.17500000E-2	V SOUND	1077.0	VYSTR.	P.P
IZ	30224.0	TIME	0.20000000E-1	DEL3MR	P.0	VZSTR.	P.P
OMEGMR	29.72000	NBS3	4.0	THSTR	-15.0	PSSTR.	P.P
OMEGTR	137.07999	NBS5	5.0	THSTR	-10.0	FLVT	273.2
KPR	15.0	PASCNT	2674.0	WMT	234.0	F8VT	695.0
PSMT	700.40000	SMT	45.0	SVT	32.30000	QSTR.	P.P
LATSTK	-1.6904761	A19	-2.4794009	IMT	29.43697	XA	39.434524
LNSTK	0.9723900	A13	4.052173	IS	-3.0	XB	10.295413
CULSTK	10.139541	THETA0	10.139541	TH75MR	0.0595413	XC	47.072134
PEDAL	29.036000	THETR	37.5	TH75TR	24.0	XP	P.0
XAIN	3.9434523	XBIN	1.0295412	XCIN	4.7072134	YPIN	P.0
XBACTP	25.150770	XBACTI	2.5150770	RSTR.	0.0	QSTR	P.0
VXB	67.320324	THETA8	5.1667290	AAOF	3.5054754	OSTR	P.0
VYB	0.0	PHIB	-1.1610475	AAIF	-2.9759461	PTTR	P.0
VZB	6.0074677	RETAFF	0.0	BBIF	-0.11532144	TITR	P.0
P	0.0	GAMC	0.0	AAPL	-4.9660046	MITR	P.0
O	0.0	OMGRAT	1.0	AAIL	0.24637844	JITR	P.0
ALF-P	-17.773577	PSIDOT	0.0	MBIL	0.14604904	MMITR	P.0
CHITPP	62.104536	EKTZ	2.0051772	EKWF	0.68735096	LMITR	P.0
EXTN	0.0	EPST	0.4499999	SIGMT	1.0357909	GHITR	P.0
Q-F	7.9291009	KQMT	0.9326660	KQVT	0.04052013	XITR	P.0
MUXS	0.00703371E-1	CTSIG	0.92916730E-1	LTOT	-30.547155	VITR	P.0
MUTS	0.0	CHSIG	-0.34959391E-2	DTOT	29.009005	LITR	P.0
MUZS	0.32040219E-2	COMSIG	0.63244462E-6	TTR	071.06125	MITR	P.0
LAMMR	-0.39356659E-1	NZ	0.9958963	MPMR	1791.5000	NITR	P.0
D-SMR	0.02561401E-1	VC	0.11252760	KTRBLK	1.0	AXP	2.0221915
YPR	1020.2667	MBAR	-0.04.05100	VXROOT	0.28590363E-2	AYP	0.10590490
YPR	-427.64149	JBAR	427.64149	VYROOT	-0.97361655E-4	AZP	-32.031626
ZPR	-19125.504	TBAR	19195.423	VZROOT	0.16378259E-3	VXP	67.320324
LPR	-5006.0140	LBARM	-1145.2653	PDOT	-0.36130440E-4	VYP	0.0
MPR	10945.627	MBARM	-9769.0510	QDOT	-0.32040219E-3	VZP	6.0874677
NPR	32341.243	QBAR	33155.096	RDOT	0.10664339	PSSTR.	P.0
XPF	-151.12421	XT	62.978297	XTR	P.0	PSIDMG	-150.0
YPF	0.0	YT	-5.5057317	YTR	010.59069	MTR	2.0
ZPF	302.01390	ZT	117.50245	ZTR	-297.94322	MADD	P.P
LPF	0.0	LT	-12.618404	LTR	5027.0110	XADD	P.P
MPF	-5127.7670	MT	3400.0496	MTR	-9231.2741	YADD	P.P
NPF	0.0	NT	155.04191	NTR	-25362.668	ZADD	P.P
XPT	64.302043	XVT	-1.4045450	ALFMTT	-3.6090061	MADD	P.P
YPT	0.0	YVT	-5.5057317	ALFVTT	0.0	MADD	P.P
ZPT	116.66074	ZVT	0.91371019	AAB01F	2.9701797	LADD	P.P

RUN 15.

9-DEC-77

1-21-77

UTTAB(S76)

WEIGHT	1900.0	FSCG	360.20200	V	60.0	PSIR2	0.0
IX	6260.0	WLCG	245.09999	DEL5	-5.0	VXSTR.	0.0
IY	41507.0	RMO	0.17500000E-2	VSOUND	1077.0	VYSTR.	0.0
IZ	30220.0	TIME	0.20000000E-1	DEL3MR	0.0	VZSTR.	0.0
OMEGMR	29.720000	NBS9	0.0	THSTR	-10.0	PSIR.	0.0
OMEGTR	137.07999	NBS9	0.0	THSTR	-10.0	WLVT	273.0
KFR	15.0	PASCNT	1760.0	WLMT	234.0	FSTV	695.0
FSTV	700.00000	SMT	45.0	SVT	32.30000	QSTR.	0.0
LATSTK	-1.0204239	A19	-1.7097144	IMT	20.993322	XA	43.722350
LNGSTK	9.2400419	B19	4.5259636	IS	-3.0	XB	17.319205
CULSTK	17.327400	THETA0	17.327400	TH75MR	7.247405	XC	42.706754
PEDAL	29.436000	THETTR	37.5	TH75TR	24.0	XP	0.0
XAIM	4.372350	XBIN	1.7519205	XCIN	4.2796754	XPIN	0.0
XOACTP	21.993065	XOACTI	2.1993065	ASTR.	0.0	PSIR	0.0
VAB	101.23102	THETAB	3.2297766	AAIF	3.3547941	QSTR	0.0
VVB	17.350673	PHIB	0.0	ABIF	-1.0636352	RSTR	0.0
VZB	5.712036A	BETAMF	0.0633511	RBIF	-0.24623450E-1	TITR	0.0
P	0.0	GAMC	0.0	AAFL	-4.1541264	HITR	0.0
Q	0.0	OMGRAT	1.0	AIL	0.19526776	JITR	0.0
P	0.0	PMIDNT	0.0	ABIL	0.59093330E-1	WHITR	0.0
ALP=F	-0.5579009	FRTX	1.2621922	EXMFX	0.04775730	LHITR	0.0
CHITP	75.250964	EKTZ	1.9466122	EXMFX	1.0147493	QHITR	0.0
EXTP	0.0	EPMT	0.53063350	SIGT	1.2590555	XITR	0.0
QAF	13.415961	KOMT	0.47177979	KOVT	0.75479755	VITR	0.0
MUX5	0.12714544	CTSIG	0.91000263E-1	LITOT	-0.0799050	ZITR	0.0
MUY5	0.21760430E-1	CHSIG	-0.20799346E-2	OTOT	27.471151	LITR	0.0
MUZ5	0.51001512E-3	COMSIG	0.60525920E-6	TTR	0.93.24377	MITR	0.0
LAMBMR	-0.20005651E-1	NZ	0.99033767	MDMR	1512.7996	NITR	0.0
DMSMR	0.29595666E-1	VC	0.35762706E-5	KTPBLK	1.0	AXP	1.7909045
XMR	1417.3374	MBAR	-0.29.60021	VIRDOT	0.16674607E-2	AYP	-0.92339456E-1
YMR	-453.00405	JBAR	453.00405	VIRDOT	0.54645530E-3	AZP	-32.120793
ZMR	-10033.950	TBAR	10033.792	VIRDOT	0.12100016E-3	VXP	101.23102
LPR	-5609.2490	LBARM	-1421.4396	PDOT	0.33823054E-3	VYP	17.350673
MPR	16341.507	MBARM	-6230.9034	ODOT	-0.16700942E-3	VZP	5.7120568
NMR	27131.914	QBAR	27995.956	RODT	0.37654550E-1	RSTR.	0.0
XAF	-311.73696	XT	-29.194732	XTR	0.0	PSIOMG	-150.0
YAF	-207.34946	YT	-97.959074	YTR	0.0	STR	2.0
ZAF	156.50572	ZT	-73.205627	ZTR	-305.53067	MAOD	0.0
LAF	504.20444	LT	-215.61415	LTR	5155.0505	XADD	0.0
MAF	-4759.8901	MT	-2122.0414	MTR	-9466.3545	YADD	0.0
NAF	-2410.6657	NT	2733.0349	NTR	-26000.555	ZADD	0.0
XMT	-34.100615	XVT	4.9910023	ALFMTT	1.7730267	MAOD	0.0
YMT	-1.7261020	VVT	-96.232001	ALFVTT	11.104022	LAND	0.0
ZMT	-71.543200	ZVT	-1.7403400	AA0BIF	1.4637979		

RUN 16.

9-DEC-77

1-21-77

UTIAS(S76)

WEIGHT	19008.0	FSCG	360.20000	80.0	PSITR2	0.0
IX	6260.0	WLCG	245.89999	-5.0	VXSTR.	0.0
IY	41507.0	RHO	0.17500000E-2	1077.0	VYSTR.	0.0
IZ	30224.0	TIME	0.20000000E-1	0.0	VZSTR.	0.0
OMEGMR	29.72000	NBS5	4.0	-18.0	PSTR.	0.0
OMEGTR	137.07999	NBS8	5.0	-18.0	WLVT	273.0
KFR	15.0	PASCNT	2031.0	234.0	FSVT	695.0
FSHT	700.00000	9MT	45.0	32.30200	OSTR.	0.0
LATSJK	-0.06986941	AIS	-1.560727	8.7391549	XA	44.563316
LNSTJK	16.749941	015	6.0416779	-3.0	XB	11.072997
CULSTK	17.239255	THETAR	17.239255	7.1592553	YC	42.245346
PEDAL	29.436000	THEITR	37.5	24.0	XP	0.0
XAIN	4.563314	XBIN	1.1072997	4.2245346	XPIN	0.0
XBACTP	15.139236	XBACTI	1.5139236	0.0	PSTR	0.0
VIB	134.95994	THETAB	3.3575525	3.3103565	OSTR	0.0
VIB	17.445405	PHIB	0.0	-2.0342951	RSTR	0.0
VIB	7.9102032	BETAF	6.560903	-0.07259753E-2	TSTR	0.0
P	0.0	GAMC	0.0	-4.1746002	WTR	0.0
Q	0.0	OMGRAT	1.0	0.22450934	JTR	0.0
R	0.0	PSIDOT	0.0	0.16232964	WTR	0.0
ALF.F	-3.9300427	EKTX	1.4147717	0.09050506	LWTR	0.0
CHITPP	79.064179	EKTZ	1.7900190	1.0101358	OWTR	0.0
EXTR	0.0	EP9MT	0.51560890	1.0742954	XTR	0.0
QF	20.343912	KQHT	0.87177979	0.70967019	VTR	0.0
MUS	0.16952722	CTSIG	0.91627454E-1	-1.4132319	ZTR	0.0
MUS	0.21070300E-1	CHSIG	-0.29616340E-2	25.520130	LWTR	0.0
MUS	0.10501704E-2	COMSIG	0.59724199E-6	903.09224	WTR	0.0
LAMBMR	-0.21700420E-1	NZ	0.99011019	1500.5396	NWTR	0.0
DASHMR	0.22766590E-1	VC	0.0	1.0	AXP	1.9330294
XMR	1597.4450	HBAR	-607.79460	0.10490209E-1	AYP	0.23461506E-1
YMR	-435.04047	JBAR	435.00047	-0.24149630E-2	AZP	-32.115199
ZMR	-10069.059	TBAR	10929.074	0.34192703E-2	VXP	134.95094
LPR	-5900.7009	LBARM	-1465.9083	-0.10921264E-2	VYP	17.445405
MPR	12125.547	MBARM	9432.6397	-0.51005313E-3	VZP	7.9102032
NMR	27059.601	QBAR	27917.121	-0.19204157E-1	PSIR.	0.0
XPF	-479.96389	YT	6.4560422	0.0	PSIDMG	-150.0
YPF	-352.03201	YT	-137.43266	923.07322	NTR	2.0
ZPF	61.935217	YT	92.107300	-336.26300	MADD	0.0
LPR	609.14604	LT	-305.17034	5674.4606	XADD	0.0
MPR	-4341.5509	MT	2612.9741	-10410.508	VADD	0.0
NPR	-3004.6163	NT	3035.0900	-20624.671	ZADD	0.0
XMT	5.1201052	XVT	1.5367169	-1.5274318	NADD	0.0
YMT	-1.5970551	YVT	-135.03561	7.9560775	LADD	0.0
ZMT	92.105647	ZVT	-0.27034640	2.0343005		

UTAS(376) 1-21-77 9-DEC-77 RUN 17.

WEIGHT	19000.0	FSCG	360.20000	V	60.0	PSIR2	0.0
IX	6260.0	WLCG	245.09999	DELS	-5.0	VXSTR.	0.0
IY	41507.0	RMO	0.23700000E-2	V SOUND	1117.0	VYSTR.	0.0
IZ	30224.0	TIME	0.20000000E-1	DEL3MP	0.0	VZSTR.	0.0
OMEGMR	29.72000	NSS	4.0	TMSTR	-18.0	PSTR.	0.0
OMEGTR	137.07999	NSS	5.0	TMSTR	-18.0	WLV	273.0
KPR	15.0	PASCNT	1073.0	WLV	234.0	FST	695.0
FSMT	700.0000	SMT	45.0	SVT	32.30000	QSTR.	0.0
LAT3TK	-0.07202037	AIS	-1.3909302	IMT	13.111709	XA	44.544672
LANG3TK	0.4713916	BIS	4.4085099	IS	-3.0	XB	20.005753
COL3TK	15.510192	THETA0	15.510192	TH75MR	5.4301929	XC	31.430704
PEDAL	24.097009	THETTR	30.933320	TH75TR	17.433320	XP	12.502919
XAIN	4.4544072	XBIN	2.0065753	XCIN	3.1430706	XPIN	0.67945999
XOACTP	24.902105	XOACTI	2.4902105	PSTR.	0.0	PSTR	0.0
VXB	101.19271	THETAB	3.6510470	AAOF	3.1100014	QSTR	0.0
VYB	15.212541	PHIB	0.0	AAIF	-2.5952790	RSTR	0.0
VZB	6.4574910	HEAMP	7.3930179	BBIF	-0.1252700E-1	TIYR	0.0
P	0.0	GAMC	0.0	AAOL	-3.7810409	HIYR	0.0
R	0.0	OMGRAT	1.0	AAIL	0.10120714	MIYR	0.0
ALFHF	-5.5941072	PSIDOT	0.0	BBIL	0.13596708	MMIYR	0.0
CHITPP	70.102497	EKT	1.3627530	EKMFY	0.07956745	LMIYR	0.0
EKTR	0.0	EKTZ	1.0499202	EKWFZ	1.0110574	QMIYR	0.0
QWF	16.630927	EPGMY	0.52393017	SIGMT	1.1768334	XIYR	0.0
MUXS	0.12710534	KQMT	0.07177979	KQVT	0.77059002	YIYR	0.0
MUY3	0.19077976E-1	CTSIG	0.67441533E-1	LTOT	-3.4719342	ZIYR	0.0
MUZ3	0.14450710E-2	CHSIG	-0.21905100E-2	DTOT	26.192169	LIR	0.0
LAMPBR	-0.20724706E-1	CM3IG	0.41409561E-6	TIYR	0.0	MIYR	0.0
D-8MMR	0.22100508E-1	NZ	0.99792090	MPMR	1376.7031	NIR	0.0
XMR	1604.0092	VC	0.35762706E-5	KIRBLK	1.0	AXP	2.0523527
YMR	-375.05036	HBAR	-614.92593	VIRDOT	0.30229022E-2	AYP	-0.44747059E-2
ZMR	-19072.772	JBAR	375.05036	VIRDOT	-0.30011074E-2	AZP	-32.100133
LMR	-5353.1576	TBAR	10932.370	VZDOT	0.92500360E-3	VXP	101.19271
MPR	12042.760	LBARM	-1765.9570	POOT	-0.11774270E-2	VYP	15.212541
NMR	24729.090	MBARM	25479.027	QOOT	-0.13679194E-3	VZP	6.4574910
XMP	-309.72100	XT	2.2530232	MOOT	-0.31201199E-3	RSTR.	0.0
YMP	-324.33345	YT	-110.05096	XIR	0.0	PSIOMG	-150.0
ZMP	96.10099	ZT	25.323549	YIR	0.16.46602	RIYR	2.0
LMP	593.97437	LT	-262.24373	ZIR	-207.17019	MAOD	0.0
MPF	-4340.4450	MT	707.31196	LIR	5014.7669	XADD	0.0
NMP	-2735.6706	NT	3294.2255	MIR	-9207.3231	YADD	0.0
XMT	-1.0356040	XVT	4.0095001	NIR	-25296.063	ZADD	0.0
YMT	-1.3390229	YVT	-116.71106	ALFMTT	-0.4003997	NADD	0.0
ZMT	26.312079	ZVT	-0.94933011	ALFVTT	9.5416202	LADD	0.0
				AA0BIF	2.5953092		

UTAS(S76) 1-21-77 9-UEC-77 RUN 10.

WEIGHT	1900.0	FSCG	300.20000	V	0.0	PSIAR2	0.0
IX	6260.0	WLCG	245.89999	DELS	-5.0	VXSTR.	0.0
IY	41507.0	RHO	0.2370000E-2	VOUND	1117.0	VYSTR.	0.0
IZ	30224.0	TIME	0.2000000E-1	DEL3MR	0.0	VZSTR.	0.0
OMEGMR	29.72000	NBSS	4.0	THSTR	-10.0	PSTR.	0.0
OMEGTR	137.07999	NSSS	5.0	THSTR	-10.0	WLVT	273.0
KFR	15.0	PASCNT	1427.0	WLMT	234.0	FSVT	695.0
FSMT	700.40000	SMT	45.0	SVT	32.30000	OSTR.	0.0
LATSTK	-0.7150490	AIN	-1.2400906	IST	-0.66097055	XA	45.520469
LANGTK	10.096223	RIS	7.905121	IS	-3.0	XB	11.497442
CGLSTK	15.501452	THETA0	15.501452	TH5MR	5.5014520	XC	31.000000
PEDAL	23.591000	THETTR	29.712031	TH5TR	16.212031	XP	16.203457
XAIN	4.552000	XBIN	1.1497442	XCIN	3.1000000	XPIN	0.07496395
XOACTP	15.430922	XOACTI	1.5430922	RSTR.	0.0	PSTR	0.0
VXB	134.65000	THETAB	5.0997732	ARCF	3.1233969	OSTR	0.0
VYB	14.292419	PHIB	0.0	AAIF	-5.0396724	RSTR	0.0
VZB	12.017546	RETAWF	5.5400412	BBIF	0.2134100E-1	TSTR	0.0
P	0.0	GMC	0.0	AAFL	-3.9001306	HSTR	0.0
Q	0.0	OMGRAT	1.0	AAIL	0.21007200	JSTR	0.0
R	0.0	PSIDOT	0.0	ABIL	0.33310363	MMSTR	0.0
ALF.F	-0.67705070	EKTX	1.4160471	EKWF	0.91667421	LHSTR	0.0
CHITPP	81.202633	EKTZ	1.6073790	EKWFZ	1.0007173	OHSTR	0.0
EKTR	0.0	EPSMT	0.5054000	SIGY	0.94000359	VSTR	0.0
OKF	25.995102	KQMT	0.8717799	KQVT	0.81254771	VSTR	0.0
MUXS	0.16941364	CTSIG	0.60251451E-1	LTOT	2.2973439	ZSTR	0.0
MUYS	0.17920055E-1	CHSIG	-0.40000199E-2	DTOT	24.009434	LSTR	0.0
MUZS	0.62116452E-2	COMSIG	0.41469513E-6	TTR	914.20640	MSTR	0.0
LAMMR	-0.1009503E-1	NZ	0.99002522	WPHR	1410.4313	NSTR	0.0
DMSHH	0.17107000E-1	VC	0.0	WPHLK	1.0	AXP	2.0477020
XMR	2294.6309	HBAR	-1293.7999	VXDOT	-0.10001341E-1	AYP	-0.17060955E-1
YMR	-324.46021	JBAR	324.46421	VYDOT	-0.91565769E-2	AZP	-32.046421
ZMR	-19064.277	TBAR	19159.733	VZDOT	-0.19513996E-2	VXP	134.63440
LMR	-5538.0030	LBARM	-2220.1502	PDOT	-0.40471713E-2	VYP	14.292419
MMR	947.13549	MBARM	-14746.621	QDOT	0.69054394E-3	VZP	12.017546
NMR	25411.521	DBAR	20101.522	RDOT	-0.47716187E-4	RSTR.	0.0
XMF	-614.44516	XT	10.017197	XTR	0.0	PSIDMG	-150.0
YMF	-370.46377	YT	-141.63925	YTR	AS9.13600	RTR	2.0
ZMF	-52.449030	ZT	417.29761	ZTR	-312.70005	MADD	0.0
LMP	507.00217	LT	-356.11011	LTR	5276.0479	XADD	0.0
MMP	-3076.9300	MT	11047.035	MTR	-9600.5147	YADD	0.0
NMP	-3294.2009	NT	4510.9690	NTR	-26610.924	ZADD	0.0
XMT	12.109209	XVT	-2.0920122	ALFMTT	-5.7648229	NADD	0.0
YMT	-2.7437537	YVT	-150.09549	ALFVTT	6.2653794	LADD	0.0
ZMT	417.11105	ZVT	0.10656219	ARBF	5.0397176		



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RUN 19.

WEIGHT	19922.P	FSCG	362.24020	V	102.0	PSI102	2.2
IX	6260.0	WLCG	245.09999	DELS	-5.0	VXSTR.	0.2
IY	41507.0	RHO	0.23702202E-2	VOUNDO	1117.0	VYSTR.	0.2
IZ	30224.0	TIME	0.24022020E-1	DEL3-H	2.0	VZSTR.	0.2
O-EUMR	29.72000	NBS5	4.0	TSSTR	-10.0	WVSTR.	0.2
O-EUTR	137.07999	NBS8	5.0	TSSTR	-10.0	WVSTR.	0.2
KPR	15.0	PASCM	1259.0	WVSTR	-10.0	WVSTR	273.2
PSMT	720.42200	SMT	45.0	WVSTR	230.0	WVSTR	695.2
LATSTR	-0.66472623	A19	-1.2425347	WVSTR	32.32202	WVSTR	2.2
L-ESTK	12.140100	B19	0.5011313	WVSTR	-3.1902603	WVSTR	45.045506
CULSTR	16.070500	THETAB	16.070500	WVSTR	-3.2	WVSTR	7.0736077
PEDAL	24.061061	THETAB	30.769742	WVSTR	5.995500	WVSTR	34.941231
XAIN	0.5085500	XBIN	0.70734077	WVSTR	17.269742	WVSTR	14.902503
XBACTP	9.2460792	XBACTI	0.92460791	WVSTR	3.4941251	WVSTR	2.82461000
VIB	100.52400	THETAB	4.2905974	WVSTR	0.2	WVSTR	0.2
VIB	14.399203	PHIB	2.0	WVSTR	3.1235591	WVSTR	0.2
VIB	12.656104	RETABF	4.4079102	WVSTR	-5.7161325	WVSTR	0.2
P	0.2	GAMC	0.0	WVSTR	0.07333581E-3	WVSTR	0.2
Q	0.2	GAMGRAT	1.0	WVSTR	-4.4294557	WVSTR	0.2
R	0.0	PSIDOT	0.0	WVSTR	2.23465514	WVSTR	0.2
ALP-F	0.51612054	EXTX	1.3949970	WVSTR	0.42551923	WVSTR	0.2
C-TIPP	0.1800635	EXTZ	1.4092091	WVSTR	0.92420223	WVSTR	0.2
E-T	0.0	EPSHT	0.49427910	WVSTR	1.2081313	WVSTR	0.2
O-F	30.190503	KQMT	0.27177979	WVSTR	2.01993160	WVSTR	0.2
MUS	0.21107279	CTSIG	2.60347305E-1	WVSTR	2.02452001	WVSTR	0.2
MUS	0.10257721E-1	CHSIG	-0.40840533E-2	WVSTR	3.7721906	WVSTR	0.2
MUS	0.47003037E-2	CHSIG	0.01210100E-6	WVSTR	24.556422	WVSTR	0.2
LAMBDA	-0.09520440E-2	WZ	0.99712299	WVSTR	1254.1073	WVSTR	0.2
O-S-M4	2.13741140E-1	VC	2.14305114E-4	WVSTR	1596.9259	WVSTR	0.2
WAB	2350.7740	WAB	-1340.6069	WVSTR	1.0	WVSTR	2.4052013
WAB	-327.23460	JAB	327.23460	WVSTR	-0.3377150E-2	WVSTR	-0.3650092E-1
Z-R	-19000.270	LABH	19100.441	WVSTR	-2.10796972E-1	WVSTR	-32.203037
L-R	-0306.3009	LABH	-2479.3970	WVSTR	2.27409139E-2	WVSTR	160.52404
M-R	-1522.0972	WABH	-14919.292	WVSTR	-2.1112170E-1	WVSTR	14.399023
M-R	2019.152	QAB	29552.422	WVSTR	2.72051041E-3	WVSTR	12.656104
X-F	-006.29779	XT	-17.014739	WVSTR	-2.12066422E-2	WVSTR	0.0
Y-F	-01.62434	YT	-212.97063	WVSTR	0.2	WVSTR	-150.0
Z-F	-152.26561	ZT	540.42292	WVSTR	990.60571	WVSTR	2.0
L-F	705.71753	LT	-471.40610	WVSTR	-362.50001	WVSTR	0.0
M-F	-3394.0900	MT	16119.754	WVSTR	6204.0232	WVSTR	0.0
M-F	-0003.7102	NT	5943.4235	WVSTR	-11171.995	WVSTR	0.0
X-T	-10.255064	XVT	-6.7500745	WVSTR	-32694.745	WVSTR	0.0
Y-T	-2.9446552	YVT	-210.03370	WVSTR	-5.6100302	WVSTR	0.0
Z-T	500.13721	ZVT	0.20571432	WVSTR	4.910772	WVSTR	0.0
				WVSTR	5.7161391	WVSTR	0.0

UTTA8(S76) 1-21-77 9-DEC-77 RUN 20.

WEIGHT	1900.0	FSCG	360.20000	V	120.0	PSIR2	0.0
IX	6260.0	MLCG	245.09999	DELS	-5.0	VXSTR.	0.0
IY	41907.0	RHO	0.23700000E-2	V SOUND	1117.0	V9STR.	0.0
IZ	30224.0	TIME	0.20000000E-1	DEL3MR	0.0	V2STR.	0.0
OMEGR	29.72000	NBS3	4.0	THSTR	-16.0	PSIR.	0.0
OMEGR	137.07999	NBS3	5.0	THSTR	-16.0	MLVT	273.0
KR	15.0	PASCNT	1970.0	MLMT	234.0	FSVT	695.0
FSMT	700.00000	AMT	45.0	SVT	32.30000	OSTR.	0.0
LAT6TK	-0.72002374	A18	-1.3971259	IMT	-5.1240397	XA	45.457351
LM6TK	14.149999	R13	10.374674	IS	-3.0	XB	0.0
COL6TK	16.907700	THETAB	16.907700	TH7SMR	6.9077003	XC	40.673670
PEDAL	25.000727	THETTR	33.400073	TH7STR	19.990073	XP	10.300314
XAIN	0.5457351	XBIN	0.0	XCIN	4.0673677	XPIN	0.50095439
XOACTP	0.46556752	XOACTI	0.46556752E-1	RSTR.	0.0	PSIR	0.0
VXB	202.30529	THETAB	3.6517221	AA0F	3.1256101	OSTR	0.0
VYR	15.319704	PHID	0.0	AAIF	-6.7929436	RSTR	0.0
VZB	12.917360	BETAWF	4.154007	BBIF	-0.00790551E-1	TITR	0.0
P	0.0	GAMC	0.0	AAFL	-5.3466337	MITR	0.0
Q	0.0	OMGRAT	1.0	AAIL	0.26640419	JITR	0.0
R	0.0	PSIDOT	0.0	ABIL	0.56004102	MMITR	0.0
ALP4F	0.90000509	EKTX	1.4552094	EKMF	0.01643035	LMITR	0.0
CHITPP	01.203075	EKTZ	1.6550753	EKMFZ	1.0007361	OMITR	0.0
EKTR	0.0	EPSWT	0.49150690	SIGWT	0.73122557	XITR	0.0
OKP	53.139541	KOMT	0.47177979	KOVT	0.02071133	YITR	0.0
MUXS	0.25029060	CTSIG	0.60039306E-1	LTOT	4.4343106	ZITR	0.0
MUYS	0.19212360E-1	CHSIG	-0.50432062E-2	DTOT	24.706343	LITR	0.0
MUZS	0.20931406E-2	CHMSIG	0.41490097E-6	TTR	1292.9737	MITR	0.0
LAMBMR	-0.06002910E-2	NZ	0.99750623	MPMR	1920.0460	NITR	0.0
DSHMR	0.11501432E-1	VC	0.7152573E-5	KTRBLK	1.0	AP	2.0164442
XMR	2537.1915	MBAR	-1520.0541	VX0DOT	0.4546011E-2	ATP	-0.51147725E-2
VPR	-360.05666	JBAR	360.05666	VY0DOT	-0.77302145E-2	AZP	-32.030599
ZPR	-19216.025	TBAR	19324.700	VZ0DOT	0.13155201E-1	VXP	202.30529
LPR	-7746.7114	LBARM	-3717.0741	PDOT	-0.31503696E-2	VYP	15.319704
MPR	-5916.5070	MBARM	-22406.000	DDOT	0.23261606E-1	VZP	12.917360
MRR	34053.410	DBAR	35695.334	RODT	-0.33879355E-2	RSTR.	0.0
MPF	-1270.0206	XT	-44.200230	XTR	0.0	PSIDMG	-150.0
YPF	-579.57605	YT	-279.24160	YTR	1215.0001	STR	2.0
ZPF	-257.56423	ZT	075.40005	ZTR	-442.25679	MADD	0.0
LMP	009.51607	LT	-617.00076	LTR	7463.1120	XADU	0.0
MMP	-4220.0539	MT	24016.015	MTR	-13702.509	YADD	0.0
NMP	-5120.7702	NT	7742.6092	NTR	-37647.401	ZADD	0.0
XMT	-33.210424	XVT	-13.061014	ALFMTT	-6.3456064	MADD	0.0
YMT	-3.9290070	YVT	-275.31179	ALFVTT	4.3320620	NADD	0.0
ZMT	075.20600	ZVT	0.27037634	AA0IF	6.7934240	LADD	0.0

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WEIGHT	1990P.P	FSCG	300.20000	V	DEL3	60.0	PSITR2	0.0
IX	6260.0	WLCG	205.9999	V	VOUNO	-5.2	VXSTR.	0.0
IY	41507.0	RHO	0.23702000E-2	V	VOUNO	1117.0	VYSTR.	0.0
IZ	30224.0	TIME	0.20002000E-1	V	DEL3-MR	0.0	VZSTR.	0.0
OMEGMR	25.64999	W093	0.0	V	W093-MR	-1A.0	W093	0.0
OMEGTR	110.32230	W993	5.0	V	W993-MR	-1A.0	W993	0.0
KFR	15.0	PASCNT	1015.0	V	W093	234.0	W093	0.0
FSMT	700.0000	SHY	45.0	V	W093	32.30000	W093	0.0
LATSYK	-1.1143000	A18	-1.0366022	V	W093	15.097291	W093	0.0
LNGSTK	5.3100954	B18	5.0574330	V	W093	-3.0	W093	0.0
COLSTA	17.493420	THETAB	17.493420	V	W093	7.4134200	W093	0.0
PEDAL	12.190950	THETTR	20.007054	V	W093	7.1070542	W093	0.0
XAIN	4.3035624	XBIN	5.1205315	V	W093	4.3033475	W093	0.0
XEACTP	36.043353	XEACTI	3.6043353	V	W093	2.0	W093	0.0
V0	101.19230	THETAB	3.60554366	V	W093	4.0633621	W093	0.0
V0	12.310592	PHIB	0.0	V	W093	-2.5242755	W093	0.0
V0	6.4652500	RETAMF	5.9973912	V	W093	0.65069069E-1	W093	0.0
P	0.0	GAMC	1.0	V	W093	-4.7997730	W093	0.0
O	0.0	OMGRAT	1.0	V	W093	0.26241277	W093	0.0
R	0.0	PSIDOT	0.0	V	W093	0.10505260	W093	0.0
ALP=F	-5.5905902	EKTX	1.3616490	V	W093	0.00000107	W093	0.0
CHILPP	70.210353	EKTX	1.3616490	V	W093	1.0117016	W093	0.0
EXTR	0.0	EP9MT	0.50997390	V	W093	1.0036705	W093	0.0
OMF	16.543600	KQMT	0.07177979	V	W093	0.00255461	W093	0.0
MUX0	0.14732006	CT9IG	0.00102200E-1	V	W093	-3.7422789	W093	0.0
MUY0	0.17000000E-1	CH9IG	-0.30037924E-2	V	W093	25.372659	W093	0.0
MUZ0	0.16056370E-2	COM9IG	0.79665479E-6	V	W093	0.15.17476	W093	0.0
LAMBMR	-0.24000000E-1	NZ	0.99709500	V	W093	1116.0431	W093	0.0
OMHMR	0.25606121E-1	VC	0.35762746E-5	V	W093	1.0	W093	0.0
XMR	1630.7650	W0AR	-644.02196	V	W093	-0.98053992E-4	W093	0.0
YMR	-0.04.97912	J0AR	404.97912	V	W093	-0.25446759E-2	W093	0.0
ZMR	-12796.090	T0AR	10057.145	V	W093	0.10246533E-2	W093	0.0
LPR	-4900.0311	LBARM	-1270.6740	V	W093	-0.50966543E-3	W093	0.0
MPR	15122.247	MBARM	-6114.2667	V	W093	0.11013627E-3	W093	0.0
NPR	23160.601	QBARM	23930.749	V	W093	-0.19505591E-3	W093	0.0
XPF	-306.45109	XT	-27.321130	V	W093	0.0	W093	0.0
YPF	-260.92967	YT	-101.67155	V	W093	766.07257	W093	0.0
ZPF	100.00502	ZT	-72.907055	V	W093	-270.02746	W093	0.0
L0F	477.06000	LT	-225.51177	V	W093	4705.2320	W093	0.0
M0F	-4303.4137	MT	-2090.9165	V	W093	-0.639.0040	W093	0.0
N0F	-2260.5501	NT	2037.2036	V	W093	-23735.422	W093	0.0
XMT	-27.610196	XVT	0.20905771	V	W093	1.5276435	W093	0.0
YMT	-1.2604004	YVT	-100.41109	V	W093	7.3053554	W093	0.0
ZMT	-72.037101	ZVT	-0.69074630E-1	V	W093	2.5251349	W093	0.0

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UTIAS(S76)

WEIGHT	19900.0	FSCG	369.20000	V	00.0	PSIR2	0.0
IX	6200.0	WLCG	245.8999	DELS	-5.0	VISTR.	0.0
IY	41507.0	RMO	0.23700000E-2	VOUNO	1117.0	VISTR.	0.0
IZ	30224.0	TIME	0.20200000E-1	DEL3MR	0.0	VZSTR.	0.0
DEGMR	25.64999	NBS5	4.0	TMSTR	-10.0	PSW.	0.0
OPETR	110.32250	NBS5	5.7	TMSTR	-10.0	WLV	273.2
KPR	15.0	PASGNT	1343.0	WLV	234.0	FSVT	695.0
FMT	700.40700	SMT	45.0	SVT	32.30200	OSTR.	0.0
LATSK	-1.0331856	AIS	-1.7400650	IHT	1.3570012	XA	43.542590
LCSTK	0.0954724	015	0.4032327	IS	-3.0	XB	21.394090
COLSK	17.614760	THEYAB	17.614760	TH75MR	7.5307601	XC	44.592251
PEDAL	10.707400	THEYTR	19.249200	TH75TR	5.7692003	XP	51.919004
XIN	4.3542590	XOIN	2.1394290	XCIN	4.4592251	XPIN	2.0035964
XOACTP	25.410750	XOACTI	2.5410750	OSTR.	0.0	OSTR	0.0
VX0	134.61045	THEYAB	5.3136714	AAEF	4.4600576	OSTR	0.0
VX0	11.377554	PHIB	2.0	AAIF	-5.0645150	OSTR	0.0
VZ0	12.520339	MEYAF	4.4030309	ABIF	0.10794234	OSTR	0.0
P	0.0	GAMC	0.0	ABOL	-4.6959404	OSTR	0.0
Q	0.0	OMGRAT	1.0	ABIL	0.3520570	OSTR	0.0
R	0.0	PSI00T	0.0	BBIL	0.36514841	OSTR	0.0
ALP.F	-0.45797920	ERTX	1.4013349	EKWF	0.91945726	OSTR	0.0
C-110P	01.496714	ERTZ	1.4007715	EKWFZ	1.0045032	OSTR	0.0
EAT	0.0	EPST	0.49403030	SIGMT	0.77433489	OSTR	0.0
QPR	25.001134	KQMT	0.47177979	KQVT	0.2751174	OSTR	0.0
MUXS	0.19626972	CTSIG	0.90066701E-1	LTOT	2.2114023	OSTR	0.0
MUY5	0.1045935E-1	CM5IG	-0.04453533E-2	DTOT	24.460007	OSTR	0.0
MUZ3	0.79301620E-2	CM5IG	0.79452923E-6	TTR	0.16.2308	OSTR	0.0
LAMMR	-0.1102050E-1	NZ	0.99500643	HPMR	1000.4997	OSTR	0.0
O-SMMH	0.19733020E-1	VC	0.71529573E-5	RTBRLK	1.0	OSTR	0.0
XMR	2302.9949	WBAR	-1309.5454	VX00T	0.15337902E-2	OSTR	0.0
YMR	-339.76671	JBAR	339.76671	VY00T	-0.10671942E-1	OSTR	0.0
ZMR	-10920.916	TBAR	19021.103	VZ00T	0.10621177E-2	OSTR	0.0
LMR	-4010.5007	LBARM	-1451.7616	PDOT	-0.54754573E-2	OSTR	0.0
MMR	4612.1125	MBARM	-12314.596	QDOT	0.10814745E-2	OSTR	0.0
NMR	22059.057	QBAR	23309.150	ADOT	0.10814745E-2	OSTR	0.0
MMR	-612.37447	XT	-2.0059710	ZTR	2.2	OSTR	0.0
YMR	-290.55915	YT	-135.00009	PSIDMG	-150.0	OSTR	0.0
ZMR	-52.349173	ZT	240.32375	BT	4.0	OSTR	0.0
LPR	460.66064	LT	-299.99599	MADD	0.0	OSTR	0.0
MPR	-2009.1767	MT	7052.3756	YADD	0.0	OSTR	0.0
NPR	-2066.2677	NT	3769.4577	ZADD	0.0	OSTR	0.0
XPT	2.4451756	XVT	-4.4911475	ALFMTT	-3.4009646	OSTR	0.0
YPT	-1.5574429	YVT	-133.52344	ALFVTT	4.054196	OSTR	0.0
ZPT	247.90613	ZVT	0.37761092	AAB6IF	5.2656660	OSTR	0.0

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WEIGHT	19900.0	FSCG	360.20000	V	100.0	PSITR2	0.0
IA	6260.0	WLCG	245.99999	DELS	-5.0	VASTR.	0.0
IV	41507.0	RHO	0.23700000E-2	V SOUND	1117.0	VASTR.	0.0
I2	30224.0	TIME	0.20000000E-1	DEL3MR	0.0	VZSTR.	0.0
DEGMM	25.649999	N0SS	4.0	TH3MR	-1A.0	PSTR.	0.0
DEGTR	110.32250	NSSS	5.0	TH5TR	-1A.0	WLVT	273.0
KFR	15.0	PASCHT	734.0	WLMT	234.0	FSVT	695.0
F0M1	700.40000	SMT	45.0	SVT	32.300000	OSTR.	0.0
LATSK	-1.0312716	AIS	-1.0287007	IMT	-1.0411474	YA	43.554552
LGSTK	9.0102219	BIS	10.001302	IS	-3.0	XB	10.133491
CULSTK	10.222006	THETA0	10.222006	TH7MR	0.1420064	XC	40.392540
PEDAL	9.7795515	THETTR	19.070919	TH5TR	5.5709190	XP	54.492261
XAIN	0.3554551	XBIN	1.0133490	XCIN	4.0392540	XPIN	2.9425055
XOACTP	20.353026	XOACTI	2.0353026	RSTR.	0.0	PSTR	0.0
VXB	160.49340	THETAB	4.4169025	AAZF	4.4330706	OSTR	0.0
VVB	10.530105	PMIB	0.0	AAIF	-5.4631660	PSTR	0.0
VZ0	13.015705	RETAHF	3.3736040	BBIF	0.16941002	TITR	0.0
P	0.0	GAMC	0.0	AAAL	-5.0002702	JITR	0.0
Q	0.0	OMGRAT	1.0	AAIL	0.3700704	MITR	0.0
R	0.0	PSIDOT	0.0	BBIL	0.41706320	MMITR	0.0
ALF.F	0.05760469	ERTX	1.3595030	EKWF	0.92951579	LMITR	0.0
C-TTPP	0.2270446	ERTZ	1.6405924	EKWFZ	1.0077295	DMITR	0.0
EATR	0.0	EP9MT	0.40373694	SIGAT	0.59376052	XITR	0.0
QAF	30.065721	KOMT	0.07177979	KOVT	0.43247253	VITR	0.0
MUXS	0.24547100	CT9IC	0.90005233E-1	LTOT	3.5331622	ZITR	0.0
MUYS	0.15312795E-1	CM9IG	-0.67155750E-2	DTOT	24.452018	LITR	0.0
MUZS	0.00722517E-2	COM9IG	0.79010591E-6	TTP	0.98.59902	MITR	0.0
LAMDMR	-0.97344651E-2	NZ	0.99479045	MFMR	1177.5302	NITR	0.0
D9MHR	0.15006710E-1	VC	0.7150573E-5	KTRBLK	1.0	AXP	2.4621393
XMR	2306.7646	MBAR	-1404.2200	VXBDOT	-2.13490022E-1	AYP	-0.43255973E-1
YMR	-309.46253	JBAR	349.46253	VYBDOT	-0.17294303E-1	AZP	-32.073531
ZMR	-19003.121	TBAR	19004.131	VZBDOT	0.60194110E-2	VXP	166.49340
LHR	-510.4126	LBARM	-1993.9741	PDOT	-2.11931120E-1	VYP	10.530105
MHR	3615.9116	MBARM	-13100.757	QDOT	0.07663020E-3	VZP	13.015705
NHR	24331.416	OBAR	25209.107	PDOT	0.16261166E-2	RSTR.	0.0
XFF	-910.00404	XT	-23.001094	XTR	0.0	PSIDMG	-150.0
YFF	-336.79717	YT	-160.47020	YTR	0.0	BTR	4.0
ZFF	-144.97466	ZT	320.72285	ZTR	-327.36241	MAOD	0.0
LFF	520.54290	LT	-375.30099	LTR	5106.7612	XACD	0.0
MFF	-3309.3500	MT	9333.0069	MTR	-9523.1120	YADD	0.0
NFF	-2979.0364	NT	4721.0222	NTR	-26164.404	ZADD	0.0
XMT	-12.257109	XVT	-11.504704	ALFMTT	-3.274023	MAOD	0.0
YMT	-1.5633330	YVT	-146.90695	ALFVTT	3.5723047	LAOD	0.0
ZMT	320.27262	ZVT	0.45023344	AABIF	5.4657922		

UTTAS(976) 1-21-77 9-DEC-77 RUN 24.

WEIGHT	1900.0	PSCG	360.20000	V	120.0	PSITR2	0.0
IX	6260.0	WLCG	245.69999	DELS	-5.0	VXSTR.	0.0
IY	41507.0	RMO	0.23700000E-2	V SOUND	1117.0	VYSTP.	0.0
IZ	30224.0	TIME	0.20000000E-1	DEL3MR	0.0	VZSTR.	0.0
OMENR	25.69999	NBS	4.0	TMSTR	-14.0	PSTR.	0.0
OMECTR	110.32250	NSS	5.0	TMSTR	-14.0	WLVT	273.0
KFR	15.0	PASCNT	734.0	WLMT	234.0	F3VT	695.0
PSMT	700.00000	SHY	45.0	SVT	32.30000	QSTR.	0.0
LATSTK	-1.2012029	AIS	-2.1545959	INT	-2.7932671	XA	42.242481
LAGESTK	10.526190	RIS	12.003467	IS	-3.0	XB	12.698972
CULSTK	19.347092	THETA0	19.347092	TH7MR	9.2670929	XC	55.424332
PEDAL	9.090772	THETTR	19.740548	TH7STR	9.2405406	XP	56.370694
XAIN	4.2242401	XBIN	1.2690972	XCIN	5.5424332	XPIN	3.0443703
XACTP	13.102046	XBACTI	1.3102046	RSTR.	0.0	PSTR	0.0
VXB	202.37653	THETAB	3.690997	AAOF	4.4399445	QSTR	0.0
VYB	11.202683	PHIB	0.0	AAIF	-6.3350158	RSTR	0.0
VZB	13.004149	METAF	3.0600500	MOIF	0.72793074E-1	TSTR	0.0
P	0.0	GMC	0.0	AAOL	-6.0197218	WTR	0.0
Q	0.0	OMGRAT	1.0	AAIL	0.42263350	JSTR	0.0
R	0.0	PSIOOT	0.0	MOIL	0.52650947	MTSTR	0.0
ALFPP	1.2500231	EKTX	1.4151984	EKMF	0.92336560	LMSTR	0.0
CHITPP	01.797354	EKTZ	1.6410714	EKWFZ	1.0002026	OMSTR	0.0
EKTR	0.0	EPSMT	0.4000049	SIGMT	0.53454879	XSTR	0.0
QAF	52.995270	KQMT	0.07177979	KQVT	0.03397817	VSTR	0.0
MUXS	0.29464009	CTSIG	0.91227919E-1	LTOT	4.1299011	ZSTR	0.0
MUYB	0.16394733E-1	CHSIG	-0.73962822E-2	DTOT	24.509656	LSTR	0.0
MUZB	0.35940713E-2	COMSIG	0.7914110E-6	YTR	1079.6046	MSTR	0.0
LAMBMR	-0.90315197E-2	NZ	0.99795217	MPMR	1392.9969	WTR	0.0
D-SMMR	0.13226391E-1	VC	0.14305114E-4	KTRBLK	1.0	XTP	2.0579582
XMR	2542.6446	HBAR	-1546.7649	VXBDOT	-0.12965316E-1	AYP	-0.52401133E-1
YMR	-370.97399	JBAR	370.97399	VYBDOT	-0.22267100E-1	AZP	-32.100374
ZMR	-10967.224	TBAR	19075.787	VZBDOT	-0.12950307E-2	VAP	202.37653
LPR	-6400.3585	LBARM	-2451.9144	PDOT	-0.14140191E-1	VVP	11.202683
MRR	777.58178	MBARM	-15267.100	QDOT	0.22700711E-2	VZP	13.084149
NMR	29061.721	QBARM	29069.330	RDOT	0.16331273E-2	PSTR.	0.0
XMF	-1273.6230	XT	-45.203449	XTR	0.0	PSIDMG	-150.0
YMF	-425.57035	YT	-223.31336	YTR	1014.6471	OTR	4.0
ZMF	-242.51104	ZT	530.12750	ZTR	-359.32200	MADD	0.0
LMF	659.00979	LT	-497.05230	LTR	6231.9973	XADD	0.0
NMF	-4203.9240	MT	15042.990	MTR	-11442.209	YADD	0.0
XMT	-3760.6631	NT	6231.3654	NTR	-31437.151	ZADD	0.0
YMT	-27.094164	XVT	-10.109265	ALFMTT	-3.0656400	MADD	0.0
YMT	-2.0503715	YVT	-221.20290	ALFVTT	3.1700531	LADD	0.0
ZMT	929.70050	ZVT	0.33900129	AA00IF	6.3354340		

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RUN 25.

WEIGHT	19900.0	FSCG	360.20000	V	140.0	PSIR2	0.0
IX	6260.0	WLCG	245.89999	DELS	-5.0	VXSTR.	0.0
IY	41507.0	PHO	0.23700000E-2	V SOUND	0.7	VYSTR.	0.0
IZ	38224.0	TIME	0.20000000E-1	DEL3MR	-18.0	VZSTR.	0.0
OMEGMR	25.64999	NSS	5.0	THSTR	-18.0	PLVT	273.0
OMEGTR	118.32250	NSS	5.0	THSTR	-18.0	FSVT	695.0
KFR	15.0	PASCNT	545.0	WMT	32.300000	OSTR.	0.0
PSHT	700.40000	SHT	45.0	YVT	-3.9155390	XA	39.100325
LATSTK	-1.7426600	AIS	-2.0255022	IMT	-3.0	XB	5.460036
LNGSTK	12.602532	BIS	10.707116	IS	10.913729	XC	65.71012
CULSTK	20.993729	THETA0	20.993729	TH5MR	7.6135644	XP	50.007546
PEDAL	0.4970009	THETTR	21.113564	XCIN	6.5710012	XPIN	3.1344859
XAIN	3.9100324	XOIN	0.54600036	RSYH.	0.0	OSTR	0.0
XOALTP	4.2752305	XOACTI	0.42752305	AARF	4.4791231	RSTR	0.0
VX0	236.22023	THETA0	3.1344640	AAIF	-7.5695760	TITR	0.0
VY0	12.650036	PHIB	0.0	AAIF	-0.20720963	MTR	0.0
VZ0	12.936097	DETAWF	3.0103030	AAEL	-7.5708539	JTR	0.0
P	0.0	GANC	0.0	AAEL	0.49024679	MHTR	0.0
O	0.0	OMGRAT	1.0	BBIL	0.60751014	LMTR	0.0
R	0.0	PSIDOT	0.0	EXMPX	0.90069129	DMTR	0.0
ALFWF	1.1764397	EXTX	1.49908578	EKWFZ	1.0093314	XITR	0.0
CHITPP	0.660562	EKTZ	1.4719400	SIGMT	0.53123541	ZITR	0.0
EXTR	0.0	EPST	0.40010302	KQVT	0.83417000	LITR	0.0
QF	70.645015	KQVT	0.47177979	LTOT	4.3209443	MTR	0.0
MUXS	0.34370716	CISIG	0.91857910E-1	DTOT	24.536600	NITR	0.0
MUY9	0.10672335E-1	CMSIG	-0.85570176E-2	TTR	1373.4589	AXP	1.7454004
MUZ3	0.80690709E-3	CMMSIG	0.79039460E-6	HPMR	1754.9047	AYP	0.53346055E-1
LAMBMR	-0.10601267E-1	NZ	0.99977009	KTRBLK	1.0	AZP	-32.191099
DASHMR	0.11400175E-1	VC	0.71525573E-5	VX000T	-0.30997069E-1	VXP	236.22023
YMR	2792.0645	MBAR	-1789.4423	VZ000T	0.33907549E-1	VYP	12.050036
ZMR	-412.42414	TBAR	412.42414	QOOT	0.15292613E-1	VZP	12.936097
LMR	-19086.055	LBARM	19207.519	ROOT	-0.12315566E-1	PSIOHG	-150.0
MMR	-0042.7057	MBARM	-3442.7019	XTR	0.0	MTR	4.0
MMR	-3476.6411	QBAR	10220.176	YTR	1290.7252	MADD	0.0
XPF	36705.714	XT	37629.536	ZTR	-469.78647	XADD	0.0
YPF	-1699.4940	YT	-69.632660	MTR	7927.6781	YADD	0.0
ZPF	-559.69024	ZT	612.66937	NTR	-14555.550	ZADD	0.0
LMP	867.61330	LT	-604.83744	ALFATY	-39902.969	NADD	0.0
MPF	-5331.2277	MT	23051.252	ALFVY	-4.4057417	LADD	0.0
MPF	-4944.7711	MYT	8329.0489	AAR01F	7.5724115		
MYT	-44.626930	XVT	-25.005721				
YMT	-2.8443798	YVT	-295.64196				
ZMT	812.41951	ZVT	0.24006309				

UTTAS(376) 1-21-77 9-DEC-77 RUN 26.

WEIGHT	19900.0	FSCG	360.20000	V	150.0	PSIIR2	0.0
IX	6246.0	WLCG	245.09999	DELS	-5.2	VXSTR.	0.0
IY	41507.0	RHO	0.23700000E-2	V SOUND	1117.0	VYSTR.	0.0
IZ	30224.0	TIME	0.24000000E-1	DEL3MR	0.0	VZSTR.	0.0
OMEGMR	25.64999	NBS	4.0	THSTR	-19.0	PSTR.	0.0
OMEGTR	110.32250	NBS	5.0	THSTR	-19.0	WLVT	273.0
KPR	15.0	PASCNT	3294.0	WLHT	234.0	FSVT	495.0
FSMT	700.40000	SH	45.0	IMT	32.30000	OSTR.	0.0
LATSTK	-2.216159	AIS	-3.4129692	IS	-4.3206919	XA	36.149004
LGSTK	14.14999	AIS	15.79999	THSTR	-3.0	XB	0.0
CULSTK	22.099517	THETAY	22.099517	THSTR	12.019517	XC	72.621904
PEDAL	0.302531	THETTR	22.325904	THSTR	A.259404	XP	50.365030
XAIN	3.6149004	XBIN	0.0	XCIN	7.2621904	XPIN	3.1516301
XBACTP	-2.2396354	XBACTI	-0.22396354	RSTR.	0.0	PSTR	0.0
VX0	253.29009	THETAB	2.3192952	A0F	4.5502531	OSTR	0.0
VY0	13.701456	PHI0	0.0	AAIF	-7.6023703	RSTR	0.0
VZ0	10.250742	RETAUF	3.0307912	0BIF	-0.37113694	TITR	0.0
P	0.0	CANC	0.0	AAFL	-0.0421291	HITR	0.0
Q	0.0	CMGRAT	1.0	AAFL	0.55023757	JITR	0.0
ALFAF	0.60601377	PSIOOT	0.0	0BIL	0.68174652	MMITR	0.0
CRITPP	00.042700	EKTZ	1.6000454	EKAFY	0.90055507	LMITR	0.0
EKTZ	0.0	EPSMT	0.40030791	EKAFZ	1.00099572	OMITR	0.0
QAF	00.600742	KUMT	0.87177979	SIGMT	2.53341925	HITR	0.0
MUX3	0.36030113	CTSIG	0.93234225E-1	KQVT	0.83411050	VITR	0.0
MUX5	0.20026251E-1	CHSIG	-0.03591531E-2	LTOI	3.3031420	ZITR	0.0
MUZS	-0.43760047E-2	CHSIG	0.01249943E-6	DTOT	24.307962	LITR	0.0
LAMDR	-0.15174622E-1	NZ	1.0002731	TPR	1597.6634	MITR	0.0
DSMR	0.10790017E-1	VC	0.71525573E-5	WPR	2033.4914	NITR	0.0
XPR	2765.6450	WBAR	-1747.9015	KTRBLK	1.0	AXP	1.0020084
YMR	-002.65004	JBAR	402.45084	VX00T	-0.20309090E-1	AVP	0.1210000
ZMR	-19375.599	TBAR	19495.306	VY00T	0.59411606E-1	AZP	-31.099029
LMR	-9240.3032	LBARM	-4066.7670	VZ00T	-0.35327247E-1	VXP	253.29009
MMR	-2459.7066	WBARM	-14239.072	P00T	0.33700004E-1	VYP	13.701056
NMR	42530.435	OBAR	43403.130	Q00T	0.10044975	VZP	10.250742
XPF	-1929.0330	XT	-75.399421	R00T	-0.13412590E-3	RSTR.	0.0
YPF	-640.87034	YT	-343.04360	XTR	0.0	PSIDMG	-150.0
ZPF	-206.69001	ZT	1115.5512	YTR	1521.4242	ATR	4.0
LPF	992.91030	LT	-762.00700	ZTR	-506.47477	MANO	0.0
MPF	-3642.0055	MT	31444.102	LTR	9221.7983	XADD	0.0
NPF	-5666.7463	NT	9372.5640	WTR	-16931.609	YADD	0.0
XMT	-46.710259	XVT	-20.609141	ALFMTT	-46519.125	ZADD	0.0
YMT	-3.6612336	YVT	-339.34236	ALFVTT	-5.4067124	NADD	0.0
ZMT	1115.0077	ZVT	0.54353510	AABVTT	3.2094670	LADD	0.0



UTTAS(S7A) 1-21-77 9-DEC-77 RUN 27.

WEIGHT	1900.0	FSCG	360.20000	V	40.0	PSIR2	0.0
IX	6260.0	WLCG	245.49999	DELS	-5.0	VXSTR.	0.0
IY	41587.0	RHO	0.23780000E-2	VSDUND	1117.0	VYSTR.	0.0
IZ	30224.0	TIME	0.20000000E-1	DEL3MR	0.0	VZSTR.	0.0
OMEGMR	25.64999	NBS3	0.0	THSTR	-18.0	WLVT	273.0
OMEGTR	110.32250	NBS3	5.0	THSTR	-18.0	FSVT	695.0
KFR	15.0	PASCNT	1007.0	WLHT	234.0	QSTR.	0.0
FSHT	700.40000	SHT	45.0	SVT	32.30000	XA	38.317704
LATSTK	-1.0691673	AIS	-2.6567322	IHT	20.714152	XB	35.273604
COLSTK	4.1675690	BIS	4.3301650	IS	-3.0	XC	47.789131
PEDAL	18.126260	THETA0	10.126260	TH5MR	8.0442609	XP	46.223361
XAIN	12.762309	THETTR	21.937822	TH5STR	4.7789131	XPIN	2.4959965
XACTP	3.4317704	XBIN	3.5273604	XCIN	0.0	PSTR	0.0
XACTI	41.020402	YBACTI	4.1020402	RSTR.	4.6145207	QSTR	0.0
VXB	67.405900	THETA0	4.3330896	AADF	-2.5366971	RSTR	0.0
VYB	0.0	PHIB	-1.3741857	AAIF	-0.19851061	TITR	0.0
VZB	5.1006221	GETAWF	0.0	ABIF	-5.0288369	MTR	0.0
P	0.0	GAMC	0.0	AABL	0.29556190	JTR	0.0
Q	0.0	OMGRAT	1.0	ABIL	0.13382036	MHTR	0.0
R	0.0	PSIDOT	0.0	EBIL	0.76153032	LHTR	0.0
ALF.F	-13.715266	EKTX	1.1083357	EKWX	1.0203787	OHTR	0.0
CHITPP	67.010641	EKTZ	2.0450841	EKWFZ	0.0	XITR	0.0
EXTR	0.0	EPSMT	0.44999999	SIGMT	0.0	VITR	0.0
QWF	9.5327540	KOHT	0.47177979	KOVT	0.0	ZITR	0.0
MUXS	0.98193366E-1	CTSIG	0.91022367E-1	LTOT	-21.916640	LITR	0.0
MUYS	0.0	CHSIG	-0.32369161E-2	DTOT	26.850100	MTR	0.0
MUZS	0.0	COMSIG	0.22252902E-6	TTR	972.90912	NITR	0.0
LAMMR	-0.35075020E-1	NZ	0.99705450	MPMR	1350.3650	AXP	2.4749037
D-SMR	0.37362377E-1	VC	0.11183023	KTRBLK	1.0	AYP	0.76263065
XMR	1671.9300	MBAR	-676.04010	VXDOOT	0.02745251E-1	AZP	-32.079715
YMR	-455.56431	JBAR	455.56431	VYDOOT	-0.09118836E-2	VXP	67.405900
ZMR	-18969.022	TBAR	19032.806	VZDOOT	-0.93508340E-2	VYP	0.0
LMR	-5595.1043	LBARH	-1344.8160	PUOT	0.30914651E-3	VZP	5.1086221
MMR	15231.157	MBARH	-6045.0067	QDOT	-0.24649542E-3	PSTR.	0.0
NMR	20090.403	QBAR	20955.214	RDOT	-0.65380024E-3	PSIDHG	-150.0
XMF	-199.19360	XT	-0.0711225	XTR	0.0	BTR	4.0
YMF	0.0	YT	-7.5864569	YTR	914.30350	MADD	0.0
ZMF	263.67519	ZT	7.1504856	ZTR	-332.77990	XADD	0.0
LAF	0.0	LT	-17.132740	LTR	5615.6A31	YADD	0.0
MAF	-5134.6506	MT	203.87240	MTR	-10310.630	ZADD	0.0
NMT	0.0	NT	211.66214	NTR	-20320.169	NADD	0.0
XMT	-2.0771792	XVT	-1.9939432	ALFHTT	-0.10366430	LAOD	0.0
YMT	0.0	VVT	-7.5864569	ALFVTT	0.0		
ZMT	6.0535030	ZVT	1.0949417	AAR01F	2.5404532		

UTTAS(S76) 1-21-77 9-DEC-77 RUN 20.

WEIGHT	19900.0	PSGG	360.20000	V	1.2E-2	PSITR2	0.0
IX	6268.0	WLCG	205.89999	DEL3	-5.0	VXSTR.	0.0
IY	41507.0	RMO	0.23700000E-2	VSOUND	1117.0	VYSTR.	0.0
IZ	30224.0	TIME	0.20000000E-1	DEL3MR	0.0	VZSTR.	0.0
OMEGMR	25.64999	WSSS	4.0	TMSTR	-10.0	PSSTR.	0.0
OMEGTR	110.32250	WSSS	5.0	TMSTR	-10.0	WLVT	273.0
KFR	15.0	PASCHT	902.0	WLMT	230.0	FSVT	695.0
PSMT	700.00000	SMT	45.0	IS	32.300000	OSTR.	0.0
LATSTK	-0.36749140	AIS	-1.3241605	IS	30.697220	XA	47.703170
LNGSTK	3.0944746	AIS	2.0743210	IS	-3.0	XB	39.065460
COLSTK	19.760126	THETA0	19.740126	TH75MR	9.6001264	XC	50.050790
PEDAL	10.706017	THETTR	29.051769	TH75TR	16.351769	XP	29.746014
XAIN	4.7703177	XBIN	3.9065459	XCIN	5.0050790	XPIN	1.6062430
XGACTP	46.041374	XOACTI	4.0041374	RSIR.	0.0	PSIR	0.0
VX0	0.16022472E-1	THETA0	5.4029340	AA0F	4.6020725	OSTR	0.0
VY0	0.0	PHI0	-2.6765260	AA1F	-2.2102575	OSTR	0.0
VZ0	0.1600099E-2	MEYAF	0.0	AA1F	-1.464503	OSTR	0.0
P	0.0	GMC	0.0	AA0L	-0.0651009	MITR	0.0
Q	0.0	OMGRAT	1.0	AA1L	-0.22407071E-1	JITR	0.0
R	0.0	PSIDOT	0.0	BB1L	0.21040305	WHITR	0.0
ALFWF	-10.260523	EXTX	-0.25213616	BB1L	0.79995393E-5	LMITR	0.0
CHITPP	-2.191092	EXTZ	0.20412232	EXWFX	0.11099360E-3	CHITR	0.0
EKTR	0.0	EP9MT	0.40999999	SIGMT	0.0	XITR	0.0
Q-F	0.36167090E-6	KOHT	0.07177979	KOVT	0.0	XITR	0.0
MUXS	0.24531407E-4	CTSIG	0.00923043E-1	LTOT	-13.625257	ZITR	0.0
MUY3	0.0	CHSIR	-0.00404397E-2	DTOT	25.106093	LITR	0.0
MUZS	0.10551903E-5	COMSIG	0.03457001E-6	TTR	1347.0544	MITR	0.0
LAMBMR	-0.61719094E-1	NZ	0.99420142	MPMR	1069.0100	NITR	0.0
DASHMR	0.61720152E-1	VC	0.11069350E-3	KTABLK	0.79599999	AP	3.0681505
XMR	1016.7303	MBAR	-0.44.05722	VXRDOT	0.51204425E-2	ATP	1.5337919
YMR	-357.41200	JBAR	357.41200	VYRDOT	0.37104655E-1	ATP	-31.909777
ZMR	-10522.693	TBAR	10507.036	VZBDOT	-0.49957007E-3	VXP	0.16022472E-1
LMR	-7775.9733	LBARM	-3530.0776	PDOT	0.41559030E-3	VYP	0.0
MMR	10141.903	MBARM	-5524.0327	DDOT	-0.93072053E-5	VZP	0.16008990E-2
NMR	39243.000	MBAR	40074.256	DDOT	-0.24697055E-4	PSIR.	0.0
XMF	-0.00062249E-5	YT	3.5121724	XTR	0.0	PSIDMG	-150.0
YMF	0.0	YT	-0.07453067E-6	YTR	1266.6630	ATP	4.0
ZMF	0.64712310E-5	ZT	4.0799329	ZTR	-441.02055	MADD	0.0
LMF	0.0	LT	-0.10716665E-5	LTR	7779.0075	XADD	0.0
MMF	-0.15602240E-3	MT	101.02900	MTR	-14204.201	YADD	0.0
NMF	0.0	NT	0.13239620E-4	NTR	-39245.443	ZADD	0.0
XMT	3.5121724	XVT	-0.11050005E-6	ALFHTT	-0.3330001	MADD	0.0
YMT	0.0	YVT	-0.07453067E-6	ALFVTT	0.0	ZADD	0.0
ZMT	4.0799329	ZVT	0.09440706E-7	AARBIT	2.4501191	LAND	0.0

UTAS(576) 1-21-77 9-DEC-77 RUN 29.

WEIGHT	1900.0	FSCG	360.20000	V	1.0E-2	PSITR2	0.0
IA	6260.0	WLCG	245.09999	DELS	-5.0	VXSTR.	0.0
IY	41507.0	RMO	0.23700000E-2	VROUND	1117.0	VYSTP.	0.0
IZ	30224.0	TIME	0.20000000E-1	DEL3MR	0.0	VZSTR.	0.0
OMEGHR	25.64999	NBS3	4.0	DEL3MR	0.0	PLVT.	0.0
OMEGTR	116.32250	NBS3	5.0	THSTR	-10.0	HLVT	273.0
KFR	15.0	PASCNT	2623.0	THSTR	-10.0	F3VT	695.0
FSMT	700.40000	SMT	45.0	WLMT	234.0	QSTR.	0.0
LATSTK	0.13636255	A13	-0.02912040	SVT	32.30000	XA	50.85266
LNGSTK	7.7033550	B13	3.7938576	IS	33.320045	XB	22.494058
CULSTK	19.053621	THETAB	19.053621	TH5MR	9.7736216	XC	50.505136
PEDAL	29.436000	THETTR	37.5	TH5TR	24.0	XP	0.0
XAIN	5.0852265	XBIN	2.2490650	XCIN	5.0505135	XPIN	0.0
XBACTP	30.149089	XBACTI	3.0149089	RSTR.	0.0	PSTR	0.0
VXB	0.16763050E-1	THETAB	7.2479777	AAIF	4.7520417	QSTR	0.0
VXB	0.0	PHIB	-1.4729578	AAIF	-4.0797753	RSTR	0.0
VXB	0.21320109E-2	BETAMF	0.0	BBIF	-0.96107339	TSTR	0.0
P	0.0	GAMC	0.0	AAFL	-7.4019529	HSTR	0.0
O	0.0	OMGRAT	1.0	AAFL	0.50621463E-1	JSTR	0.0
R	0.0	PSIDOT	0.0	AAFL	0.34473497	WHSTR	0.0
ALF-F	-0.6004920	EKTZ	-0.12003097	EKMPX	0.79995393E-5	LHSTR	0.0
CHITPP	-4.0527791	EKTZ	0.39700355E-1	EKMPZ	0.11099360E-3	GHSTR	0.0
EXTR	0.0	EPSMT	0.40999999	SIGMT	0.0	VSTR	0.0
Q-F	0.35600529E-6	KQMT	0.47177979	KQMT	0.04052013	VSTR	0.0
MUXS	0.24006219E-4	CTSIG	0.90029790E-1	LTOT	-10.000700	ZSTR	0.0
MUXS	0.0	CHSIG	-0.69166299E-2	DTOT	24.669425	LSTR	0.0
MUXS	0.10100013E-5	COMSIG	0.04710447E-6	TTR	591.69505	MSTR	0.0
LAMBDR	-0.62000970E-1	NZ	0.99162015	HPMR	1700.8470	NSTR	0.0
DMSHMR	0.62000970E-1	VC	0.49767550E-4	KTRBLK	0.79599999	AXP	3.0400207
XMR	2400.5035	HBAR	-1.425.3594	VADOT	-0.73470692E-3	AYP	-0.40010424
YMR	-73.100026	TBAR	73.100026	VADOT	-0.31529170E-2	AZP	-31.004045
ZMR	-10723.402	LBARM	10025.259	VADOT	-0.20000433E-2	VXP	0.16763050E-1
LMR	-4640.3345	LBARM	-2242.3203	PUOT	-0.10400023E-2	VYP	0.0
MMR	6342.4365	MBARM	-10105.101	QUOT	0.13423674E-3	VZP	0.21320109E-2
NMR	37207.124	QBAR	37499.645	ADOT	0.52104560	RSTR.	0.0
DMSHMR	0.62000970E-1	XT	-0.90230509	XTR	0.0	PSIDMG	-150.0
XMF	0.0	YT	-0.47546759E-6	YTR	557.93309	RTR	2.0
YMF	0.0	ZT	-1.5712545	ZTR	-203.07143	MADD	0.0
ZMF	0.51560951E-5	LT	-0.10737643E-5	LTR	3426.0439	XADD	0.0
LMF	0.0	MT	-45.439933	MTR	-6291.0297	YADD	0.0
NMF	0.0	NT	0.13265545E-4	NTR	-17286.626	ZADD	0.0
XMT	-0.90230509	XVT	-0.13621705E-6	ALFMTT	16.001275	NADD	0.0
YMT	0.0	YVT	-0.47546759E-6	ALFVTT	0.0	LADD	0.0
ZMT	-1.5712546	ZVT	0.42290006E-7	AARBIT	4.1914470		

UTTAS (\$76) 1-21-77 9-DEC-77 RUN 30.

WEIGHT	19000.0	FSCG	360.20000	V	40.0	PSITR2	0.0
IX	6208.0	WLCC	245.00999	DELS	-5.0	VXSTR.	0.0
IY	41507.0	RHO	0.23700000E-2	V SOUND	1117.0	VYSTR.	0.0
IZ	30224.0	TIME	0.20000000E-1	DEL3MR	0.0	VZSTR.	0.0
OMEGMR	25.64999	NBS	4.0	TM3MR	-1A.0	PSSTR.	0.0
OMEGTR	110.32250	NSRS	5.0	TM3TR	-1A.0	WLVT	273.0
KPR	15.0	PASCNT	4650.0	WLMT	234.0	FSVT	495.0
F3MT	700.40000	SMT	45.0	JMT	32.30000	OSTR.	0.0
LATSTK	-1.0257474	AIS	-2.6124145	IS	20.808250	XA	30.509070
LMOSTK	0.0960503	RIS	4.0030614	TM7MR	-3.0	XB	10.542337
CULSTK	10.119405	THEYAR	10.119405	TM7STR	0.0394055	XC	47.746705
PEOAL	29.436000	THEYTR	37.5	XCIN	24.0	XP	0.0
XAIN	3.0509070	XBIN	1.4502337	RSTR.	0.0	XPIN	0.0
XBACTP	25.159423	XBACTI	2.5159423	AAOF	4.6140702	PSTR	0.0
VX0	67.392324	THEYAB	4.460155	AAIF	-2.6150384	RSTR	0.0
VT0	0.0	PHI0	-1.2494472	ABIF	-0.14973264	YSTR	0.0
VZ0	5.2639111	MEYAF	0.0	AAFL	-5.7752405	WTR	0.0
P	0.0	GAMC	0.0	ABIL	0.30263166	WTR	0.0
Q	0.0	OMGRAT	1.0	ABIL	0.13951417	WTR	0.0
R	0.0	PSIDOT	0.0	EKWPX	0.76184621	WTR	0.0
ALF.F	-13.629433	EXTX	1.1119591	EKWPZ	1.0243313	WTR	0.0
CHITPP	67.034324	EPSWT	0.44999999	SIGWT	0.0	WTR	0.0
EXTX	0.0	KOHT	0.87177979	KOVI	0.04052013	WTR	0.0
Q.F	9.5275253	CTSIG	0.91025017E-1	LTOT	-21.708201	WTR	0.0
MUXS	0.00185476E-1	CHSIG	-0.33446604E-2	DTOT	26.616161	WTR	0.0
MUVS	0.0	COMSIG	0.82285016E-6	TTR	915.57033	WTR	0.0
MUZS	0.25129026E-2	NZ	0.99604761	MPHR	1337.4117	WTR	0.0
LAMBMR	-0.34075999E-1	VC	0.10474920	KIRBLK	1.0	WTR	0.0
D-SHMR	0.37300002E-1	MBAR	-699.37122	VXBDOT	-0.32944707E-2	WTR	2.4865005
XMR	1694.4574	JBAR	439.06373	VYBDOT	-0.26279674E-3	WTR	0.60778162
YMR	-430.06373	TBAR	19033.360	VZBDOT	-0.16534635E-2	WTR	-32.065042
ZMR	-10969.196	LBARM	-1224.2050	PDOT	-0.15701076E-3	WTR	67.392324
LMR	-5333.1520	MBARM	-6239.3115	RDOT	0.14667156E-3	WTR	0.0
MHR	14000.581	QBARM	20677.444	RTOT	0.36663021E-1	WTR	5.2639111
NMR	27408.737	XT	-10.495076	XTR	0.0	WTR	0.0
XMF	-199.56271	YT	-7.5867556	YTR	0.0	WTR	-150.0
YMF	0.0	ZT	-2.0503125	ZTR	0.0	WTR	2.0
ZMF	261.20410	LT	-17.133423	LTR	-313.16730	WTR	0.0
LMP	0.0	MT	-05.217752	MTR	5204.7205	WTR	0.0
NMP	-5106.2943	NT	211.47940	NTR	-9702.9094	WTR	0.0
XMT	0.0	XVT	-1.9903154	ALFMTT	0.19954133	WTR	0.0
YMT	-0.4987609	YVT	-7.5867556	ALFVTT	0.0	WTR	0.0
ZMT	0.0	ZVT	1.0920066	AA0BIF	2.6193175	WTR	0.0
ZMT	-3.9431992					WTR	

RUN 31.

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UTTAS(576)

WEIGHT	1900.0	FSCG	360.20000	V	40.0	PSITR2	0.0
IX	6268.0	WLCG	245.89999	DELS	-5.0	VXSTR.	0.0
IY	41587.0	RHO	0.2370000E-2	V SOUND	1117.0	VYSTR.	0.0
IZ	38224.0	TIME	0.2000000E-1	DEL3MR	0.0	VZSTR.	0.0
OPEGR	25.60999	NBR3	4.0	THSTR	-18.0	PSTR.	0.0
OMEGR	11A.32250	NBR3	5.0	THSTR	-18.0	WLVT	273.0
KFR	15.0	PASCNT	3030.0	WMT	234.0	FVST	495.0
FSMT	700.00000	SHT	45.0	SVT	32.30000	OSTR.	0.0
LATSTK	-1.1511648	AIS	-1.0700291	IMT	14.765413	XA	42.005220
LNGSTK	9.9709200	01S	5.2944673	IS	-3.0	XB	14.738769
CULSTK	17.459265	THETA0	17.459265	TH75MR	7.3792651	XC	43.620407
PEDAL	29.43000	THETTR	37.5	TH75TR	24.0	XP	0.0
XAIN	4.2005219	XBIN	1.4730769	XCIN	4.3620407	YPIN	0.0
XOACTP	19.520119	XBACTI	1.9520119	RSTR.	0.0	PSTR	0.0
VXB	101.20000	THETAB	3.5070164	AAIF	4.0593772	OSTR	0.0
VYB	15.065700	PHIB	0.0	AAIF	-2.2976745	RSTR	0.0
VZB	6.2043170	RETAWF	7.3236017	BBIF	-0.55062462E-1	TITR	0.0
P	0.0	GAMC	0.0	AAFL	-4.0709755	HITR	0.0
Q	0.0	OMGRAT	1.0	AAFL	0.26150579	JITR	0.0
R	0.0	PSIDOT	0.0	ABIL	0.05494901E-1	MMITR	0.0
ALFAF	-5.6720245	EKTZ	1.3554900	EMFEX	0.00184741	LMITR	0.0
CHITPP	70.309765	EKTZ	1.8546667	EMFEX	1.0116502	OMITR	0.0
EXTH	0.0	EPST	0.52323601	SIGWT	1.1681266	YITR	0.0
QAF	16.627011	KQMT	0.07177979	KQVT	0.77223721	VITR	0.0
MUXB	0.14732010	CTSIG	0.90065102E-1	LTOT	-3.6119500	ZITR	0.0
MUYB	0.21091100E-1	CHSIG	-0.28275913E-2	OTOT	26.173346	LITR	0.0
MUZB	0.13060003E-2	CHMSIG	0.79407501E-6	TTR	947.90642	MITR	0.0
LAMHMR	-0.24251926E-1	NZ	0.99006783	HPMR	1134.3126	NITR	0.0
D-3MR	0.25557933E-1	VC	0.0	KTRBLK	1.0	AXP	2.00000064
XMR	1575.9005	WBAR	-591.25023	VXDOOT	0.13936430E-2	AYP	0.235177A0
YMR	-451.72947	JBAR	451.72947	VYDOOT	0.00582442E-3	AZP	-32.110970
ZMR	-14774.426	TBAR	10432.441	VZDOOT	0.62550137E-3	VXP	101.20000
LPR	-5970.6190	LBARH	-1594.1608	PDOOT	0.10340231E-2	VYP	15.065280
MPR	15933.000	WBARH	-5595.6919	QDOOT	0.16919067E-3	VZP	6.2043170
NMR	23450.071	QBAR	24322.492	ROOT	-0.93570869E-1	RSTR.	0.0
XAF	-349.50300	XT	-17.649534	XTR	0.0	PSIDMG	-150.0
YAF	-321.14253	YT	-117.37709	YTR	0.0	ATR	2.0
ZAF	99.034000	ZT	-51.491177	ZTR	-324.22792	MADD	0.0
LAF	509.06070	LT	-260.24586	LTR	5471.3462	XADD	0.0
MAF	-4391.1109	MT	-1409.3947	MTR	-10045.650	YADD	0.0
NAF	-2712.4412	NT	3275.4902	NTR	-27600.166	ZADD	0.0
XMT	-21.503008	XVT	3.0587732	ALFMTT	1.0550561	NADD	0.0
YMT	-1.4805043	YVT	-115.09698	ALFVTT	9.4287320	LADD	0.0
ZMT	-50.540035	ZVT	-0.94134230	AA8BIF	2.5983534		

UTAS(S76) 1-21-77 9-DEC-77 RUN 32.

WEIGHT	1900.0	FSCG	360.2000	V	DEL	80.0	PSITR2	0.0
IX	6200.0	WLCG	245.0999	DEL	DEL	-5.0	VXSTR.	0.0
IY	41507.0	RHO	0.23700000E-2	VSDUND	1117.0	0.0	VYSTR.	0.0
IZ	30224.0	TIME	0.20000000E-1	DEL	DEL	0.0	VZSTR.	0.0
OMEGMX	25.64999	NR98	4.0	TMSTR	-18.0	0.0	PSTR.	0.0
OMEGTH	110.32250	NR99	5.0	TMSTR	-18.0	273.0	WLVT	695.0
KFR	15.0	PASCM	2579.0	WLWT	234.0	0.0	FVST	0.0
FSMT	700.4000	SMY	45.0	SVT	32.30000	0.0	OSTR.	0.0
LATSTK	-1.1469044	AIS	-1.0769543	IMT	0.43004964	42.031047	YA	3.6730309
LNGSTK	13.110532	018	0.4375651	IS	-3.0	44.299144	XB	0.0
CULSTK	17.567863	THETA0	17.567863	TH7SHR	7.4070636	0.0	XC	0.0
PRDAL	29.436000	THETR	37.5	TH7STR	24.0	0.0	XP	0.0
XIN	4.2031047	XBIN	0.30730300	XCIN	4.4299147	0.0	XPIN	0.0
XOACTP	7.6243394	XOACTI	0.76243394	RSTR.	0.0	0.0	PSTR	0.0
VXB	130.64921	THETAB	5.1250476	AAOF	4.4550721	0.0	OSTR	0.0
VYB	15.445096	PHIB	0.0	AAIF	-4.77215A2	0.0	RSTR	0.0
VZB	12.076954	RETAWF	5.9065925	BBIF	-0.12200867	0.0	TITR	0.0
P	0.0	GAMC	0.0	AAPL	-4.8759070	0.0	HITR	0.0
Q	0.0	OMGRAT	1.0	AAIL	0.32041090	0.0	JITR	0.0
R	0.0	PSIDOT	0.0	BBIL	0.33471029	0.0	MMITR	0.0
ALFWF	-0.60300027	ERTX	1.3003208	EKWF	0.92117753	0.0	LMITR	0.0
CHITPP	01.629042	ERTZ	1.6069439	EKWFZ	1.0083709	0.0	OMITR	0.0
ERTH	0.0	EPST	0.50996591	SIGWT	1.0033774	0.0	XITR	0.0
OF	26.013094	KQHT	0.87177979	KQVT	0.00257252	0.0	VITR	0.0
MUX3	0.19429224	CT8IG	0.90826236E-1	LTOY	2.4757086	0.0	ZITR	0.0
MUX5	0.22443007E-1	CH8IG	-0.03126120E-2	OYOT	25.177955	0.0	LITR	0.0
MUX9	0.72030734E-2	CONSIG	0.79425024E-6	TTR	1054.9689	0.0	MITR	0.0
LAMBMR	-0.12353203E-1	NZ	0.90614387	WPMR	1124.5401	0.0	NITR	0.0
DMSMM	0.19637156E-1	VC	0.71525573E-5	KTPBLK	1.0	2.9354164	AXP	0.42255177
XMR	2311.9A13	MBAR	-1319.9691	VX8DOT	-0.65732426E-2	0.0	AYP	-32.040295
YMR	-405.30354	JBAR	405.30354	VY8DOT	-0.10056156E-1	0.0	AZP	134.64921
ZMR	-18095.212	TBAR	18091.795	VZ8DOT	-0.7005203AE-2	0.0	VXP	15.445096
LRR	-5934.6069	LBARM	-2202.3624	PDOT	0.59509946E-2	0.0	VYP	12.076956
MPR	5600.6145	MBARM	-11049.970	QDOT	-0.33937055E-3	0.0	RSTR.	0.0
NMR	23291.512	QBAR	24112.946	RODT	-0.16160933	0.0	PSIDMG	-150.0
XFF	-616.22910	XT	5.4142104	XTR	0.0	0.0	ATR	2.0
YFF	-409.76730	YT	-170.30329	YTR	991.42020	0.0	MADD	0.0
ZFF	-57.712014	ZT	299.57067	ZTR	-360.04014	0.0	XADD	0.0
LFF	632.45074	LT	-376.76512	LTR	6009.3365	0.0	YADD	0.0
MFF	-2995.3109	MT	0500.0413	MTR	-1100.270	0.0	ZADD	0.0
NFF	-3520.7089	NT	4752.5471	NTR	-30717.502	0.0	NADD	0.0
XMT	6.1732542	XVT	-0.75903575	ALFHTT	-4.1694056	0.0	LADD	0.0
YMT	-2.4112292	YVT	-167.09206	ALFVIT	6.8746774	0.0		
ZMT	299.51216	ZVT	0.46514361E-1	AA0BIF	4.7737301	0.0		

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HEIGHT	16450.0	PSCG	360.20000	V	40.0	PSIR2	0.0
IX	5130.0	WLCG	205.09999	DELS	-5.0	VXSTR.	0.0
IY	39615.0	PHO	0.17500000E-2	VOUND	1077.0	VYSTR.	0.0
IZ	37363.0	TIME	0.20000000E-1	DEL3MR	0.0	VZSTR.	0.0
ONEGR	25.64999	WSS	4.0	THSTR	-10.0	PSR.	0.0
ONEGR	110.32250	WSS	5.0	THSTR	-10.0	MLVT	273.0
W	15.0	PASCT	671.0	WMT	234.0	FSVT	495.0
PSMT	700.40000	SMT	45.0	SVT	32.30000	QSTR.	0.0
LATSTK	-0.94260293	AIS	-1.7401170	IMT	21.823440	XA	44.108731
LAGSTK	4.2111302	BIS	4.5151154	IS	-3.0	XB	35.119652
COLSTK	10.300533	THETA0	10.300533	TH5MR	0.2205332	YC	40.070333
PEDAL	12.436023	THETTR	21.021462	TH5TR	0.3214620	XP	47.125604
XAIN	4.410731	XOIN	3.5119652	KCIN	4.0070332	XPIN	2.5447207
XRACTP	39.414441	XOACTI	3.9414440	RSTR.	0.0	PSR.	0.0
VXB	101.32364	THETA0	2.2407646	AAOF	3.7105700	OSTR	0.0
VYB	13.342627	PHI0	0.0	AAIF	-1.1332231	RSTR	0.0
VZB	3.9646071	BETAWF	6.3795790	BBIF	0.63350257E-1	TITR	0.0
P	0.0	GAMC	0.0	AAFL	-4.1586307	HITR	0.0
O	0.0	OMGRAT	1.0	AAIL	0.19210300	JITR	0.0
R	0.0	PSIOOT	0.0	ABIL	-0.74642221E-2	MHITR	0.0
ALF=F	-7.600051	EXTX	1.2795091	EKMFZ	0.6924564	LHITR	0.0
CHITPP	77.204151	EKTZ	1.9221221	EKFZ	1.0127950	OHITR	0.0
EXTR	0.0	EPST	0.5137950	SIGMT	1.0510670	XITR	0.0
Q=F	12.630364	KGHT	0.47177979	KOVT	0.79393649	VITR	0.0
MUXS	0.14732047	CTSIG	0.99844720E-1	LTOT	-6.9481085	ZITR	0.0
MUYS	0.19380013E-1	CHSIG	-0.11149857E-2	OTOT	26.109206	LITR	0.0
MUZS	-0.19526075E-2	COMSIG	0.09972114E-6	TTR	705.08276	MITR	0.0
LAMBMR	-0.30402036E-1	NZ	0.99935601	MPHR	970.83550	NITR	0.0
DASHMR	0.20450229E-1	VC	0.0	KTRBLK	1.0	AXP	1.2630751
XMR	975.39353	WBAR	-171.57349	VXDOOT	0.50835026E-2	AYP	0.55202300E-2
YMR	-360.03724	JBAR	360.03724	VYDOOT	2.10096050E-2	AZP	-32.152006
ZMR	-15332.032	TBAR	15364.260	VZDOOT	-0.35065520E-2	VXP	101.32364
LMR	-4300.4755	LBARM	-970.26990	PDOT	0.22046033E-2	VYP	13.342627
MMR	16862.931	MBARM	-2765.3301	QDOT	-0.19230434E-3	VZP	3.9646071
NMR	20121.870	OBAR	20017.137	RODT	-0.12201600E-3	RSTR.	0.0
XMF	-294.62006	XT	-66.054969	YTR	0.0	PSIDMG	-150.0
YMF	-212.92143	YT	-00.360834	ZTR	662.61033	OTR	4.0
ZMF	120.04113	ZT	-101.96701	MTR	-201.17090	MADD	0.0
LMF	410.62241	LT	-175.92013	NTR	4069.7751	XADD	0.0
MMF	-4109.9575	MT	-5226.3519	ALPHTT	-7472.2785	YADD	0.0
NMF	-1044.2607	NT	2202.9373	ALPHTT	-20529.076	ZADD	0.0
XMT	-67.913007	XVT	1.0546300	ALPHTT	4.0679609	NAOU	0.0
YMT	-1.7112039	YVT	-74.649629	ALPHTT	4.1235055	LADD	0.0
ZMT	-101.60504	ZVT	-0.32196012	AA00IF	1.1349925		

WEIGHT	16459.0	FSCG	362.20000	V	60.0	PSIR2	P.0
IX	5130.0	WLCG	245.09999	NELS	-5.0	VXSTR.	P.0
IY	3915.0	RMD	0.17500000E-2	VSDUND	1077.2	VYSTR.	P.0
IZ	37363.0	TIME	0.20000000E-1	NEL3MR	2.0	VZSTR.	P.0
OMEGMR	25.649999	N888	5.0	THSTR	-10.0	PSIR.	P.0
OMEGTR	110.32250	N888	5.0	THSTR	-10.0	WLV	273.0
KFR	15.0	PASCNT	2070.0	WLMT	234.0	FST	695.0
FST	700.40000	SM	45.0	SVT	32.300000	QSTR.	P.0
LATSTK	-0.94579690	A19	-1.7511792	INT	21.013925	YA	44.000769
LONGTK	0.4949164	M19	4.5132079	IS	-3.0	XB	19.002627
COLSTK	10.299245	THETA0	10.299245	TH75MR	0.2192455	XC	40.070205
PEOAL	27.790575	THETA1	37.173670	TH75TR	23.673670	XP	4.5014996
XATN	4.4000768	XBIN	1.992627	XCIN	4.0070205	XPIN	0.24631457
FEACTP	24.200559	XBACTI	2.420559	ASTR.	0.0	PSIR	P.0
VXB	101.32200	THETA0	2.2409515	AAPF	3.7141217	QSTR	P.0
VXB	13.210032	PHIB	0.0	AAPF	-1.1347947	PSIR	P.0
VXB	3.0791501	DETAHF	6.3146594	AAIF	0.64744271E-1	TSTR	P.0
P	0.0	GAMC	0.0	AAIF	-4.1567302	HTR	P.0
Q	0.0	OMGRAT	1.0	AAIF	0.1920015	JTR	P.0
ALP-F	-7.63336293	PSIDOT	P.0	MBIL	-2.74801997E-2	MHTR	P.0
CHITPP	77.209750	EKTZ	1.9219297	EKMFZ	1.0127902	OHTR	P.0
EKT	0.0	EPSW	0.51314659	SIGMT	1.0432657	XTR	P.0
QF	12.627252	KQMT	0.47117979	KQMT	0.79536171	YTR	P.0
MUXS	0.14732047	CTSIG	0.99027900E-1	LTOT	-6.9504752	ZTR	P.0
MUY5	0.19195341E-1	CHSIG	-0.11192057E-2	CTOT	26.149549	LTR	P.0
MUZ5	-0.19315520E-2	COMSIG	0.9901062E-6	TTR	703.51300	HTR	P.0
LAMBMR	-0.30303509E-1	NZ	0.99915147	MPMR	970.40505	NTR	P.0
DMBMR	0.20852036E-1	VC	2.17001393E-5	KTRBLK	1.0	ASP	1.2637517
XMR	975.92710	MBAR	-172.22286	VXDOT	0.16769313E-2	AVP	0.50936000E-2
YMR	-300.34770	JBAR	360.34770	VYDOT	0.46680959E-2	AVP	-32.145743
ZMR	-1330.225	TBAR	15361.404	VZDOT	0.20332270E-2	AVP	101.32200
LMB	-0.992.0345	LBARM	-974.07132	PDOT	0.18151235E-2	AVP	13.210232
MRR	10052.569	MBARM	-2769.2469	QDOT	0.00360959E-4	AVP	3.0791501
NMR	20113.295	OBAR	20007.006	RDOT	0.05291750E-3	PSIR.	P.0
XMF	-294.49805	XT	-66.924606	XTR	2.2	PSIDMG	-150.0
YMF	127.99500	YT	-79.774521	YTR	661.13513	MTR	2.0
ZMF	414.13660	ZT	-101.06710	ZTR	-240.61397	WADD	P.0
LMP	-4100.5065	LT	-174.67263	LTR	4060.7144	WADD	P.0
MMP	-1020.0261	MT	-5225.2204	MTR	-7455.6426	WADD	P.0
NMP	-67.062962	NF	2226.5014	NTR	-2044.178	ZADD	P.0
XMT	-1.6904175	XVT	0.93035696	ALFMTT	4.0669606	WADD	P.0
YMT	-1.6904175	YVT	-70.908103	ALFVTT	0.0264202	LAND	P.0
ZMT	-101.50116	ZVT	-0.20593661	AABIF	1.1366401	LAND	P.0



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UT 243 (976)

[illegible]

UTTAS(976) 1-21-77 9-DEC-77 RUN 36.

WEIGHT	16450.0	FSCG	360.20000	V	100.0	PSITP2	0.2
IX	5130.0	MLCG	245.89999	DELS	-5.0	VXSTR.	0.2
IY	39015.0	RHO	0.17500000E-2	V SOUND	1077.0	VXSTR.	0.2
IZ	37363.0	TIME	0.20000000E-1	DEL3MR	0.0	VZSTR.	0.2
OPEGMR	25.609999	MBS3	4.0	TMSTR	-10.0	PSSTR.	0.2
OPEGTR	110.32250	NBS3	5.0	TMSTR	-10.0	HLVT	273.0
KPR	15.0	PASCNT	1301.0	WLMT	234.0	F3VT	695.0
F3MT	700.00000	SWT	45.0	WMT	32.300000	OSTH.	0.2
LATSTK	-0.00013416	ALS	-1.6950009	IMT	1.7115743	XA	40.074161
LNGSTK	12.159046	B13	9.3162000	IS	-3.0	XB	7.0351720
CULSTK	10.973929	THETAB	10.973929	TH75MR	0.0939290	XC	53.007062
PEDAL	24.411169	THETTR	34.603003	TH75TR	21.103005	XP	13.930001
XAIN	4.0074161	XBIN	0.70351720	XCIN	5.3007062	XPIN	0.75220251
XGACTP	0.0531192	XOACTI	0.00531192	RSTR.	0.0	PSTR	0.2
VIB	160.60620	THETAB	3.3011251	AAPF	3.7014791	OSTR	0.2
V70	11.332305	PHI0	0.0	AAIF	-4.0057342	PSR	0.2
VZ0	9.0672007	BETAF	3.5995326	ABIF	0.15721923	TSTR	0.2
P	0.0	GAMC	0.0	AA0L	-4.3326761	HTR	0.2
Q	0.0	OMGRAT	1.0	AA1L	0.30046201	JSTR	0.2
R	0.0	PSIDOT	0.0	BB1L	0.21517150	MMTR	0.2
ALFAP	-0.73096071	EXTX	1.3153372	EKWF	0.92016403	LHTR	0.2
CHITPP	02.106465	EXTZ	1.6953143	EKWFZ	1.0070335	GMTR	0.2
ERTH	0.0	EP3MT	0.40599532	SIGMT	0.63351777	XSTR	0.2
OPF	20.472930	KOMT	0.07177979	KQVT	0.03130643	VSTR	0.2
MUX3	0.20533356	CTSIG	0.10122313	LTOT	1.5531704	ZSTR	0.2
MUY3	0.16066954E-1	CH9IG	-0.51501514E-2	DTOT	24.299906	LSTR	0.2
MUZ3	0.16335345E-2	COMSIG	0.89650039E-6	TTR	765.63526	MSTR	0.2
LAMHMR	-0.14091051E-1	NZ	0.99063206	MPMR	1010.1277	NSTR	0.0
DMSMR	0.17725005E-1	VC	0.0	KTRBLK	1.0	AXP	1.0942200
XMR	1606.5243	MBAR	-702.50293	VXRDOT	-0.66367910E-2	AYP	2.11113094E-2
YMR	-319.95071	JBAR	319.95071	VXRDOT	0.9590201E-3	AZP	-32.134423
ZMR	-15512.130	TBAR	15574.169	VZROOT	-0.13033067E-1	VXP	160.69620
LMR	-4553.7545	LBARM	-1404.3110	POOT	-0.34269634E-3	VYP	11.332305
MMR	6131.2007	MBARM	-9973.7326	QOOT	-0.17100009E-2	VZP	9.9672007
NMR	21017.710	OBAR	21659.050	ROOT	-0.31547400E-3	OSTR.	0.0
XAP	-676.06624	XT	-10.500363	XTR	0.0	PSIDMG	-150.0
YAP	-260.46657	YT	-130.63103	YTR	719.51529	STR	0.2
ZAP	-35.079472	ZT	192.07072	ZTR	-201.00265	MADD	0.2
LAP	424.72047	LT	-291.29146	LTR	4419.2073	XADD	0.2
MAP	-3500.5223	MT	5082.9007	MTR	-0.113.9976	YADD	0.2
NAP	-2300.0764	NT	3645.1431	NTR	-22292.901	ZADD	0.2
XMT	-2.7207517	XVT	-7.0636114	ALFMTT	-2.5455529	NADD	0.2
YMT	-1.1402391	YVT	-129.40759	ALFVTT	3.0530306	LADD	0.2
ZMT	192.20334	ZVT	0.50530124	AARBF	0.0807579		

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WEIGHT	16459.0	FSCG	369.20000	V	DEL3	60.0	PSITR2	0.0
IX	5130.0	MLCG	245.09999	DEL3	VSOUNO	-5.0	VXSTR.	0.0
IY	39015.0	RMO	0.17500000E-2	VSOUNO	DEL3MR	1077.0	VYSTR.	0.0
IZ	37363.0	TIME	0.20000000E-1	DEL3MR	0.0	0.0	VZSTR.	0.0
ONEGMR	29.700000	NBS3	4.0	TMSTTR	-1A.0	0.0	PSSTR.	0.0
ONEGTR	137.00499	NBS3	5.0	TMSTTR	-1A.0	273.0	MLVT	0.0
KFR	15.0	PARCNT	965.0	MLMT	234.0	695.0	FSVT	0.0
PSMT	700.40000	SMT	45.0	SVT	32.30000	0.0	OSTR.	0.0
LATSTK	-0.01077867	AIS	-1.3402002	IMT	19.613152	44.932633	XA	0.0
LAGSTK	7.9360415	BIS	3.5765435	IS	-3.0	21.957450	XB	0.0
COLSTK	16.006011	THETAB	16.00011	TH75MR	6.0060114	35.002572	XC	0.0
PEDAL	26.045622	THETTR	33.573796	TH75TR	20.073796	7.1011303	YP	0.0
XAIN	4.0932633	XBIN	2.1957449	XCIN	3.5042572	0.30777095	XPIN	0.0
XBACTP	26.310005	XBACTI	2.6310005	RSTR.	0.0	0.0	PSSTR	0.0
VIB	101.30966	THETAB	2.3910042	AA0F	2.6190938	0.0	OSTR	0.0
VIB	16.470456	PHID	0.0	AA0F	-1.3754625	0.0	RSTR	0.0
VIB	4.2309563	MEYAF	7.0676330	AA0F	-0.10690767E-1	0.0	TSTR	0.0
P	0.0	GAMC	0.0	AA0L	-3.2337521	0.0	HTTR	0.0
P	0.0	OMGRAT	1.0	AA0L	0.13150246	0.0	JSTR	0.0
P	0.0	PHIDOT	0.0	BB0L	0.61676079E-1	0.0	MMTR	0.0
ALPAP	-7.5102190	EXTX	1.2073449	EKWF	0.06025303	0.0	LMTR	0.0
CHITPP	77.113906	EXTZ	1.9163014	EKWFZ	1.0120060	0.0	OMTR	0.0
EXTR	0.0	EPSMT	0.92067633	8IGWT	1.2355064	0.0	XSTR	0.0
QAP	12.695079	KQMT	0.07117979	KQVT	0.75945056	0.0	VSTR	0.0
MUXS	0.12723128	CTSIG	0.74704607E-1	LTOT	-6.4420239	0.0	ZSTR	0.0
MUY3	0.20679470E-1	CHSIG	-0.02500307E-3	DTOT	27.043605	0.0	LSTR	0.0
MUZ3	-0.13517562E-2	COMSIG	0.47330013E-6	TTR	740.10517	0.0	HTTR	0.0
LAMBMR	-0.25904665E-1	NZ	0.99009402	MPMR	1102.0533	0.0	NSTR	0.0
OSMMR	0.20552909E-1	VC	0.35702706E-5	KTRBLK	1.0	1.3210477	ASP	0.0
XMR	974.73700	MBAR	-170.37095	VX0DOT	-0.20549174E-1	-0.23931713E-2	AVP	0.0
YMR	-337.66920	JBAR	337.66920	VY0DOT	-0.21641330E-3	-32.137753	AZP	0.0
ZMR	-15301.457	TBAR	15412.493	VZ0DOT	0.60940700E-2	101.30966	VXP	0.0
LMR	-0.000.9009	LBARM	-1401.2043	PDOT	-0.10674055E-3	16.478454	VVP	0.0
MMR	15044.105	MBARM	-4457.9277	QDOT	0.30062500E-3	4.2309563	VZP	0.0
MMR	21000.251	OBAR	21067.454	ROOT	0.73797150E-3	0.0	PSSTR.	0.0
XMP	-206.60329	XT	-37.500457	XTR	0.0	-150.0	PSIDMG	0.0
YMP	-204.67329	YT	-93.205707	YTR	495.52300	2.0	STR	0.0
ZMP	121.50030	ZT	-107.00003	ZTR	-253.15019	0.0	WADD	0.0
LMP	519.45500	LT	-205.00000	LTP	4271.9263	0.0	XADD	0.0
MPF	-0.004.0329	MT	-3103.6107	MTR	-7043.4367	0.0	YADD	0.0
MPF	-2226.0747	NT	2603.4001	NTR	-21549.623	0.0	ZADD	0.0
XMT	-41.763245	XVT	4.2227078	ALFMTT	2.0509564	0.0	LADD	0.0
YMT	-1.7260003	YVT	-91.559779	ALFVTT	10.510570	0.0		0.0
ZMT	-106.42613	ZVT	-1.2710002	AA0BIF	1.3755005	0.0		0.0

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WEIGHT	16050.0	FSCG	360.20000.	V	DEL3	82.0	PSITR2	0.0
IX	5130.0	WLCG	245.09999	DEL3	-5.0	-5.0	PSITR2	0.0
IY	39015.0	RMD	0.1750000E-2	V SOUND	1077.0	1077.0	VXSTR.	0.0
IZ	37363.0	TIME	0.2000000E-1	DEL3MR	0.0	0.0	VYSTR.	0.0
OMEGMA	237.0000	WSS	4.0	THSTR	-10.0	-10.0	VZSTR.	0.0
OMEGTA	137.0000	NSS	5.0	THSTR	-10.0	-10.0	WVT	273.0
KFR	13.0	PASCNT	1133.0	WMT	230.0	230.0	FSVT	695.0
FSMT	700.4000	SHY	45.0	SVT	32.30000	32.30000	OSTR.	0.0
LATSTK	-0.60001981	A18	-1.2250309	IMT	7.630217	7.630217	XA	45.969251
LMBSTK	9.2193217	A19	5.1950422	IS	-3.0	-3.0	XB	17.422091
CULSTK	16.112106	THFT40	16.112106	TH7MR	6.0321861	6.0321861	XC	35.201163
PDAL	25.669127	THFT40	32.427750	TH7STR	10.927750	10.927750	XP	10.442649
XAIN	4.5969250	XBIN	1.7422091	XCIN	3.5201163	3.5201163	XPIN	0.56300840
TOACTP	20.415165	XBACTI	2.0415165	RSTR.	2.0	2.0	PSTR	0.0
VAB	135.04795	THFT40	2.605066	AARF	2.5900061	2.5900061	OSTR	0.0
VAB	15.243051	PHIB	0.0	AAIF	-2.5560002	-2.5560002	PSTR	0.0
VAB	6.242700	RETAHF	5.0433117	00IF	7.36690170E-1	7.36690170E-1	YSTR	0.0
P	0.0	GAMC	0.0	AAOL	-3.3400274	-3.3400274	WSTR	0.0
Q	0.0	PMGRAT	1.0	AAIL	0.16501324	0.16501324	JSTR	0.0
ALP.F	-3.4440853	PSIDOT	0.0	00IL	0.14343030	0.14343030	WSTR	0.0
CHITPP	00.732520	ERTX	1.3502125	EKWF	0.9095206	0.9095206	WSTR	0.0
ERTW	0.0	EPST	0.50043311	EKWFZ	1.0092674	1.0092674	CHITR	0.0
QAF	19.633692	KQMT	0.07177979	SIGWT	0.96457045	0.96457045	YSTR	0.0
MUXS	0.16964162	CT9IG	0.75207418E-1	KQVT	0.06000295	0.06000295	VSTR	0.0
MUY5	0.19129613E-1	CH9IG	-0.10093661E-2	LTCI	-0.96440010	-0.96440010	ZSTR	0.0
MUZ5	-0.10065957E-2	CH9IG	0.40090844E-6	DTOT	25.005904	25.005904	LSTR	0.0
LAMDMR	-0.19949175E-1	NZ	0.99874922	TTR	700.00236	700.00236	WSTR	0.0
D-5MR	0.1002370E-1	VC	0.35762706E-5	HPMR	1214.5954	1214.5954	NSTR	0.0
XMR	1104.7607	WBAR	-373.24927	KTRBLR	1.0	1.0	AXP	1.4881076
YMR	-309.93071	JBAR	309.93071	VX00T	0.25930495E-2	0.25930495E-2	AYP	-0.10610955E-2
ZMR	-15073.993	TBAR	15515.990	VY00T	-0.32812099E-2	-0.32812099E-2	AZP	-32.133431
LMR	-4002.1097	LBARW	-1690.0475	VZ00T	0.40000510E-2	0.40000510E-2	VXP	135.004795
MMR	10050.039	WBARW	-0530.0049	POCT	-2.23200919E-3	-2.23200919E-3	VYP	15.243451
NMR	2155.201	OBAR	22002.511	DOOT	0.17250073E-3	0.17250073E-3	VZP	6.242700
XMP	-402.31027	XT	0.06910079	POOT	0.0	0.0	PSTR.	0.0
YMP	-301.23971	YT	-123.409590	XTR	0.0	0.0	PSIDMG	-150.0
ZMP	46.016452	ZT	75.700630	YTR	733.47557	733.47557	STR	0.0
LMP	513.45642	LT	-275.05600	ZTR	-266.96379	-266.96379	MADD	0.0
MMP	-3029.1305	MT	2109.3192	WTR	-0271.4279	-0271.4279	XADD	0.0
NMP	-2014.2771	NT	3457.2430	NTR	-22725.517	-22725.517	YADD	0.0
XMT	1.6066110	XVT	-0.73700221	ALPMTT	-1.3541774	-1.3541774	ZADD	0.0
YMT	-1.2130570	YVT	-102.000292	ALPVT	6.7675294	6.7675294	MADD	0.0
ZMT	75.503900	ZVT	0.11664069	AABIF	2.5569314	2.5569314	LADD	0.0

RUN 39.

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UTIAS(S76)

WEIGHT	1645R.0	FSCG	36R.20000	V	100.0	PSITR2	0.0
IX	5130.0	WLCG	245.49999	DELS	-5.0	VXSTR.	0.0
IY	39815.0	PHC	0.17300000E-2	V SOUND	1077.0	VYSTR.	0.0
IZ	37363.0	TIME	0.20000000E-1	DEL3MR	0.0	VZSTR.	0.0
OMEGMA	29.70200	NBS	4.0	TWSTMR	-1A.0	PSSTR.	0.0
OMEGTR	137.00499	NBS	5.0	TWSTTR	-1A.0	WLVT	273.0
KFR	15.0	PASANT	1133.0	WLMT	234.0	FST	695.0
PSMT	700.40000	SHY	45.0	SVT	32.30000	QSTR.	0.0
LAT8TK	-0.56600974	AIS	-1.1933575	IMT	-0.69407494	XA	46.461939
LANGSTK	11.022033	BIS	7.5755529	IS	-3.0	XB	9.0005002
COLSTK	16.569970	THETA0	16.569970	TH75MR	6.4099789	XC	30.062369
PEDAL	25.153759	THETR	33.461733	TH75TR	19.961733	XP	9.0991370
XAIN	4.6461930	XBIN	0.90005002	XCIN	3.062369	XPIN	0.49134062
XBACTP	10.772750	XBACTI	1.0772750	PSSTR.	0.0	PSR	0.0
VIB	160.71460	THETAB	3.2627225	AAQF	2.6115622	QSTR	0.0
VIB	15.392407	PHIB	0.0	AAIF	-4.3927164	RSTR	0.0
VZB	9.6104460	RETAHF	4.0608741	BBIF	0.32969094E-1	TITR	0.0
P	0.0	GAMC	0.0	AAOL	-3.0130951	MITR	0.0
Q	0.0	CMGRAT	1.0	AAIL	0.20262405	JTR	0.0
R	0.0	PSIDOT	0.0	BBIL	0.20571359	MHTR	0.0
ALFAP	-0.07610721	EXTX	1.3594462	EKWF	0.92220996	LHTR	0.0
CHITPP	01.714614	FRTZ	1.6972015	EKWF2	1.0082853	GHTR	0.0
EXTN	0.0	EPST	0.49004074	RIGHT	0.06000006	XTR	0.0
OPF	20.575914	KQMT	0.07177979	KQVT	0.82516968	YTR	0.0
MUXS	0.21205176	CTSIG	0.76163073E-1	LTOT	1.9034210	ZTR	0.0
MUYB	0.19316040E-1	CHSIG	-0.36147522E-2	DTOT	24.597374	LTR	0.0
MUZB	0.97255701E-3	CHSIG	0.47100295E-6	YTR	0.90.22405	MITR	0.0
LAMBMR	-0.14434774E-1	NZ	0.99832785	WPMR	1373.5913	NTR	0.0
DASHMR	0.15407334E-1	VC	0.14305114E-4	KTRBLK	1.0	AP	1.0444890
XMR	1567.0244	WBAR	-745.75743	VXDOOT	0.10001947E-1	AVP	0.20342417E-1
YMR	-300.09643	JBAR	309.09643	VYDOOT	0.07911120E-2	AZP	-32.121002
ZMR	-15651.540	TBAR	15713.324	VZDOOT	-0.53269003E-3	VAP	160.71460
LMR	-5362.3461	LBARM	-2163.1667	POOT	0.60930623E-2	VVP	15.392407
MMR	1961.6491	MBARM	-14614.737	DOOT	-0.1345357E-2	VZP	9.6104460
NMR	24772.351	QBARM	25430.677	ROOT	-0.13245207E-3	RSTR.	0.0
XAP	-673.72050	XT	1.9772600	XTR	0.0	PSIDMG	-150.0
YAP	-365.06102	YT	-165.06613	YTR	0.44.11727	STR	2.0
ZAP	-44.067069	ZT	390.99174	ZTR	-307.23415	MADD	0.0
LAP	574.96900	LT	-345.65500	LTR	5184.5964	XADD	0.0
MAP	-3596.5530	MT	11100.477	NTR	-9519.1301	YADD	0.0
NAP	-3244.7002	NT	4606.0950	ALPHTT	-26153.566	ZADD	0.0
XMT	6.3009205	XVT	-4.3236685	ALFVTT	-5.1247551	MADD	0.0
YMT	-2.2041971	YVT	-142.00193	AA0BIF	5.2703620	LAND	0.0
ZMT	399.65677	ZVT	0.33497190		4.3920400		

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WEIGHT	16450.0	PSCG	300.20000	V	120.0	PSITR2	P.0
IX	5130.0	WLCG	207.4999	DELS	-5.0	VXSTR.	0.0
IY	39015.0	RHO	0.17500000E-2	V SOUND	1077.0	VYSTR.	0.0
IZ	37363.0	TIME	0.20000000E-1	DEL3MR	0.0	VZSTR.	0.0
OMEGMR	29.70000	NBS	4.0	THSTR	-18.0	PSTR.	0.0
OMEGTR	137.00000	NBS	5.0	THSTR	-18.0	PLVT	273.0
KPR	15.0	PASCNT	1091.0	WLHT	234.0	FSVT	695.0
FSMT	700.40000	SHT	45.0	9VT	32.30000	QSTR.	0.0
LATSTK	-0.50259338	AIS	-1.3016991	INT	-2.2309183	XA	46.350791
LANGSTK	13.365371	PIS	9.0120624	IS	-3.0	XB	2.7725393
COLSTK	17.461608	THETAB	17.461608	TH5MR	7.3016080	YC	43.635056
PEDAL	20.251935	THETTR	36.629066	TH5TR	23.129066	XP	3.2025022
XAIN	0.6350790	XBIN	0.27725393	XCIN	4.3635056	XPIN	0.17725051
XGACTP	2.6939957	XGACTI	0.26939956	RSTR.	0.0	PSTR	0.0
VX0	202.64508	THETAB	2.2494494	AAIF	2.6201242	OSTR	0.0
VY0	16.702701	PHIB	0.0	AAIF	-5.0593560	RSTR	0.0
VZ0	7.9600765	BETAMF	4.5024199	BBIF	-0.54501303E-1	TSTR	0.0
P	0.0	GAMC	0.0	AAFL	-4.6302554	HSTR	0.0
Q	0.0	OMGRAT	1.0	ABIL	0.22629349	JSTR	0.0
R	0.0	PSIDOT	0.0	ABIL	0.37982537	MMSTR	0.0
ALFAP	-0.65755128	PATX	1.4167120	EKMF	0.91669353	LMSTR	0.0
CHITPP	01.204119	EKTZ	1.6066035	EKMFZ	1.000715A	OMSTR	0.0
ETH	0.0	EPST	0.49502420	SIGT	0.79242593	XSTR	0.0
QF	39.610794	KQMT	0.07177979	KQVT	0.02703121	VSTR	0.0
MUXS	0.25446263	CTSIG	0.76690534E-1	LTOT	2.0119065	ZSTR	0.0
MUYS	0.20960904E-1	CHSIG	-0.35079733E-2	OTOT	24.400403	LSTR	0.0
MUZS	-0.33341060E-2	COMSIG	0.47334975E-6	TTR	1099.7205	MSTR	0.0
LAMBMR	-0.16270922E-1	NZ	0.99929199	MPMR	1665.6504	NSTR	0.0
DASHMR	0.12936016E-1	VC	0.35762706E-5	KTRBLK	1.0	AXP	1.2792494
XMR	1547.1941	WBAR	-740.23269	VXBOOT	0.15560934E-1	AYP	0.37060974E-1
YMR	-336.03437	JBAR	336.03437	VYBOOT	0.21016753E-1	AZP	-32.140737
ZMR	-15760.327	TBAR	15021.979	VZBOOT	-0.17022975E-2	VXP	202.64568
LMR	-6540.0064	LBARM	-2009.4009	POOT	0.11200055E-1	VYP	16.702701
MMR	-27.869388	MBARM	-16784.410	QOOT	-0.09411943E-3	VZP	7.9600765
NMR	30092.179	OBAR	30049.082	ROOT	0.19095656E-2	RSTR.	0.0
XMF	-936.71244	XT	-9.1132620	XTR	0.0	PSIDMG	-150.0
YMF	-467.25206	YT	-219.17370	YTR	1033.4761	RTR	2.0
ZMF	-6A.920909	ZT	57A.40395	ZTR	-376.15526	MADD	0.0
LMP	731.43766	LT	-405.56995	LTR	6347.6452	XADD	0.0
MPF	-4769.7201	MT	16416.542	MTR	-11054.543	YADD	0.0
NMF	-4142.5914	NT	6116.2497	NTR	-32020.534	ZADD	0.0
XMT	-1.1046532	XVT	-7.9206096	ALFMTT	-5.0007371	NADD	0.0
YMT	-2.0915421	YVT	-216.20223	ALFVTT	4.7305911	LADD	0.0
ZMT	970.02096	ZVT	0.46299716	AARBF	5.0596512		

NO TRIM 9-DEC-77 RUN 41.

WEIGHT	16450.0	FSCG	360.20000	V	140.0	PSITR2	0.0
IX	5130.0	WLCG	245.9999	DELS	-5.0	VXSTR.	0.0
IY	39815.0	RHO	0.17500000E-2	V SOUND	1077.0	VYSTR.	0.0
IZ	37363.0	TIME	0.20000000E-1	DEL3MR	0.0	VZSTR.	0.0
OMEGR	29.70000	NS88	4.0	TWSTTR	-10.0	WLVT	273.0
OMEGR	137.00499	NS89	5.0	WLMT	234.0	FSTV	695.0
KFR	15.0	PASCNT	5000.0	SVT	32.300000	OSTR.	0.0
F3H1	700.40000	SMT	45.0	IMT	-2.9279675	XA	46.215136
LATSTK	-0.00557024	AIS	-1.4606410	IS	-3.0	XB	0.0
LGSTK	14.14999	BIS	9.0715340	TH75MR	8.7792502	XC	52.370315
COLSTK	10.059250	THETAB	10.059250	TH75TR	24.0	XP	0.0
PEDAL	29.436000	THETTR	37.5	XCIN	5.2370314	XPIN	0.0
XAIN	4.6215136	XBIN	0.0	RSTR.	0.0	OSTR	0.0
XBACTP	-2.2092616	XBACTI	-0.22092616	AA0F	2.7050066	RSTR	0.0
VXB	236.50174	THETAB	0.20934432	AAIF	-4.0040219	TSTR	0.0
VYB	15.219806	PHIB	0.0	ABIF	-0.95242330E-2	MITR	0.0
VZB	1.1946927	BETAMF	3.5520006	ABIL	-5.0052750	JSTR	0.0
P	0.0	GAMC	0.0	AA0L	0.26072603	MITR	0.0
Q	0.0	OMGRAT	1.0	ABIL	0.43714036	PHITR	0.0
R	0.0	PSIDOT	0.0	BBIL	0.90272122	LMITR	0.0
ALFHF	-1.0636709	EKTX	1.4003427	EKWF	1.0097906	GHITR	0.0
CHIIPP	00.209326	EKTZ	1.7213207	EKWFZ	0.62529291	VITR	0.0
EKTR	0.0	EPSMT	0.40552000	SIGAT	0.83161144	ZITR	0.0
Q-F	52.609406	KQHT	0.07177979	KQVT	24.290560	MITR	0.0
MUX3	0.29654438	CT8IG	0.70912072E-1	LTOT	1204.0711	NITR	0.0
MUY8	0.19095045E-1	CH8IG	-0.23192220E-2	DTOT	2093.1220	AXP	-0.33270907
MUZ8	-0.18040696E-1	COM8IG	0.48064454E-6	TTR	1.0	AYP	-0.29573595
LAMBMR	-0.25449039E-1	NZ	1.00000000	KTRBLK	0.24624279E-1	AZP	-31.583815
DMSHMR	0.11408342E-1	VC	0.99406967E-6	VXADOT	-0.51759509E-2	VXP	236.50176
XMR	1320.0127	HBAR	-470.47751	VZADOT	0.15742325E-1	VYP	15.216543
YMR	-301.34571	JBAR	301.30571	PDOT	0.23610252	VZP	1.1947452
ZMR	-16231.051	TBAR	16220.460	ODOT	0.14067960	RSTR.	0.0
LMR	-7453.7960	LBARH	-3129.2777	RDOT	0.0	PSIDMG	-150.0
MMR	2099.0574	HBARH	-16040.734	XTR	1132.2927	BTR	2.0
NMR	37721.500	QBAR	30574.350	YTR	-412.12164	MADD	0.0
XMF	-1251.4063	XT	-0.24323272	ZTR	6954.5002	XADD	0.0
YMF	-490.33037	YT	-240.59914	LTR	-12760.902	YADD	0.0
ZMF	31.006362	ZT	973.57446	MTR	-35002.202	NADD	0.0
LAF	005.01173	LT	-549.50561	ALFHTT	-7.1179811	MADD	0.0
MAE	-0302.3095	MT	27452.566	ALFVTT	3.6724344	LADD	0.0
NMF	-4350.9599	NT	6937.5440	AA0IF	4.0040312		
XMT	15.929387	XVT	-16.172620				
YMT	-3.0412724	YVT	-244.97787				
ZMT	972.36537	ZVT	1.2110010				

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WEIGHT	16450.0	FSCG	360.20000	V	150.0	PSITR2	0.0
IX	5130.0	WLCG	245.09999	DELS	-5.0	VXSTR.	0.0
IY	39015.0	RHO	0.17500000E-2	V SOUND	1077.0	VYSTR.	0.0
IZ	37363.0	TIME	0.20000000E-1	NEL3MR	0.0	VZSTR.	0.0
OMEGMR	29.700000	NBS9	0.0	TMSTR	-10.0	PSTR.	0.0
OMEGTR	137.00499	NBS8	5.0	TMSTR	-10.0	WLVT	273.0
KFR	15.0	PASCNT	1217.0	WLMT	234.0	FSTV	695.0
F8HT	700.40000	SMT	45.0	SVT	32.300000	OSTR.	0.0
LAT6TK	-0.00230961	A18	-1.0324957	IMT	-3.7900059	XA	0.0
LNGSTK	11.611350	A18	12.149227	IS	-3.0	XB	0.0
CULSTK	19.707049	TMFTAK	19.707049	TM75MR	9.6270495	XC	0.0
PRDAL	13.060240	TMETTR	24.132707	TM75TR	10.632707	XP	0.0
YAIN	4.4045564	XBIN	0.69700649	XCIN	5.7669060	XPIN	0.0
XPACTP	6.1290514	XBACTI	0.61290514	PSTR.	0.0	PSTR	0.0
VXB	253.44098	PHIAR	0.0	AAOF	2.0850514	OSTR	0.0
VVB	20.427700	PHIAR	0.0	AAIF	-6.6674919	RSTR	0.0
VVB	3.3433339	PHIAR	0.0	AAIF	-6.6674919	TSTR	0.0
P	0.0	GAMC	0.0	AAOL	-6.7631016	HSTR	0.0
O	0.0	OMGRAT	1.0	AAIL	0.28942532	JSTR	0.0
R	0.0	PSIOOT	0.0	ABIL	0.59994065	MMSTR	0.0
ALPWF	-1.1308755	EXTX	1.5297625	EMFAX	0.09109549	LMSTR	0.0
C-ITPP	79.190501	EXTZ	1.7102374	EMFZ	1.0100094	OMSTR	0.0
EXTK	0.0	EPSWT	0.49475044	SIGMT	0.787607A9	YSTR	0.0
QF	59.972029	KOHT	0.47177979	KOVT	0.02716361	YSTR	0.0
MUXB	0.31702210	CTSIG	0.70350900E-1	LTOT	1.4329671	ZSTR	0.0
MUYB	0.25635532E-1	CHSIG	-0.39405606E-2	DTOT	24.475008	LSTR	0.0
MUZS	-0.12456032E-1	CMH8IG	0.40507945E-6	TTR	1610.2133	HSTR	0.0
LAMBMR	0.23021352E-1	NZ	0.94900424	HPMR	2430.2400	NSTR	0.0
DMBMR	0.10565319E-1	VC	0.17081393E-5	KTRBLK	1.0	AXP	0.0
MR	1659.4003	H0AR	-0.14.62689	VXBDOT	0.39704544E-1	AYP	-0.0202939AE-1
YMR	-503.99743	J0AR	503.99743	VYBDOT	-0.47066247E-1	AZP	-32.131320
ZMR	-16090.499	T0AR	16164.541	VZBDOT	0.25432997E-1	VXP	253.44098
LMR	-9031.9533	L0ARH	-4430.2006	PDOT	-0.24540428E-1	VYP	20.427700
MMR	-5293.0107	M0ARH	-22055.029	ODOT	0.04535446E-2	VZP	3.3433339
NMR	43000.137	Q0AR	45004.594	ROOT	-0.4126273AE-2	RSTR.	0.0
XMR	-1410.6413	XT	-15.105101	XTR	0.0	PSIDMG	-150.0
YMR	-703.13565	YT	-336.47040	YTR	1520.7361	RTR	4.0
ZMR	-57.066646	ZT	1047.3707	ZTR	-553.50377	MAOD	0.0
LMP	1110.3496	LT	-743.22357	LTR	9300.4132	YADD	0.0
MP	-0074.7063	MT	3000.0019	MTR	-17149.391	YADD	0.0
NMP	-0074.7063	NT	9300.0019	NTR	-47117.475	ZADD	0.0
XMT	-2.0243054	XVT	-13.160716	ALPHTT	-7.0293717	NAOD	0.0
YMT	-5.1250701	YVT	-331.35352	ALFVTT	4.6209654	NAOD	0.0
ZMT	1000.6340	ZVT	0.74471134	AARBIT	6.6773701	LAOD	0.0



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UTIAS(976)

1-21-77 9-DEC-77

UTIAS(976)

WEIGHT	16450.0	PSCG	360.20000	V	40.0	PSITR2	0.0
IX	5130.0	WLCG	245.49999	DELS	-5.0	VXSTR.	0.0
IY	39815.0	RMO	0.17500000E-2	VDSOUND	1077.0	VYSTR.	0.0
IZ	37363.0	TIME	0.20000000E-1	DEL3MR	0.0	VZSTR.	0.0
OPEGR	29.700000	NBS	4.0	TWSTR	-10.0	PSTR.	0.0
OPEGR	137.00499	NBS	5.0	TWSTR	-10.0	WLVT	273.0
KPR	15.0	PASCNT	1175.0	WLMT	234.0	FSVT	495.0
FSMT	700.40000	SMT	45.0	SVT	32.300000	QSTR.	0.0
LATSTK	-1.5402550	AIS	-2.1864699	IMT	27.196170	XA	40.373406
LANGSTK	0.5755972	BIS	3.6065997	IS	-3.0	X0	19.697535
COLSTK	16.753931	THETA0	16.753931	TH75MR	6.6739314	XC	39.212072
PEDAL	29.430000	THETTR	36.944717	TH75TR	23.464717	XP	0.0
XAIN	4.0373406	X0IN	1.9697535	XCIN	3.9212072	XPIN	0.0
XOACTP	26.260005	XOACTI	2.6266005	RSTR.	0.0	QSTR	0.0
VX0	67.400062	THETAB	4.3907097	AAOF	2.7506776	RSTR	0.0
VY0	0.0	PHIB	-1.5570475	AAIF	-2.3894614	RSTR	0.0
VZ0	5.1750034	RETAWF	0.0	00IF	-0.16066970	TITR	0.0
P	0.0	GAMC	0.0	00BL	-3.7363957	MITR	0.0
O	0.0	OMGRAT	1.0	00IL	0.16875507	JITR	0.0
R	0.0	PSIDOT	0.0	00IL	0.10009442	WHITR	0.0
ALF.F	-15.302040	EKTZ	1.0547407	EKFX	0.73502347	LHITR	0.0
CHITPP	65.832575	EKTZ	2.0403256	EKFX	1.0283348	OHITR	0.0
EXTM	0.0	EPSWT	0.44999999	SIGT	0.0	XITR	0.0
QF	7.3654100	KQMT	0.07922024	KQVT	0.04852013	YITR	0.0
MUX8	0.04000431E-1	CTSIG	0.76034120E-1	LTOT	-25.805696	ZITR	0.0
MUY8	0.0	CHSIG	-0.23447061E-2	DTOT	27.767992	LITR	0.0
MUZ8	0.20500149E-2	COMSIG	0.49497150E-6	TTR	449.37751	MITR	0.0
LAMPUR	-0.33007023E-1	NZ	0.99675502	MPMR	1368.5304	NITR	0.0
DS-MR	0.3594537E-1	VC	0.12842774	KTRBLK	1.0	AXP	2.4850684
XMR	1303.9969	MBAR	-483.75106	VXROOT	0.23207764E-1	AYP	0.67764240
YMR	-364.05799	JBAR	364.05799	VYROOT	0.80000000E-2	AZP	-32.069297
ZMR	-15630.522	TBAR	15686.555	VZROOT	-0.40061604E-2	VXP	67.400062
LHR	-4090.2720	LBARH	-1355.0435	PDOT	0.60305067E-3	VYP	0.0
MHR	10204.747	MBARH	-7463.2022	QDOT	0.19318473E-4	VZP	5.1754034
NHR	24627.950	QBAR	25343.304	PDOT	0.14003002E-2	RSTR.	0.0
XAF	-147.16581	XT	51.720922	XTR	0.0	PSIDMG	-150.0
YAF	0.0	YT	-5.5030531	YTR	790.21312	ATP	2.0
ZAF	236.56495	ZT	105.22862	ZTR	-290.52637	MADD	0.0
LAF	0.0	LT	-12.600395	LTR	4902.6520	XADD	0.0
MAF	-4321.2999	MT	3038.7975	MTR	-9001.4754	YADD	0.0
NAF	0.0	NT	155.76710	NTR	-24731.302	ZADD	0.0
XMT	53.156198	XVT	-1.4352753	ALFMTT	-3.0239126	MADD	0.0
YMT	0.0	YVT	-5.5030531	ALFVTT	0.0	LADD	0.0
ZMT	104.30553	ZVT	0.06300495	AAR0IF	2.3953649		

UTTAS(S76) 1-21-77 9-DEC-77 RUN 44.

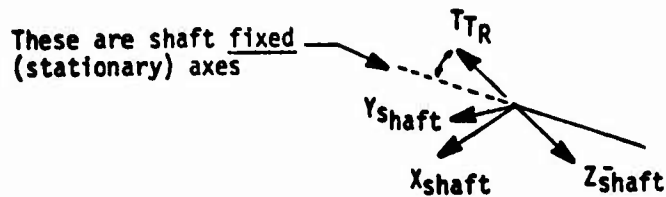
WEIGHT	16450.0	FSCG	369.20900	V	1.0E-2	PSITR2	0.0
IX	5130.0	WLCG	245.49999	NELS	-5.0	VXSTR.	0.0
IY	39015.0	RMO	0.17500000E-2	V SOUND	1077.0	VYSTR.	0.0
IZ	37363.0	TIME	0.20000000E-1	DEL3MR	0.0	VZSTR.	0.0
OMEGMR	29.700000	NBS3	0.0	THSTR	-10.0	PSTR.	0.0
OMEGTR	137.00499	NBS3	5.0	THSTR	-10.0	PLVT	273.0
KFR	15.0	PASCNT	2389.0	WLMT	234.0	FSVT	695.0
PSMT	700.00000	SMT	45.0	SVT	32.300000	QSTR.	0.0
LAT6TK	0.26094394	A19	-0.53516536	IMT	29.750190	XA	51.631150
LNGSTK	7.1574902	A19	2.6911971	IS	-3.0	XB	24.700493
COL8TK	10.211546	THETA6	10.211546	TH75MR	0.1315466	XC	40.322167
PCDAL	29.436000	THETTR	37.5	TH75TR	24.0	XP	0.0
XAIN	5.1631150	XOIN	2.4700493	XCIN	4.0322167	XPIN	0.0
XOACTP	31.855409	XOACT1	3.1855409	RSTR.	0.0	PSTR	0.0
VXB	0.16010099E-1	THETAB	5.9134644	AAOF	2.0255771	QSTR	0.0
VYB	0.0	PHIB	-1.5760910	AAIF	-2.0007439	PSTR	0.0
VZB	0.17412701E-2	MEAMF	0.0	MBIF	-0.50104067	YITR	0.0
P	0.0	GAMC	0.0	AAOL	-4.6050197	HITR	0.0
R	0.0	OMGRAT	1.0	AAIL	0.41316539E-1	JITR	0.0
ALPnF	-10.029242	PSIDNT	0.0	MBIL	0.14074582	WHITR	0.0
CHITPP	-2.8629737	EXTX	-0.20743707	EKWF	0.79995393E-3	LHITR	0.0
ERTX	0.0	EKTZ	0.14490030	EKWF2	0.11099340E-3	GHITR	0.0
QnF	0.26740755E-6	EP3MT	0.44999999	SIGMT	0.0	YITR	0.0
MUXS	0.2110075E-4	KOHT	0.07177979	LTOT	-14.990101	ZITR	0.0
MUY3	0.0	CT8IG	0.74715607E-1	OTOT	25.461353	LITR	0.0
MUZ3	0.10779339E-5	CH8IG	-0.39024013E-2	TTR	506.01745	MITH	0.0
LAM8MR	-0.56017661E-1	CUM8IG	0.51046673E-6	MPMR	1672.9676	NITR	0.0
D8SHMR	0.56010739E-1	NZ	0.99430238	KT8BLK	0.79599999	AXP	3.1646783
YMR	1610.6470	VC	0.43612962E-4	VX8DOT	0.02327105E-3	AYP	-0.23765633E-1
ZMR	-123.36074	W8AR	-0.05.10214	VY8DOT	-0.10271016E-2	AZP	-31.991149
LPR	-15350.093	J8AR	123.36074	VZ8DOT	0.25541996E-3	VXP	0.16010099E-1
MPR	-4223.5659	T8AR	15014.549	POOT	-0.62900257E-3	VYP	0.0
NMR	0.15917470	LB8ARH	-1457.6294	DOOT	-0.01397246E-4	VZP	0.17412701E-2
NMR	30633.330	MB8ARH	-0.050.2773	RUOT	0.36316204	PSTR.	0.0
XAF	-0.59362364E-5	OBAR	30900.003	YTR	0.0	PSIDMG	-150.0
YAF	0.0	XT	1.0021216	VTR	550.71722	MR	2.0
ZAF	0.52175500E-5	YT	-0.34943694E-6	ZTR	-200.44506	MADD	0.0
LAF	0.0	ZT	1.0375275	LTR	3302.5238	YADD	0.0
MAF	-0.12013420E-3	LT	-0.74914510E-6	MTR	-6210.4562	ZADD	0.0
NAF	0.0	MT	47.417676	NTR	-17063.055	MADD	0.0
XMT	1.0021217	NT	0.97492907E-5	ALFMTT	-5.2211661	LADD	0.0
YMT	0.0	XVT	-0.05092081E-7	ALFVTT	0.0		
ZMT	1.6375275	YVT	-0.34943694E-6	AA8BIF	2.9465994		
		ZVT	0.62007346E-7				

## APPENDIX C

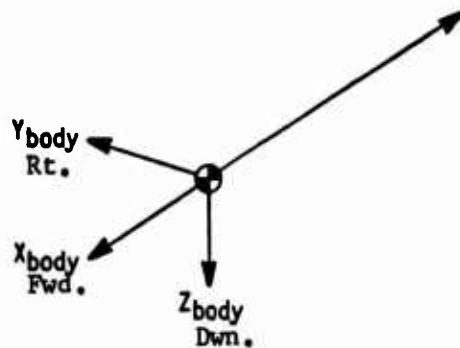
### AIRCRAFT "HANDS OFF" RESPONSE

This Appendix contains the time histories, (Figures C-2 through C-13), of the aircraft for a period of six seconds following blade loss. The axis system, the parametric definition, and the sign convention used are shown in Figure C-1. Shown below is a definition of the symbols used.

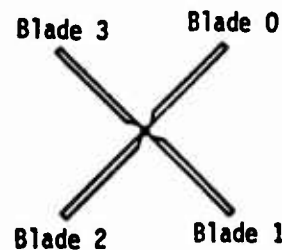
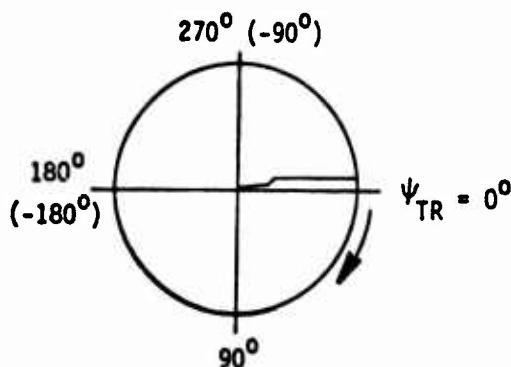
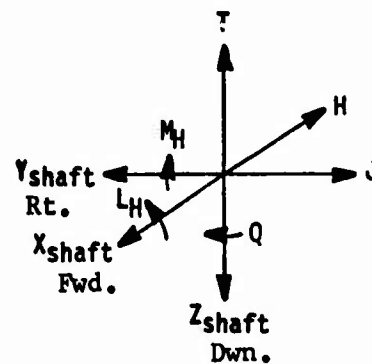
<u>Symbol</u>	<u>Definition</u>
$\psi_{TRb2}$	Tail Rotor (TR) Azimuth Position of Blade #2
$T_{TR}$	Tail Rotor Thrust
$\phi_b$	Aircraft Roll Attitude
$\theta_b$	Aircraft Pitch Attitude
$\psi_b$	Aircraft Yaw Attitude
$a_{xp}$	Longitudinal Acceleration at Pilot's Location
$a_{yp}$	Lateral Acceleration at Pilot's Location
$a_{zp}$	Vertical Acceleration at Pilot's Location



$C = TR \text{ cond angle}$



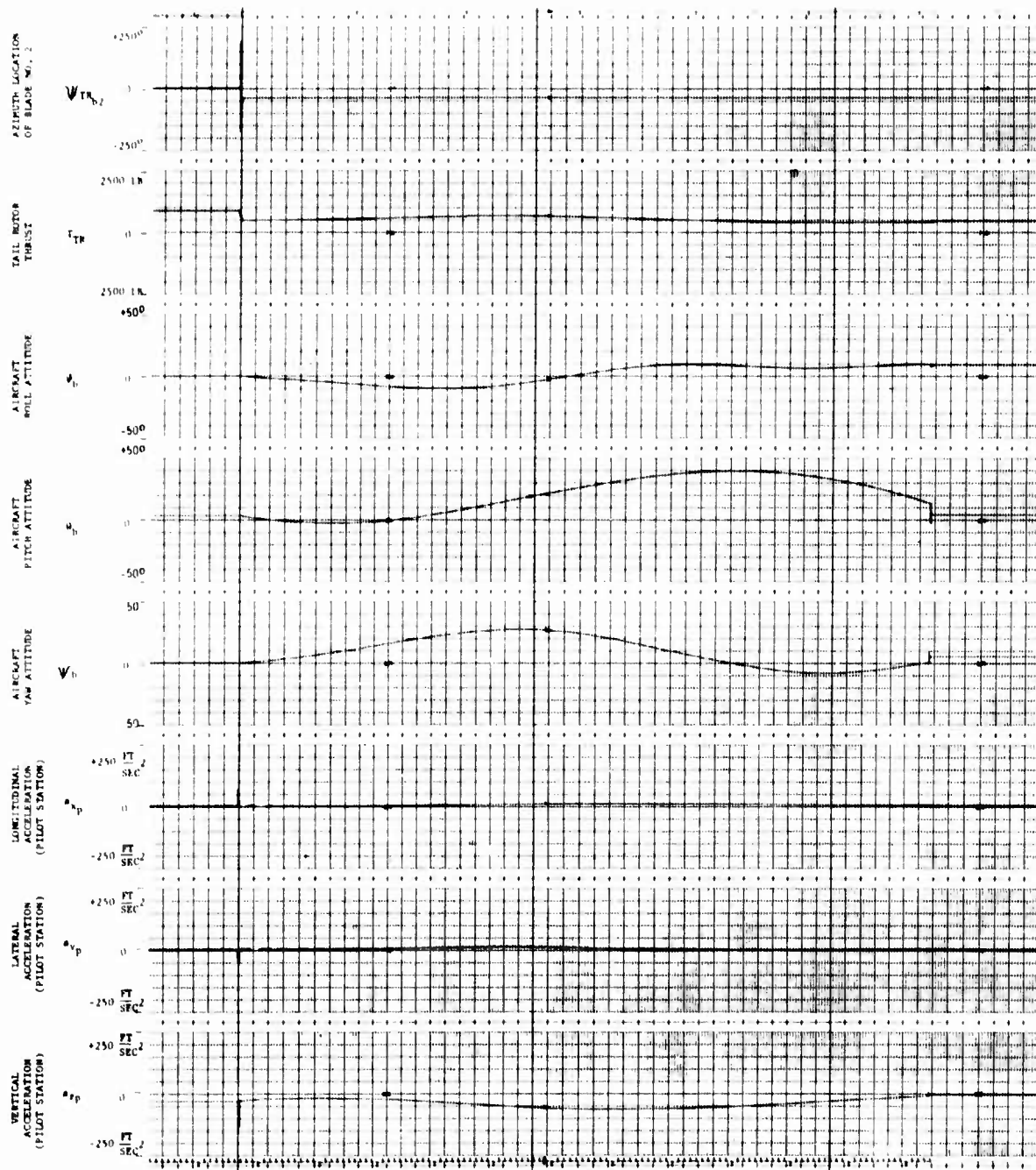
Rotor force, moment convention



**Notes:**

1. Tail Rotor Severance Simulation assumes Blade 0 is entirely lost due to ballistic damage (worst case); then, Blade 2 is completely severed when it reaches the jettison envelope.
2. Computer program required defining  $TR = \pm 180^\circ$  rather than  $0^\circ$  to  $360^\circ$ .
3. Jettison window used in the simulation study was  $-45^\circ \leq \psi_{TR} \leq 25^\circ$  to examine performance characteristics for a blade loss range that exceeds the required  $42^\circ$  window discussed in part 1 of this report.

Figure C-1. Axis System, Parametric Definition, Sign Convention



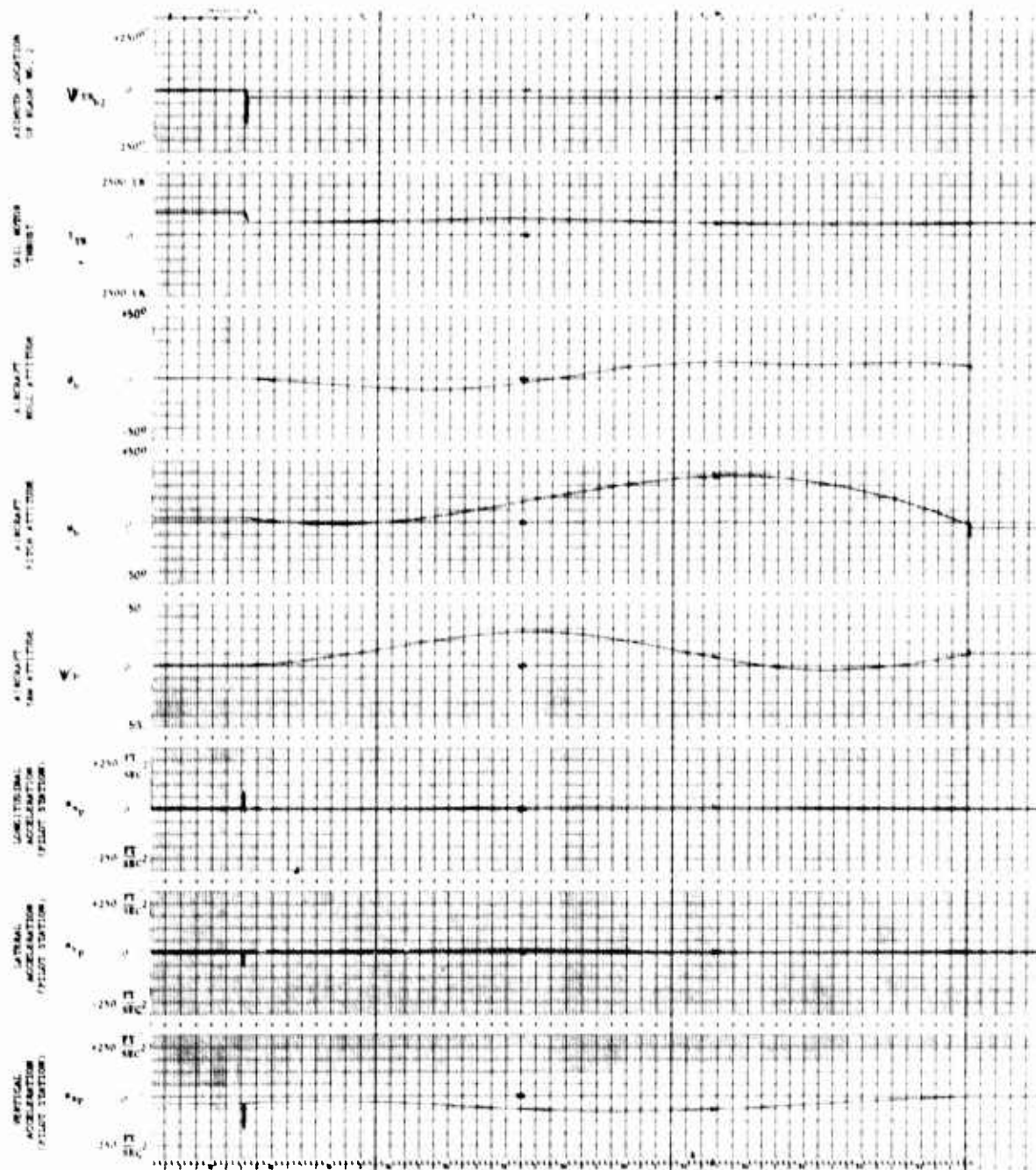
G.W.: 16,450

FSCG: 360.2

$\psi$  Damage:  $0^0$

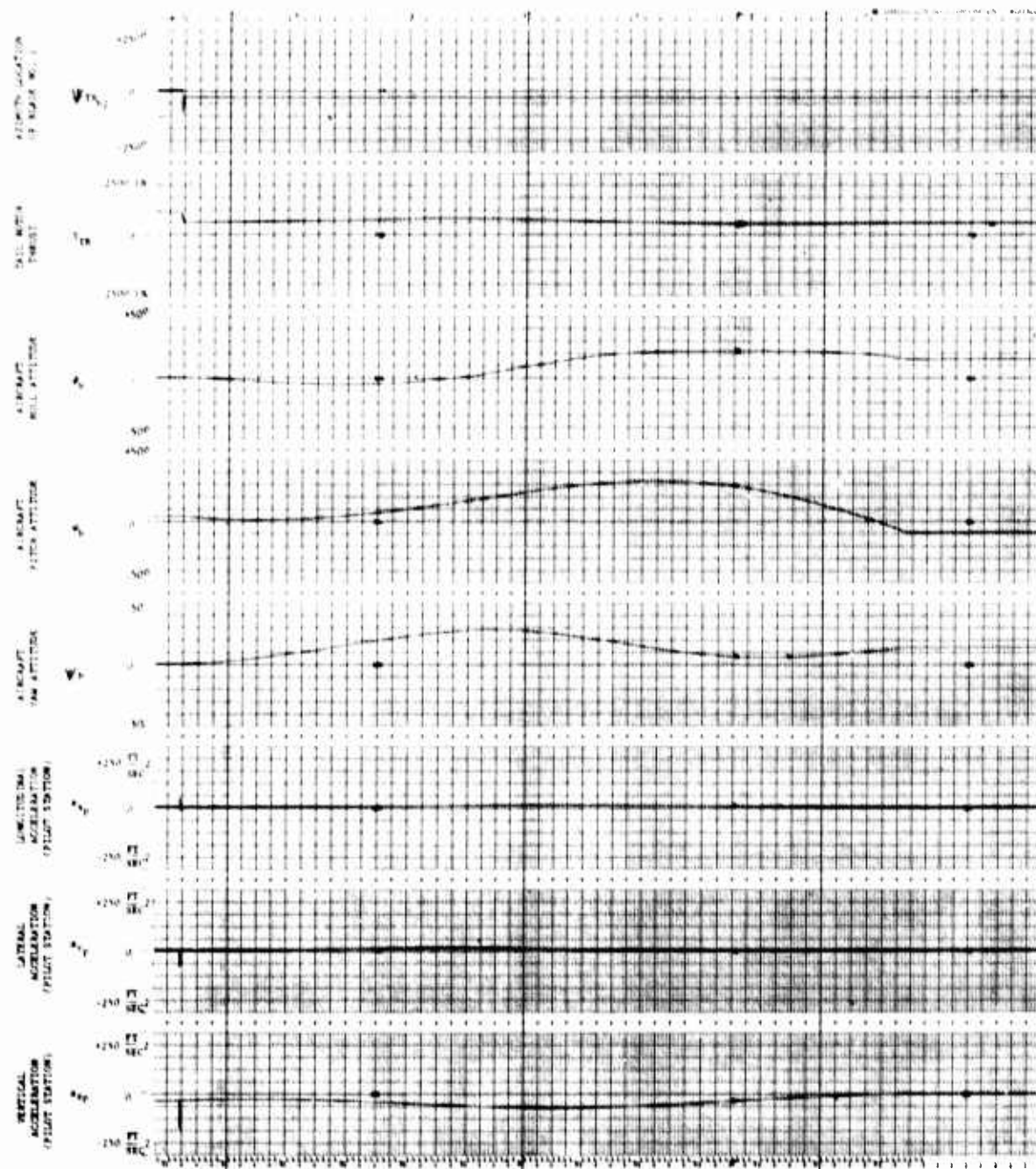
SAS: OFF

Figure C-2. Aircraft "Hands Off" Response ( $0^0$ )



G.W.: 16,450 FSCG: 360.2  $\Psi$  Damage: 50° SAS: OFF

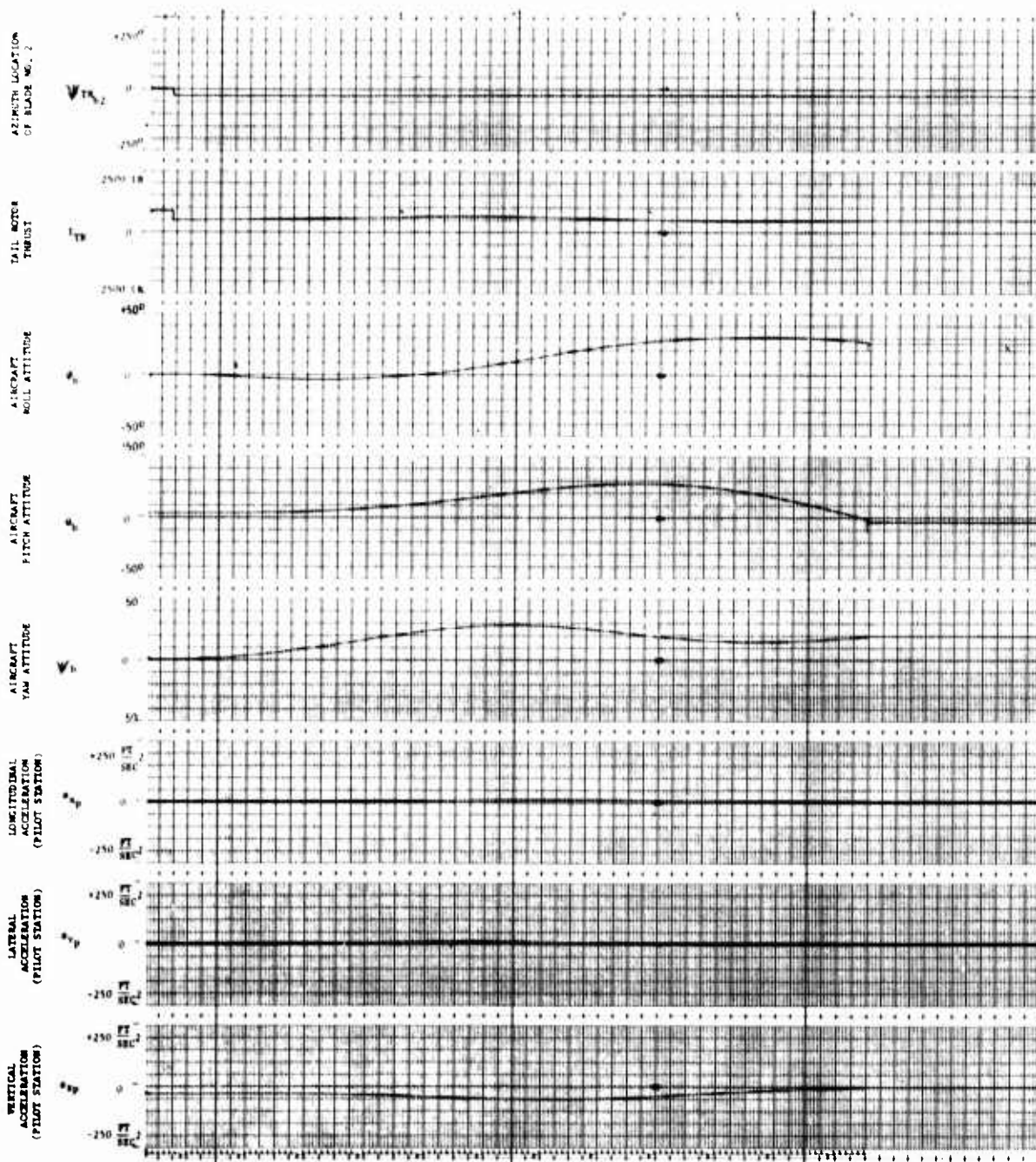
Figure C-3. Aircraft "Hands Off" Response (50°)



G.W.: 16,450      FSCG: 360.2       $\psi$  Damage:  $90^0$       SAS: OFF

Figure C-4. Aircraft "Hands Off" Response ( $90^0$ )

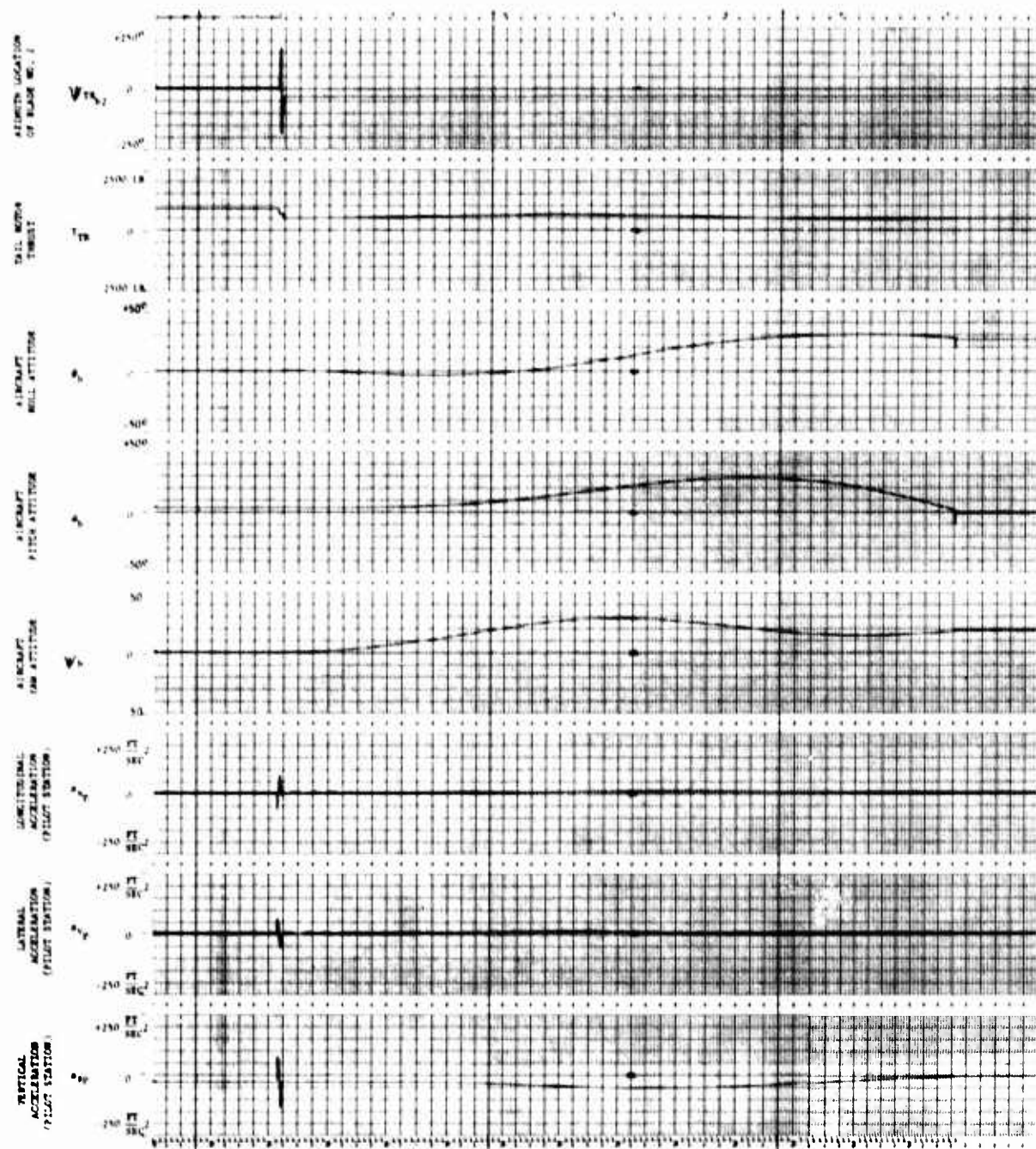




G.W.: 16,450      FSCG: 360.2       $\psi$  Damage:  $150^{\circ}$       SAS: OFF

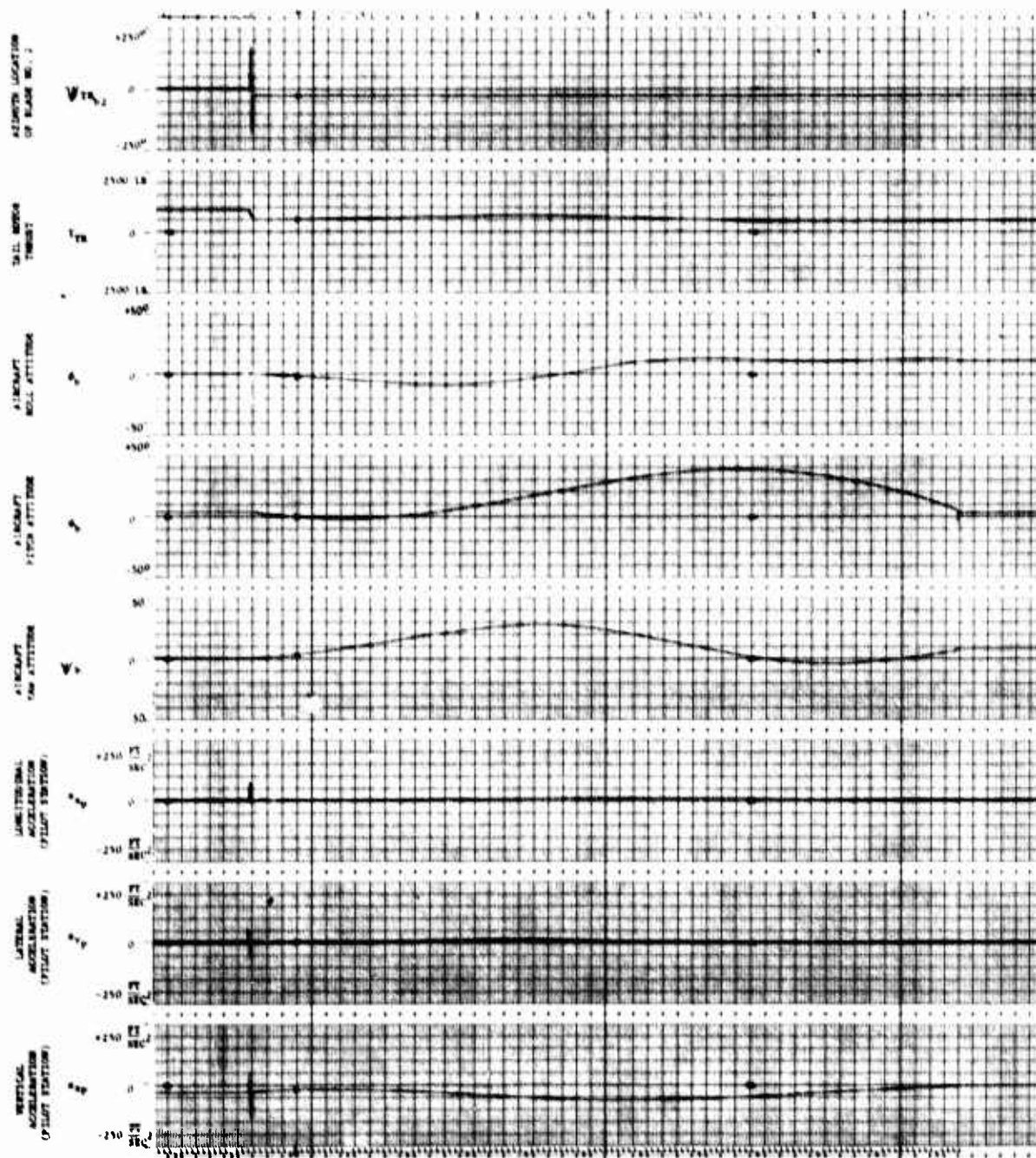
Figure C-5. Aircraft "Hands Off" Response ( $150^{\circ}$ )





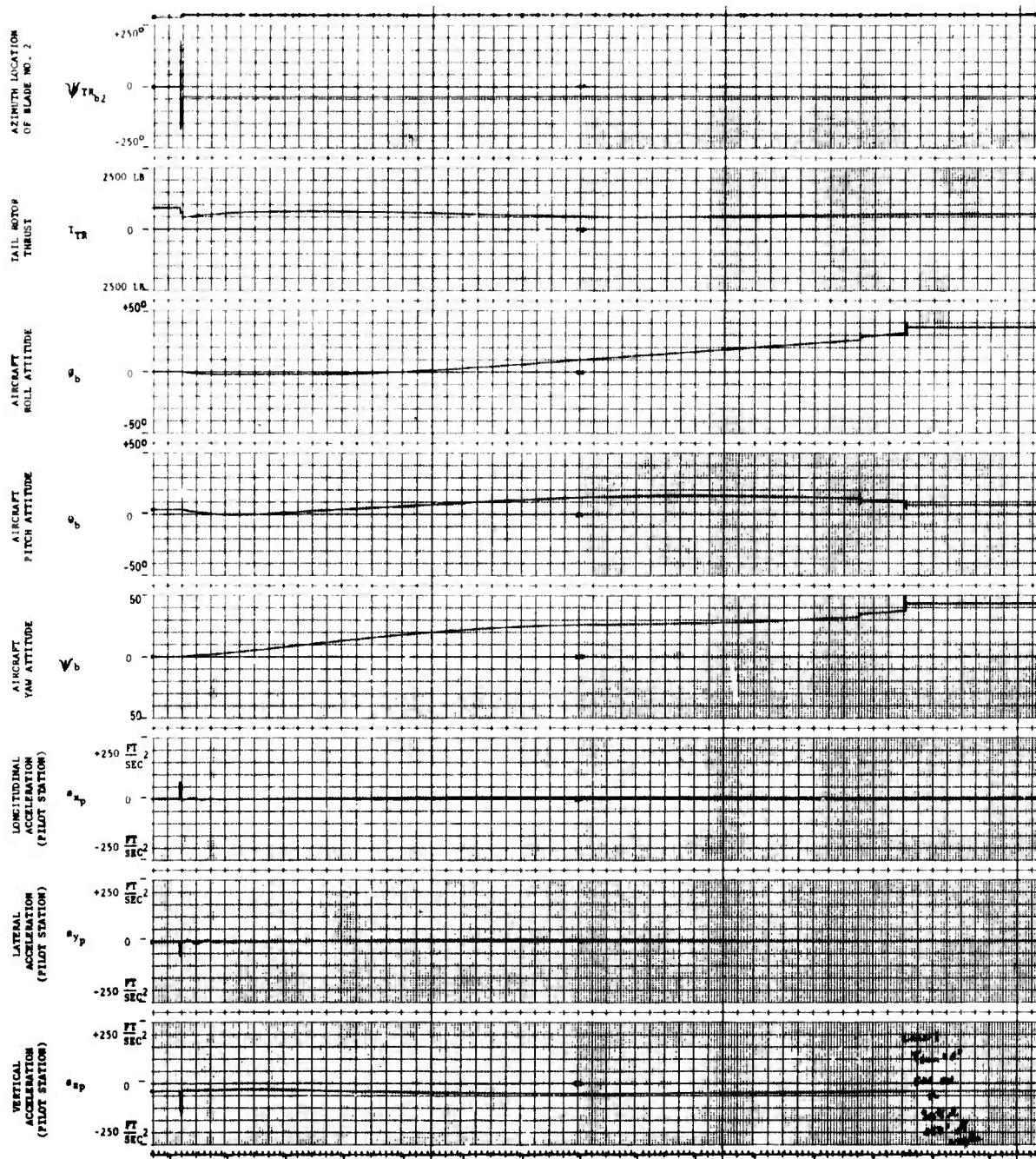
G.W.: 16,450      FSCG: 360.2       $\psi$  Damage:  $-135^{\circ}$       SAS: OFF

Figure C-6. Aircraft "Hands Off" Response ( $-135^{\circ}$ )



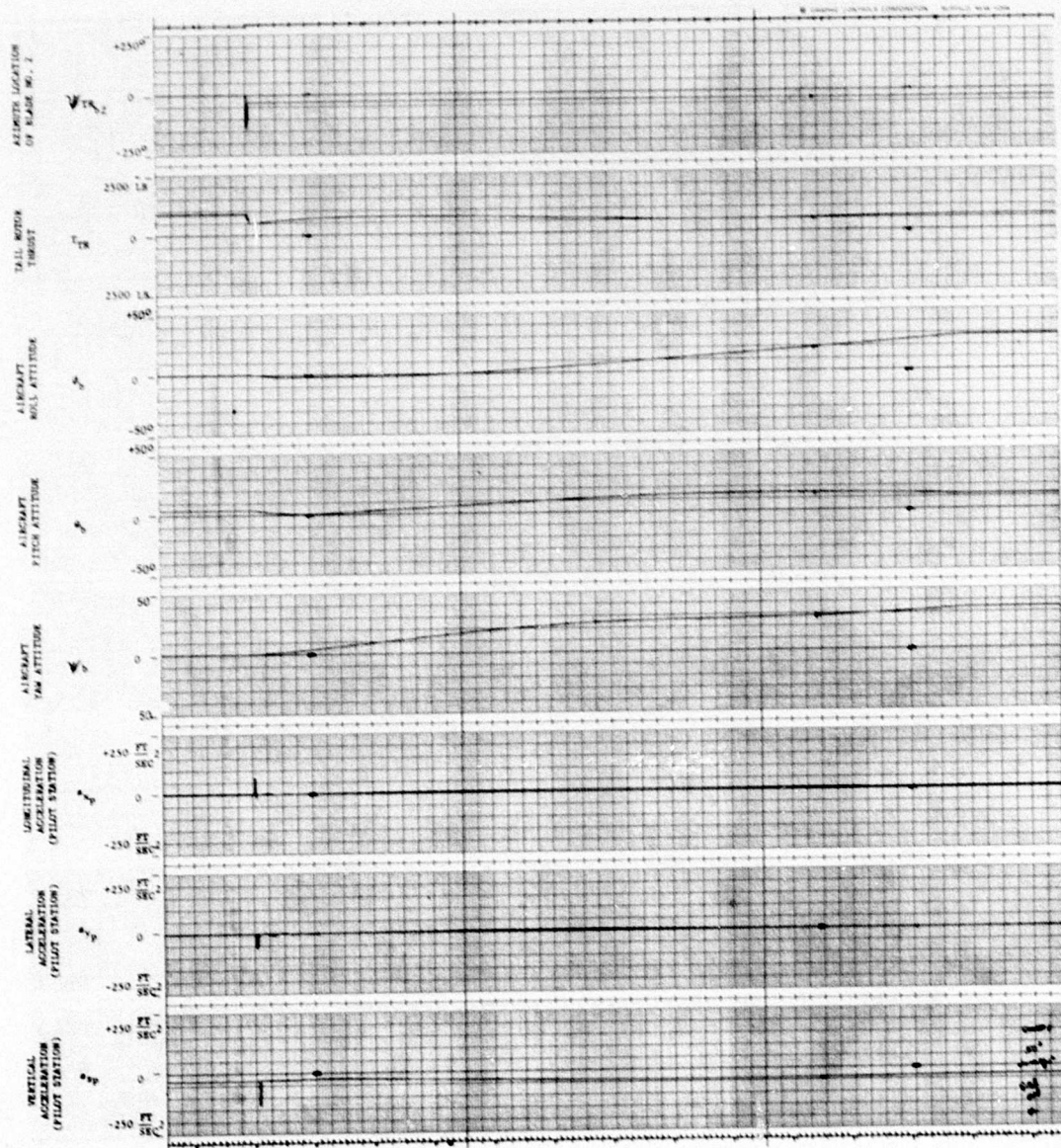
G.W.: 16,450      FSCG: 360.2       $\psi$  Damage:  $-50^\circ$       SAS: OFF

Figure C-7. Aircraft "Hands Off" Response ( $-50^\circ$ )



G.W.: 16,450      FSCG: 360.2       $\psi$  Damage:  $0^0$       SAS: ON

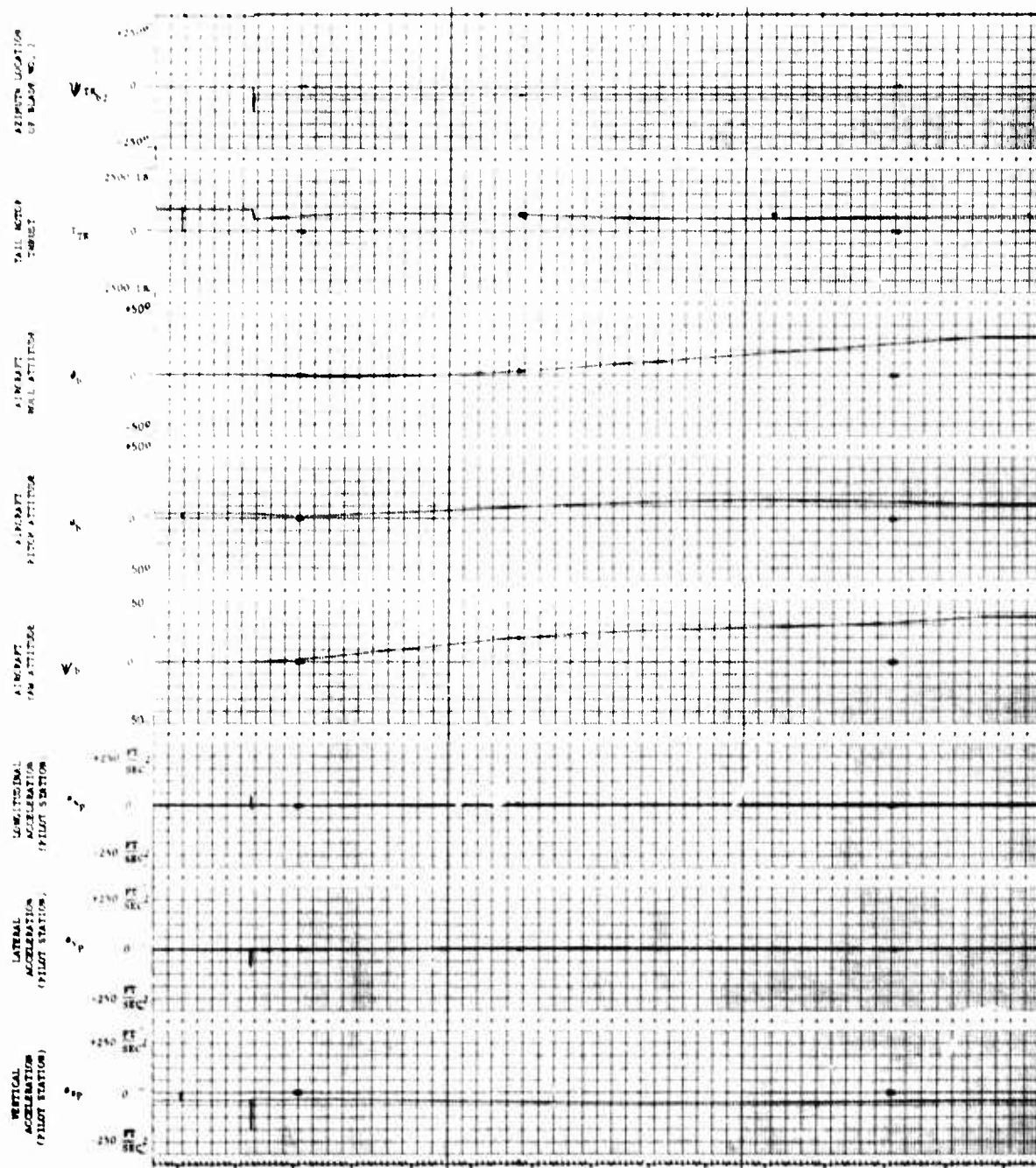
Figure C-8. Aircraft "Hands Off" Response ( $0^0$ )



G.W.: 16,450      FSCG: 360.2       $\psi$  Damage:  $50^0$       SAS: ON

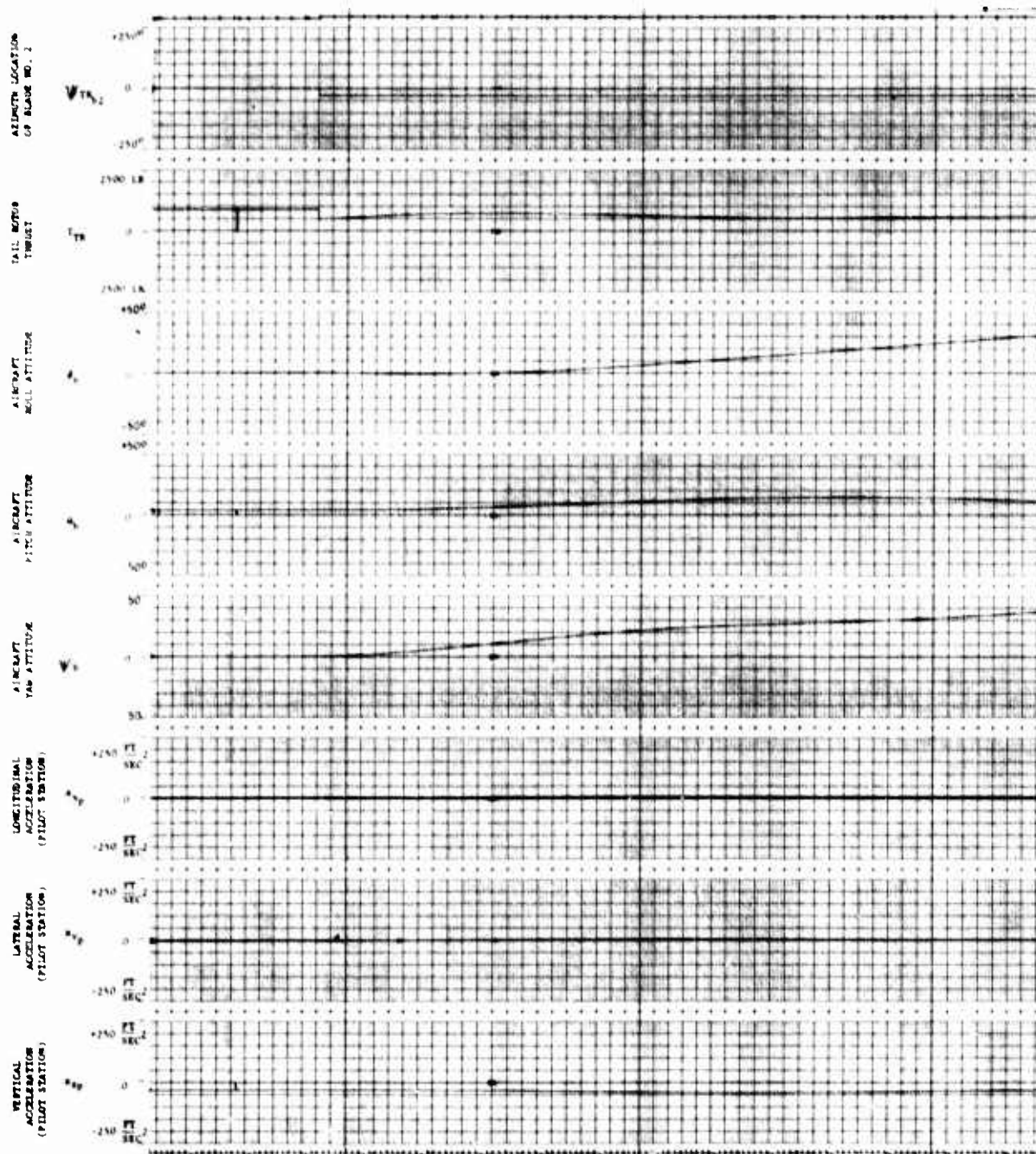
Figure C-9. Aircraft "Hands Off" Response ( $50^0$ )





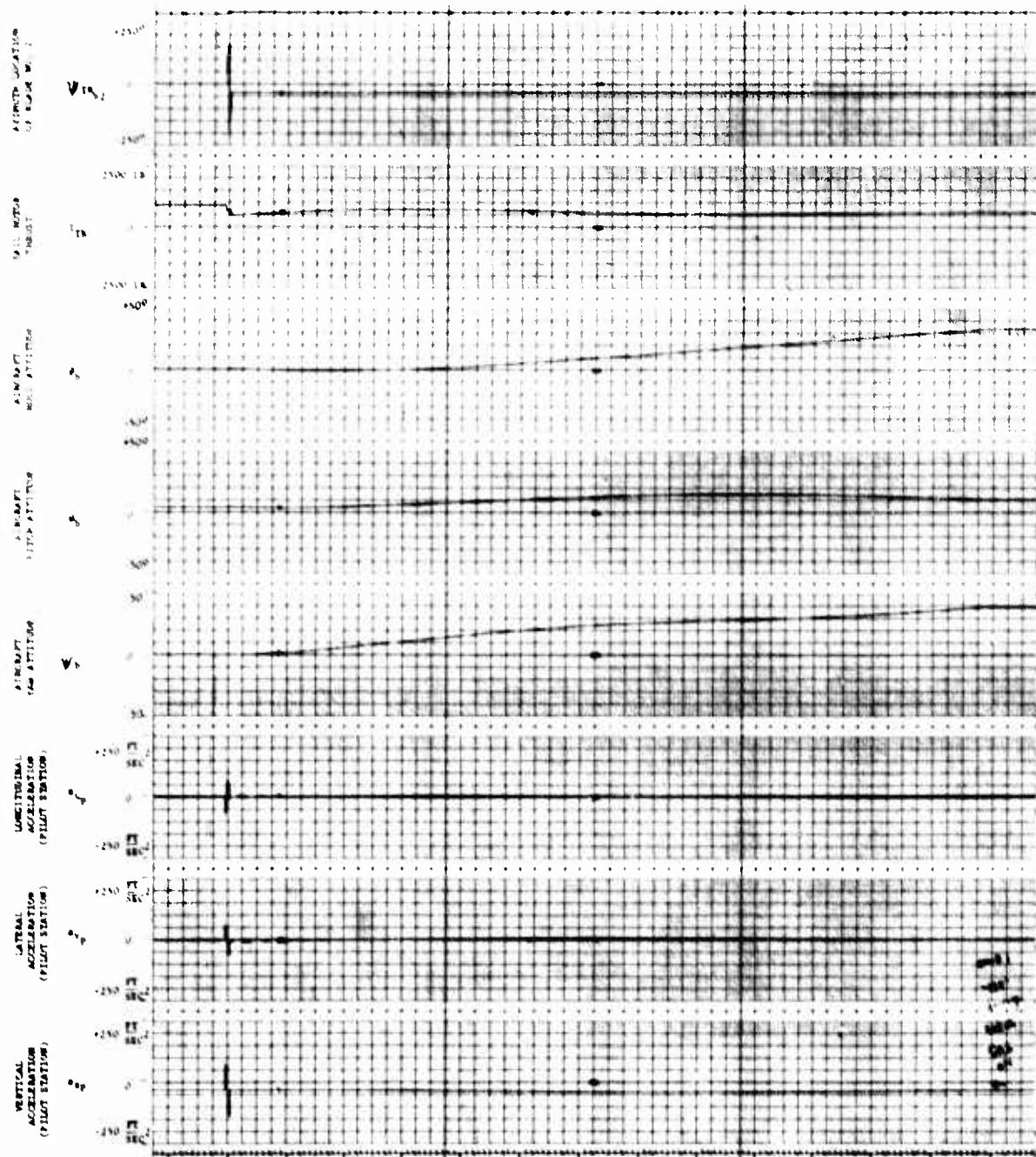
G.W.: 16,450 FSCG: 360.2  $\psi$  Damage:  $90^\circ$  SAS: ON

Figure C-10. Aircraft "Hands Off" Response ( $90^\circ$ )



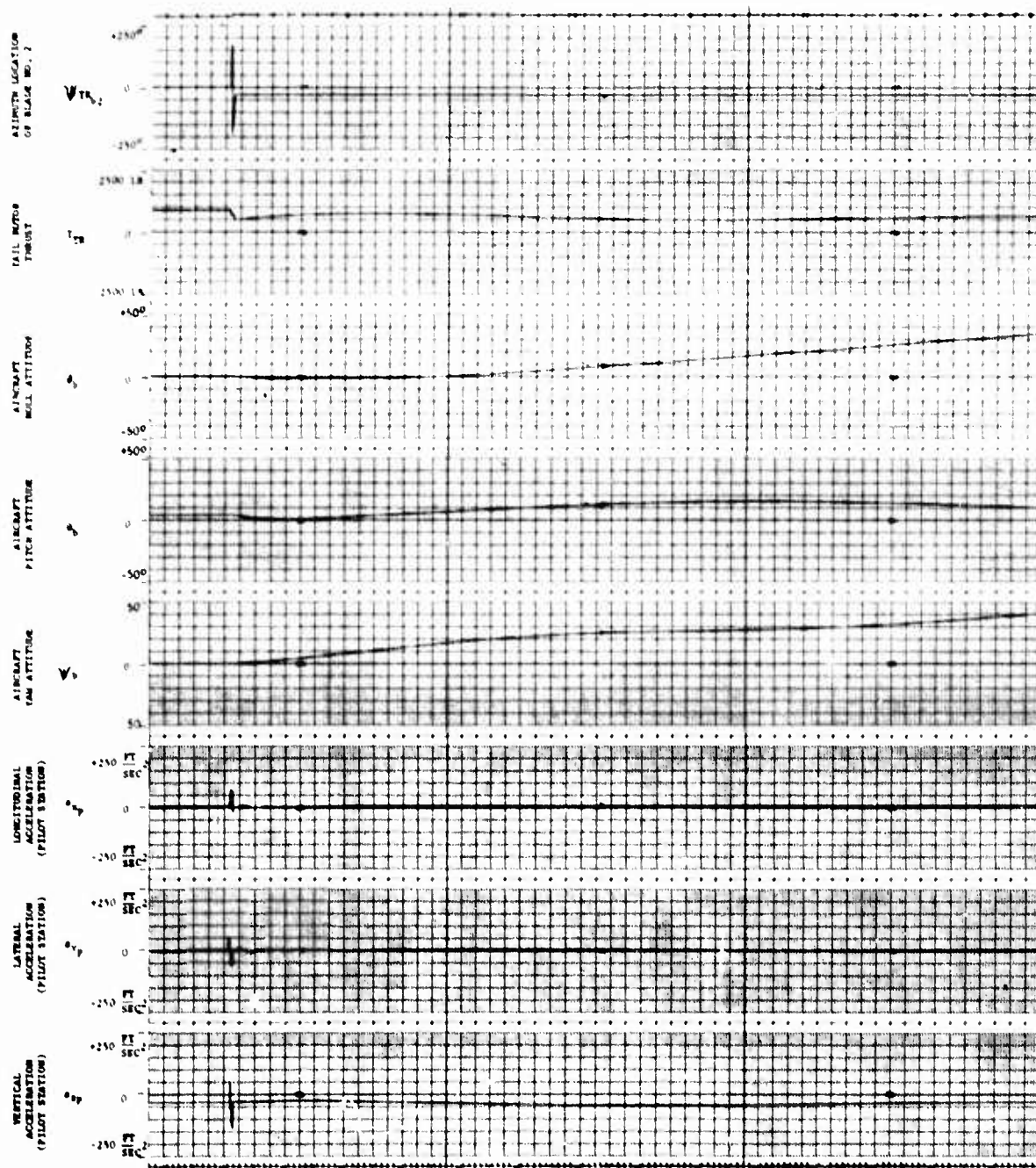
G.W.: 16,450      FSCG: 360.2       $\psi$  Damage:  $150^0$       SAS: ON

Figure C-11. Aircraft "Hands Off" Response ( $150^0$ )



G.W.: 16,450      FSCG: 360.2       $\psi$  Damage:  $-135^{\circ}$       SAS: On

Figure C-12. Aircraft "Hands Off" Response ( $-135^{\circ}$ )



G. W.: 16,450

FSCG: 360.2

$\psi$  Damage:  $-50^\circ$

SAS: ON

Figure C-13. Aircraft "Hands Off" Response ( $-50^\circ$ )



## APPENDIX D

### STEPPED TRANSITION TIME HISTORY TRIM DATA

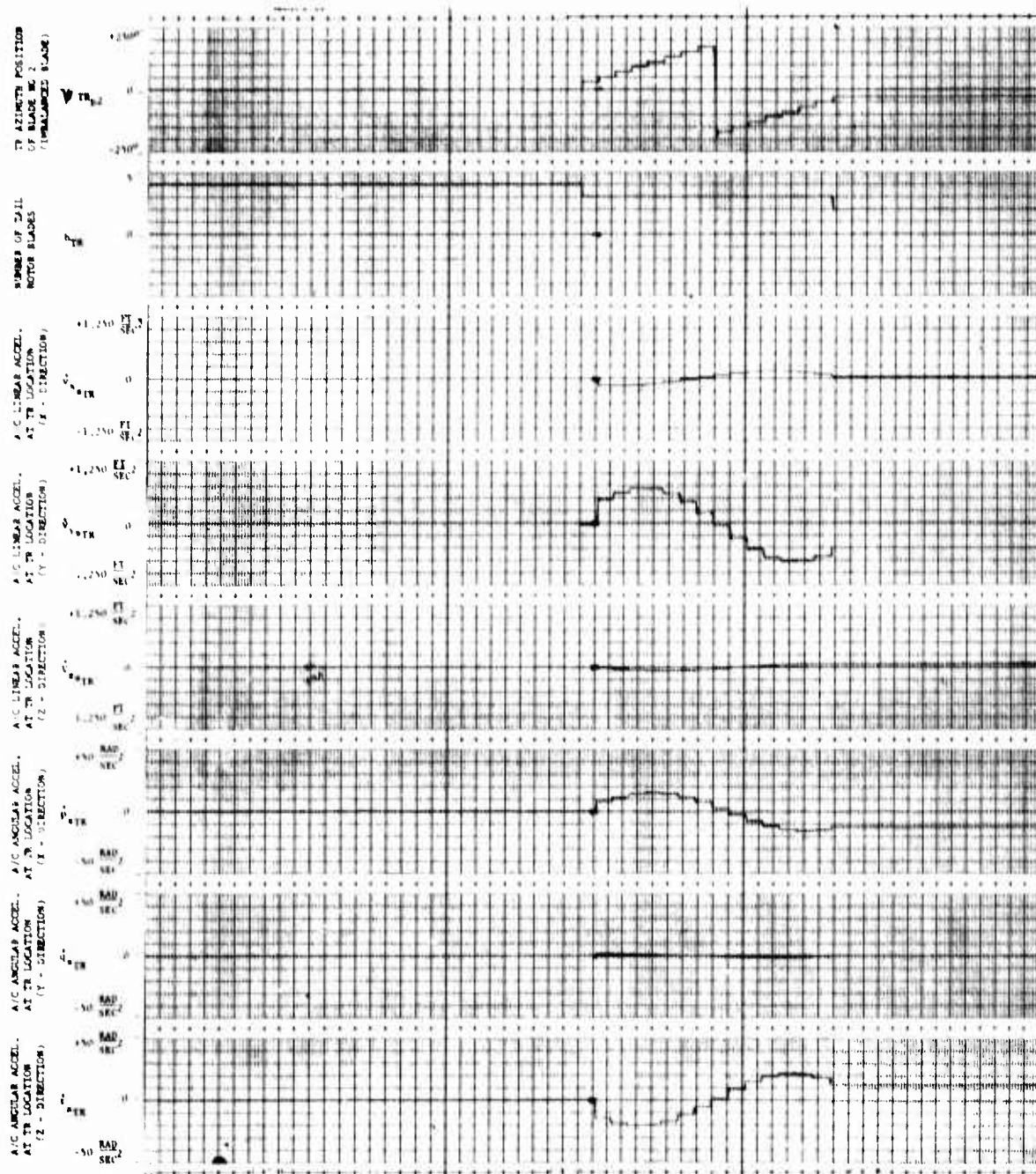
Figures D-1 through D-12, included in this Appendix, are the time history cases performed to determine the helicopter response to the unbalanced load during transition from four to two tail rotor blades. With the exception of Figure D-8, computer printouts have been provided for reference. Definitions for the key symbols and abbreviations used are provided below.

<u>Symbol</u>	<u>Definition</u>
TR b2	Tail Rotor (TR) Azimuth Position of Blade #2 (Imbalanced Blade)
b <sub>TR</sub>	Number of Tail Rotor Blades
$\dot{v}_{xSTR}$	Aircraft Linear Accelerations at TR Location (FSTR, BLTR, WLTR) Measured Along TR Fixed Shaft in X-Direction
$\dot{v}_{ySTR}$	Aircraft Linear Accelerations at TR Location (FSTR, BLTR, WLTR) Measured Along TR Fixed Shaft in Y-Direction
$\ddot{v}_{xSTR}$	Aircraft Linear Accelerations at TR Location (FSTR, BLTR, WLTR) Measured Along TR Fixed Shaft in X-Direction
$\ddot{v}_{zSTR}$	Aircraft Linear Accelerations at TR Location (FSTR, BLTR, WLTR) Measured Along TR Fixed Shaft in Z-Direction
$\dot{p}_{STR}$	Aircraft Angular Accelerations at TR Location (FSTR, BLTR, WLTR) Measured About TR Fixed Shaft in X-Direction
$\dot{q}_{STR}$	Aircraft Angular Accelerations at TR Location (FSTR, BLTR, WLTR) Measured About TR Fixed Shaft in Y-Direction
$\dot{r}_{STR}$	Aircraft Angular Accelerations at TR Location (FSTR, BLTR, WLTR) Measured About TR Fixed Shaft in Z-Direction

<u>Symbol</u>	<u>Definition</u>
$T_{TR}$	Tail Rotor Thrust
$\phi$ b	Aircraft Roll Attitude
$\theta$ b	Aircraft Pitch Attitude
$\psi$ b	Aircraft Yaw Attitude
$a_{xp}$	Longitudinal Acceleration at Pilot Location (Along Body Z-Direction)
$a_{yp}$	Lateral Acceleration at Pilot Location (Along Body Y-Direction)
$a_{zp}$	Normal Acceleration at Pilot Location (Along Body Z-Direction)
$F_{yITRb3}$	Inertial Force Along TR Blade #3 (Spar) in the Y-Direction
$*T_{ITR}$	Total (Sum of All Three Blades) TR Inertial Force Along TR Shaft (-) Z-Direction
$*H_{ITR}$	Total (Sum of All Three Blades) TR Inertial Force Along TR Shaft (-) X-Direction
$*J_{ITR}$	Total (Sum of All Three Blades) TR Inertial Force Along TR Shaft (-) Y-Direction
$*M_{HITR}$	Total TR Hub Pitching Moment Due to Blade Inertial Loads (Moment About Shaft Y-Axis)
$*L_{HITR}$	Total TR Hub Rolling Moment Due to Blade Inertial Loads (Moment About Shaft X-Axis)
$*Q_{HITR}$	Total Moment About Shaft Due to Blade Inertial Loads (Moment About Shaft Z-Axis)
$\dot{p}$	Aircraft Roll Acceleration
$\dot{q}$	Aircraft Pitch Acceleration
$\dot{r}$	Aircraft Yaw Acceleration
$p$	Roll Rate
$q$	Pitch Rate

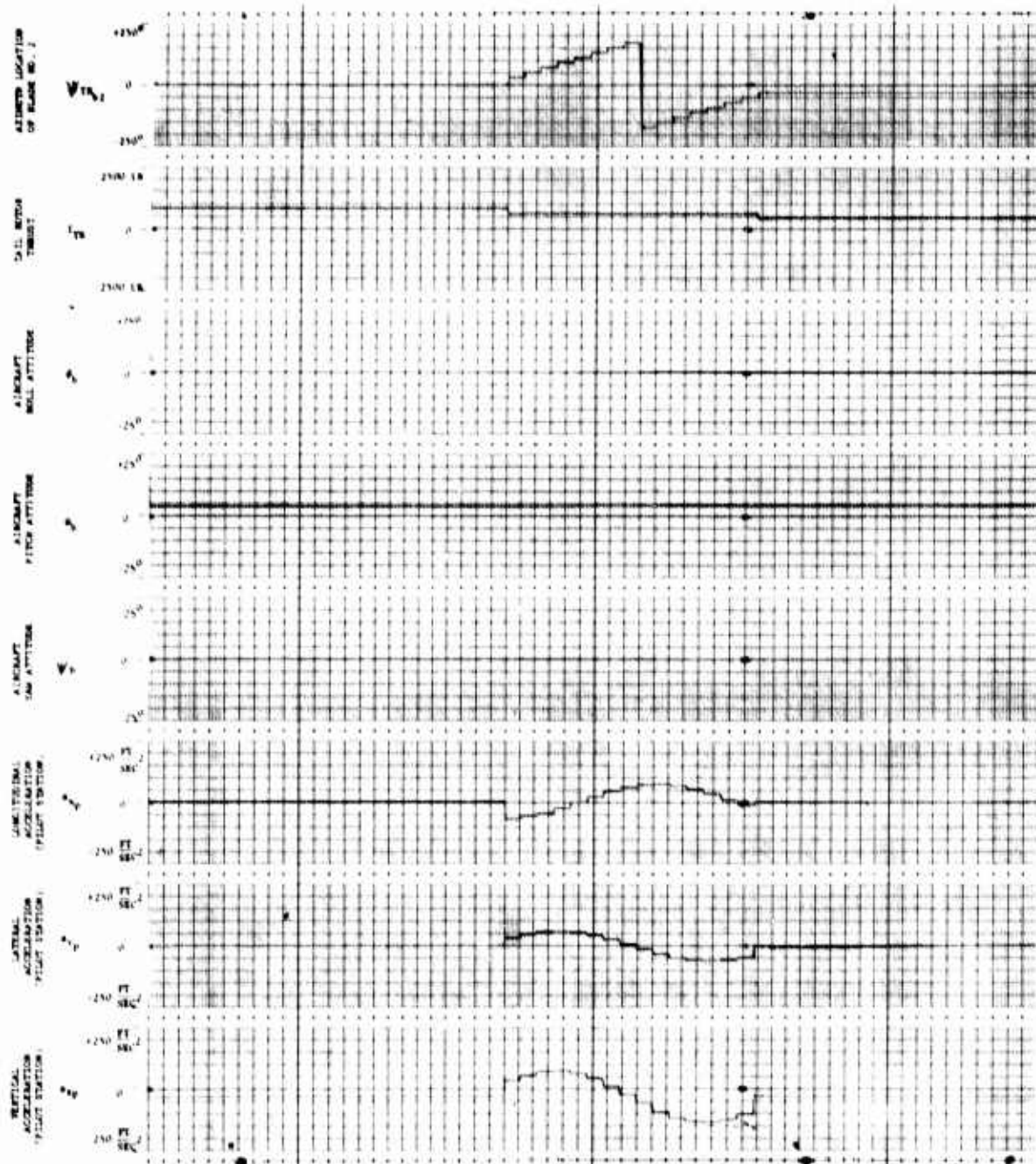
<u>Symbol</u>	<u>Definition</u>
r	Yaw Rate
V	Airspeed

\*These total forces and moments imply the summation for all three blades and are the inertial contributions without aerodynamic contributions.



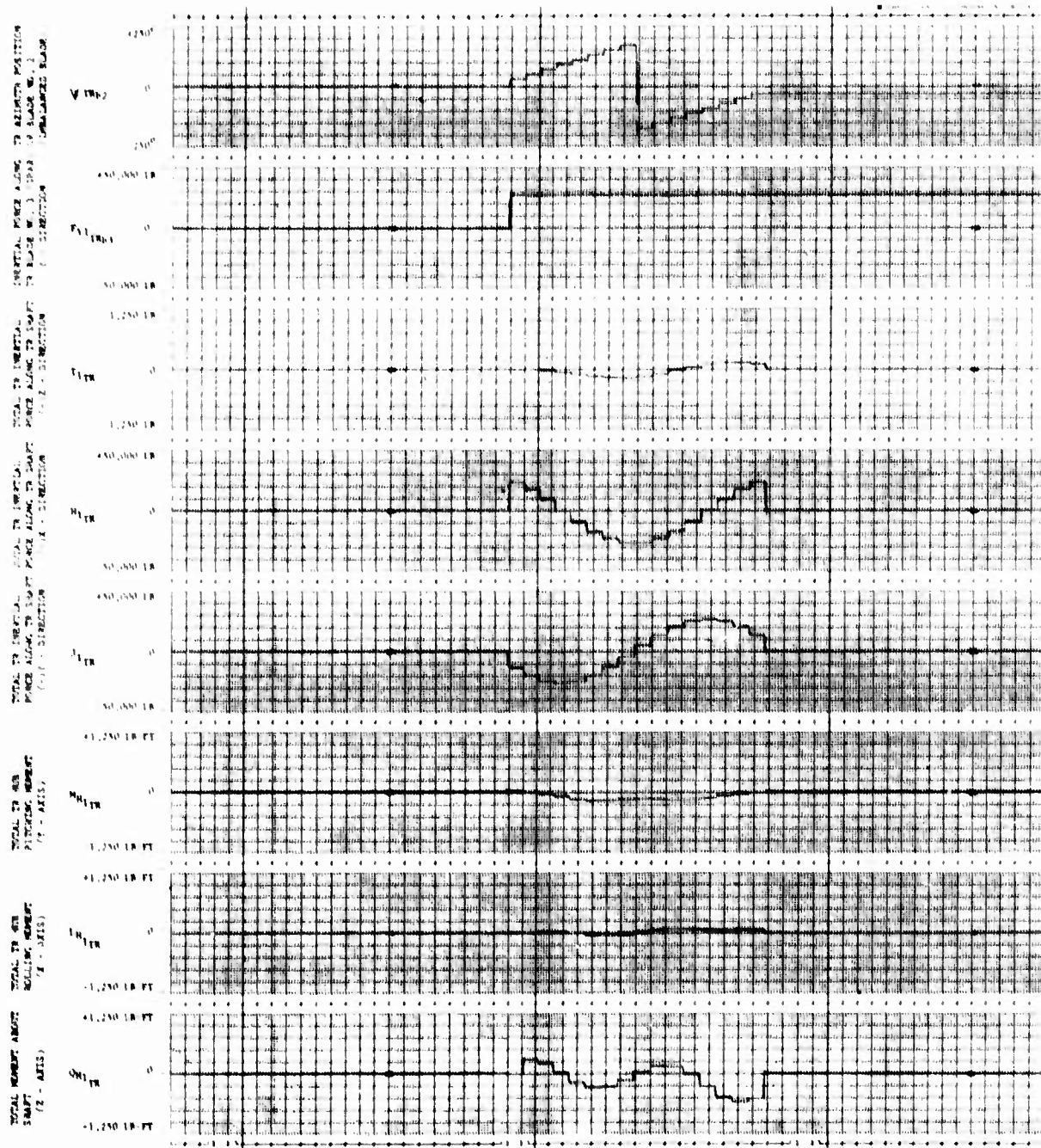
G.W.: 16,450 Lb. FSCG: 360.2 V: 100 Kts  $N_R$ : 100% SAS: OFF  
 $H_D$ : SLS

Figure D-1. Stepped Transition Time History



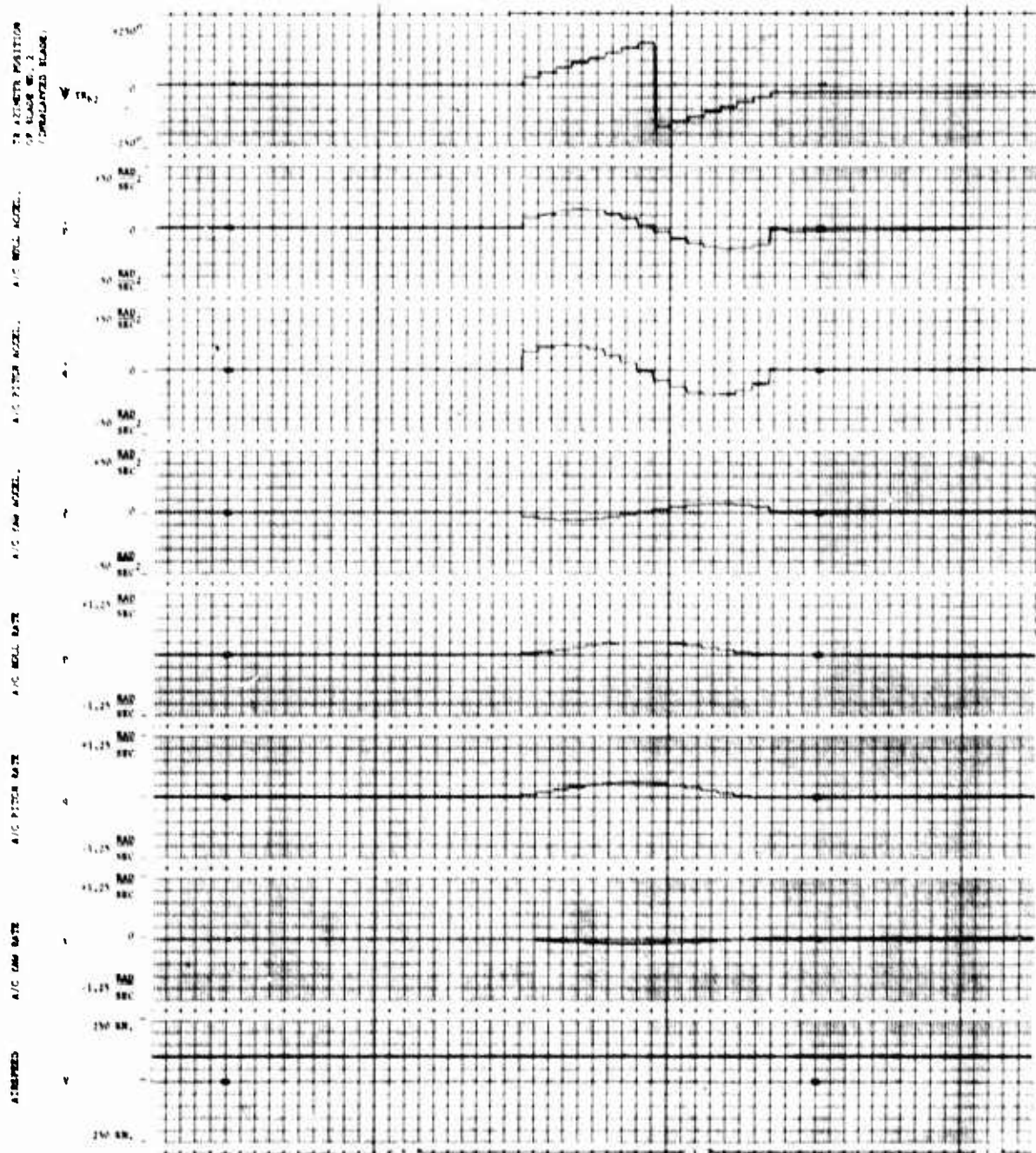
G.W.: 16,450 Lb. FSCG: 360.2 V: 100 Kts  $N_R$ : 100% SAS: OFF  $H_D$ : SLS

Figure D-1. (continued)



G.W.: 16,450 Lb. FSCG: 360.2 V: 100 Kts  $N_R$ : 100% SAS: OFF  $H_D$ : SLS

Figure D-1. (continued)



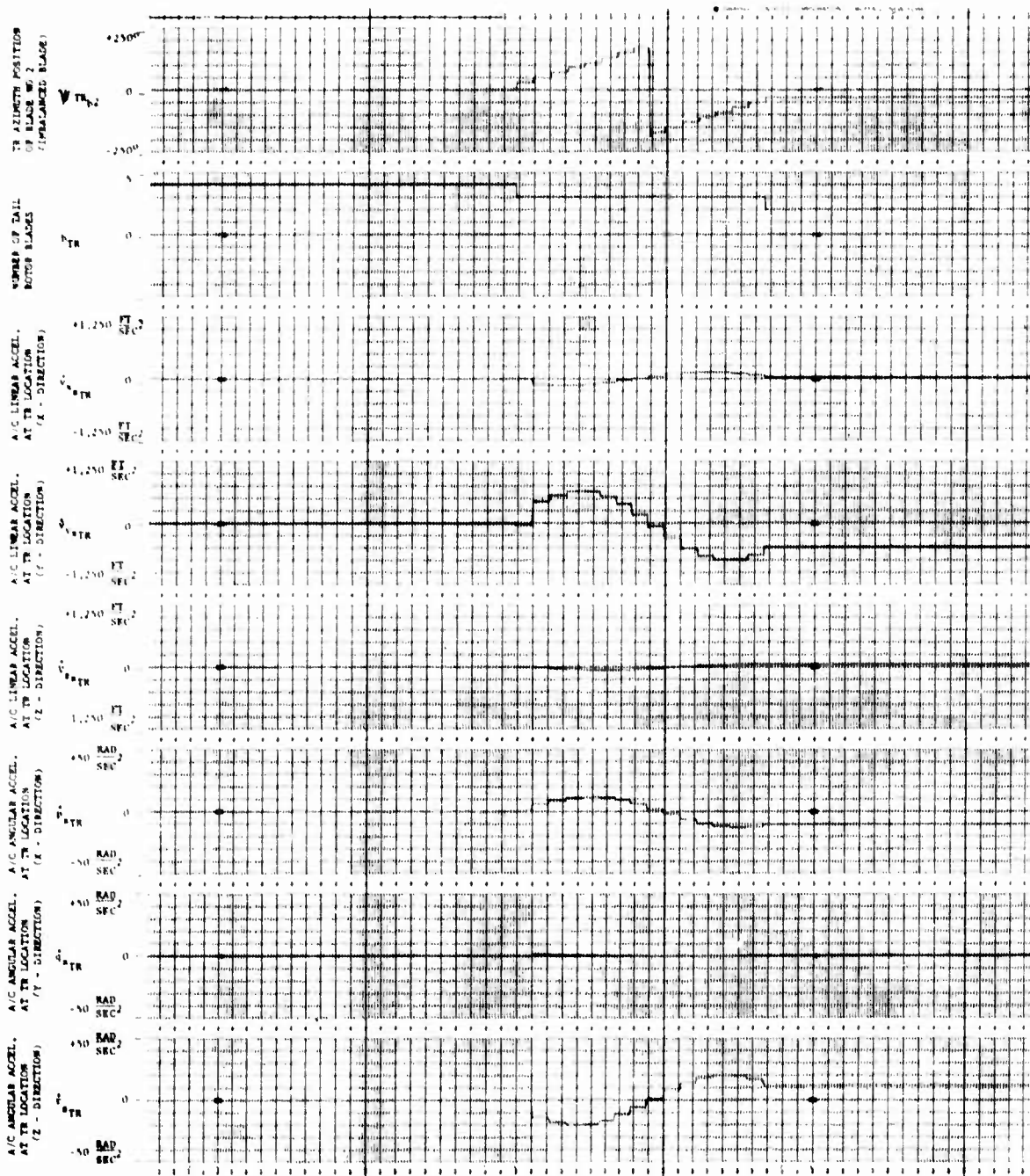
G.W.: 16,450 Lb. FSCG: 360.2 V: 100 Kts  $N_R$ : 100% SAS: OFF  $H_D$ : SLS  
 Figure D-1. (continued)



HEIGHT	16450.0	PSCG	360.20000	V	100.0	PSITR2	0.0
IX	4330.0	WLCG	245.89999	DELS	-5.0	VXSTR	0.0
IY	38515.0	RMD	0.23700000E-2	VROUND	1116.0	VYSTR	0.0
IZ	37363.0	TIME	0.20000000E-1	DEL3MR	0.0	VZSTR	0.0
OMEGMR	27.0	W88	4.0	THSTR	-18.0	PSTR	0.0
OMEGTR	124.55000	M388	5.0	THSTR	-10.0	MLVT	273.0
KFR	15.0	PASCMT	1217.0	WLMT	234.0	FSTV	695.0
FSMT	704.40000	SHY	45.0	SVT	32.30000	QSTR	0.0
LATSTR	-0.59340201	A18	-1.2161207	IHT	-2.7695562	XA	46.290737
LNGSTR	0.7472700	B18	0.0031660	IS	-3.0	XB	19.090009
COLSTR	16.525114	THETAB	16.525114	TH5MR	6.4451140	XC	37.701963
PEDAL	11.107135	THETTR	10.401292	TH5TR	4.9412920	XP	50.590054
XAIN	4.6290737	X0IN	1.0090000	XCIN	3.7701963	XPIN	2.7317019
XOACTP	21.024000	Y0ACTI	2.1024000	RSTR	0.0	PSTR	0.0
VXB	168.65003	THETAB	3.600052	AAOF	3.1014497	QSTR	0.0
VYB	11.391420	PHIB	0.0	AAIF	-5.0061062	RSTR	0.0
VZB	10.047795	BEYAF	3.6790095	BBIF	0.0064945E-1	TSTR	0.0
P	0.0	GANC	0.0	AAOL	-4.1900659	MSTR	0.0
Q	0.0	OHGRAT	1.0	AAIL	0.24107694	JSTR	0.0
ALP-F	0.5500096	P01DOT	0.0	BBIL	0.36200003	MHSTR	0.0
CHITPP	02.003004	EKTX	1.6400261	EKMF	0.92606998	LMSTR	0.0
EKTR	0.0	ERTZ	0.40079009	EKFZ	1.0079961	OHSTR	0.0
Q-F	37.429361	KDHT	0.47177979	SIGMT	0.64751975	XSTR	0.0
MUX	0.23325674	CS10	0.67070526E-1	KQVT	0.83100377	YSTR	0.0
MUY	0.15725112E-1	CH910	-0.47506950E-2	LTOT	3.4630934	ZSTR	0.0
MUZ	0.27690011E-2	CH916	0.4902652E-6	DTOT	24.401060	LSTR	0.0
LAM0MR	-0.97539494E-2	NZ	0.99785491	TTR	0.37.04561	MSTR	0.0
D-0MR	0.12522950E-1	VC	0.71325573E-5	MPMR	1133.2135	NSTR	0.0
XMR	1922.0494	H0AR	-1100.6090	NR0LK	1.0	AXP	2.0042153
YMR	-254.36015	J0AR	254.36015	VX0DOT	0.15104240E-2	AYP	-0.24406269E-1
ZMR	-15644.553	T0AR	15725.929	VY0DOT	-0.14360017E-1	AZP	-32.103912
LMR	-5026.5936	LB0AR	-2281.0103	VZ0DOT	0.23909519E-2	VXP	160.65003
MMR	-042.14135	MB0AR	-15256.386	PDOT	-0.95050965E-2	VYP	11.391420
NMR	22507.512	OBAR	23003.979	QDOT	0.20261896E-2	VZP	10.047795
XMF	-093.60000	XT	-23.053153	RUOT	-0.29749000E-2	RSTR	0.0
YMF	-361.12700	YT	-170.11212	XTR	0.0	PSIDM0	-150.0
ZMF	-130.22601	ZT	464.03322	YTR	706.62407	BTR	4.0
LMP	556.64727	LT	-395.01927	ZTR	-206.30030	MADD	0.0
MMP	-3392.2619	MT	13103.227	LTR	4031.4717	XADD	0.0
NMP	-3194.7142	NT	4970.2169	MTR	-0070.7055	YADD	0.0
XMT	-13.177201	XVT	-10.075071	NTR	-24372.235	ZADD	0.0
YMT	-1.9745510	YVT	-176.13757	ALPMTT	-4.7546403	MADD	0.0
ZMT	464.26319	ZVT	0.37003121	ALPVT	3.0617782	LAOD	0.0
				A00B1F	5.00600070		

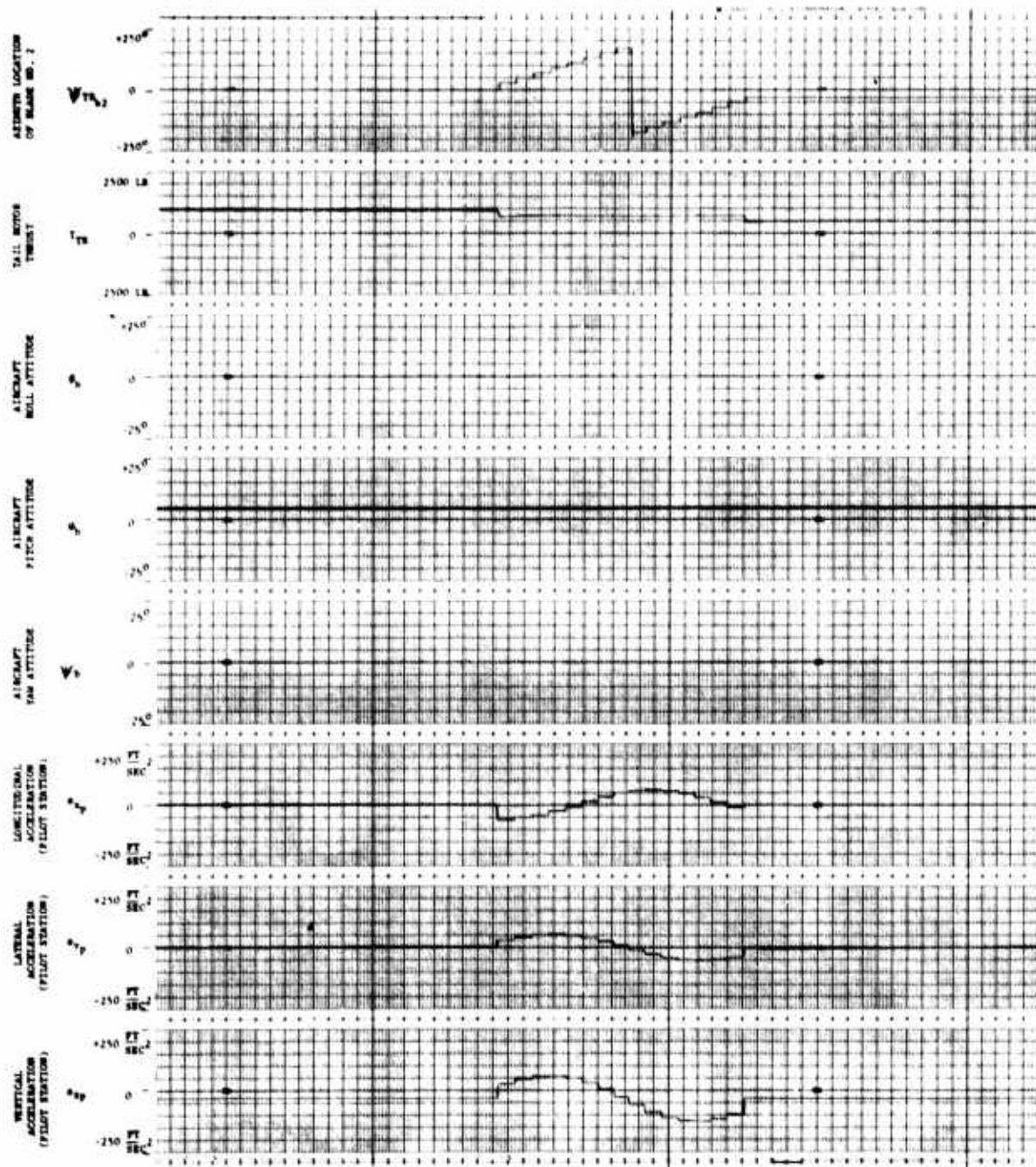
Figure D-1. (continued)





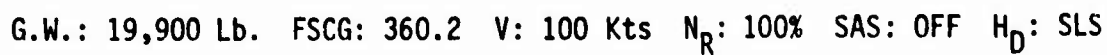
G.W.: 19,900 Lb. FSCG: 360.2 V: 100 Kts  $N_R$ : 100% SAS: OFF  $H_D$ : SLS

Figure D-2. Stepped Transition Time History

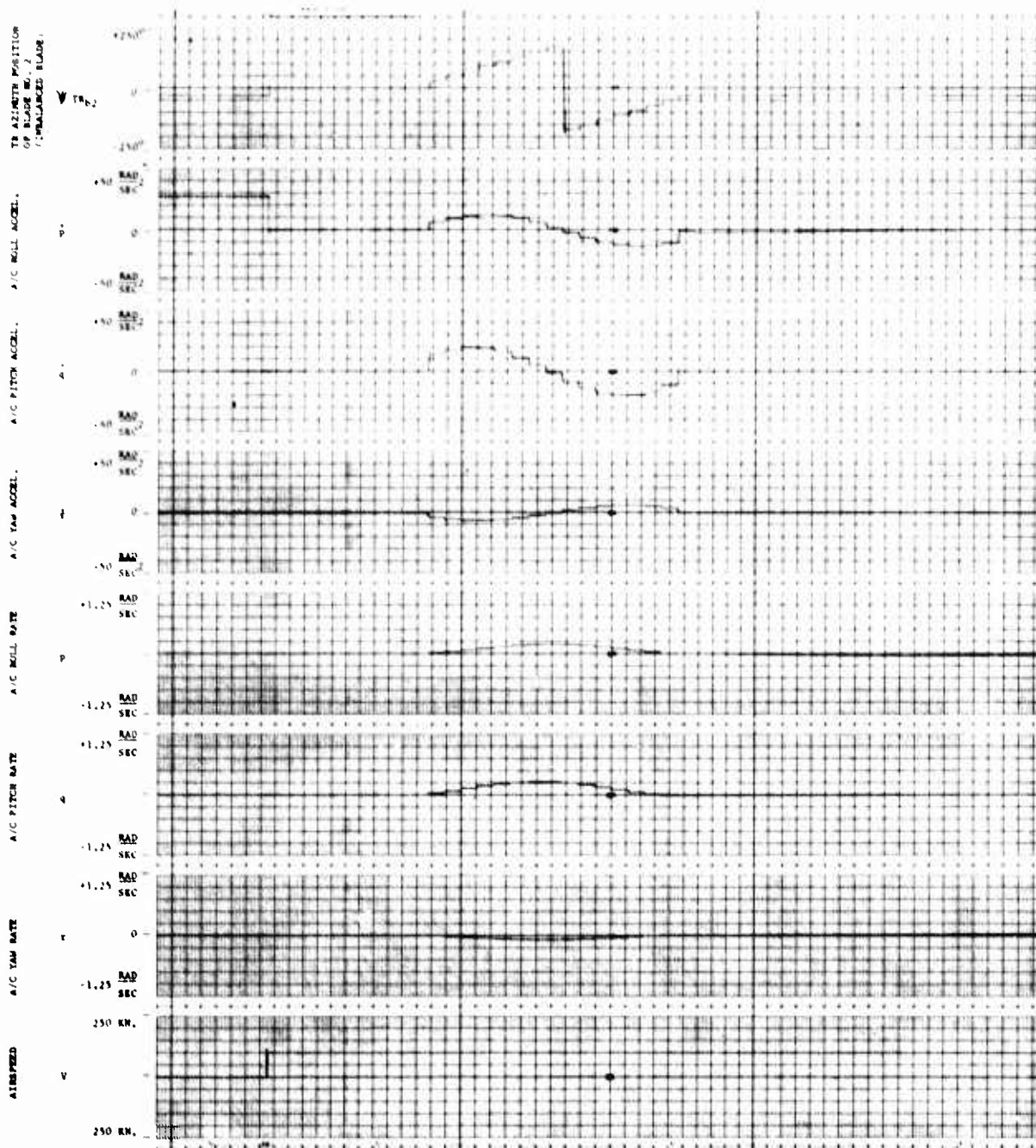


G.W.: 19,900 Lb. FSCG: 360.2 V: 100 Kts  $N_R$ : 100% SAS: OFF  $H_D$ : SLS

Figure D-2. (continued)



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G.W.: 19,900 Lb. FSCG: 360.2 V: 100 Kts  $N_R$ : 100% SAS: OFF  $H_D$ : SLS

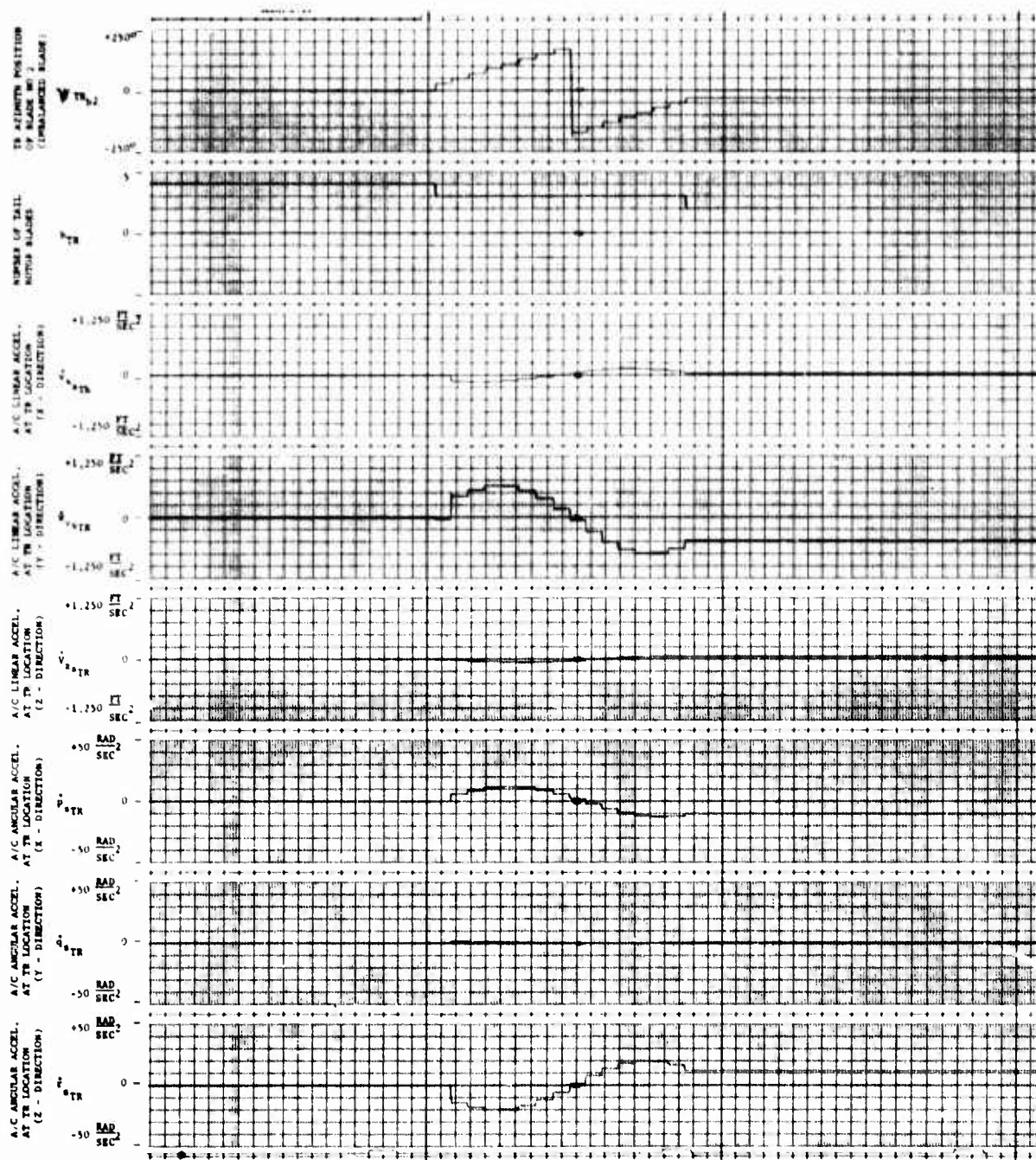
Figure D-2. (continued)

UTTA8(976) 1-21-77 1-DEC-77 RUN 15.

WEIGHT	1980.0	FSCG	360.20000	Y	100.0	PSTIR2	0.0
IX	5000.0	WLCG	245.89999	NELS	-5.0	VSTR.	0.0
IY	48207.0	RMO	0.23700000E-2	VROUND	1117.0	VSTR.	0.0
IZ	30224.0	TIME	0.20000000E-2	DEL3MR	0.0	VSTR.	0.0
OMEGMR	27.0	MBS3	4.0	THSTR	-10.0	PSTR.	0.0
OMEGTR	124.55000	MBS3	5.0	THSTR	-10.0	MLVT	273.0
KFR	1.0	PASCHT	1703.0	MLMT	234.0	FVST	695.0
F8MT	700.40000	8MT	45.0	SVT	32.30000	QSTR.	0.0
LATSTK	-0.06407007	A18	-1.5735975	INT	-1.5307504	XA	44.599507
LNGSTK	0.9744305	A18	9.5056636	IS	-3.0	XB	10.280231
COLSTK	17.360530	THETA0	17.360530	TH75MR	7.2005302	XC	43.053315
PEDAL	10.054176	THETTR	10.920412	TH75TR	5.4204127	XP	52.067596
XAIN	4.4599506	XBIN	1.0200231	XCIN	4.3053314	XPIN	2.0113771
XOACTP	20.540001	XOACTI	2.0540001	RSTR.	0.0	PSTR	0.0
V20	160.47276	THETAB	4.4973503	AAPF	3.9343147	QSTR	0.0
VY0	11.514601	PHI0	0.0	AAIF	-5.6506446	RSTR	0.0
VZ0	13.251071	GETAMP	3.6060210	BBIF	0.10634200	YSTR	0.0
P	0.0	GAMC	0.0	AA0L	-4.7133096	HSTR	0.0
O	0.0	OMGRAT	1.0	AAIL	0.32071001	JSTR	0.0
R	0.0	PSIDOT	0.0	BBIL	0.41096400	HHSTR	0.0
ALFMP	0.71200095	EKTX	1.3770799	EKMPX	0.92773091	LMSTR	0.0
CHITPP	02.133764	EKTZ	1.6437669	EKWFZ	1.0070662	OHSTR	0.0
EKTR	0.0	EP8MT	0.0	8IGHT	0.64073904	XSTR	0.0
QMF	30.100076	KOHT	0.87177979	KOVT	0.03097001	YSTR	0.0
MUX0	0.23310606	CT8IG	0.02561000E-1	LTOT	3.7561543	ZSTR	0.0
MUY0	0.15095140E-1	CH8IG	-0.52370330E-2	DTOT	24.530820	LSTR	0.0
MUZ0	0.60956703E-2	COM8IG	0.63290051E-6	TTR	923.23720	HSTR	0.0
LAMBMR	-0.90077906E-2	NZ	1.0024400	MPMR	1356.5269	NSTR	0.0
DM3MR	0.15103461E-1	VC	0.71525573E-5	KTRBLK	1.0	ASP	2.1252019
XMR	2212.0091	MBAR	-1213.5541	VX0DOT	-0.36712519	AVP	-0.46310006
YMR	-409.79052	JBAR	400.79052	VY0DOT	-0.15210037	AZP	-32.203221
ZMR	-19037.561	TBAR	19120.772	VZ0DOT	-0.17090062	VXP	160.47276
LMR	-0233.4930	LBARM	-2350.6513	P00T	-0.12327064	VYP	11.514601
MHR	2001.7540	MBARM	-15290.609	Q00T	0.03272937E-2	VZP	13.251071
NMR	26793.403	GBAR	27632.956	R00T	0.36313000E-1	RSTR.	0.0
XMP	-010.94060	XT	-22.970491	XTR	0.0	PSIDM6	-150.0
YMP	-300.41143	YT	-179.69472	YTR	0.0	STR	4.0
ZMP	-154.45675	ZT	373.22594	ZTR	-315.70003	MADO	0.0
LMP	567.02501	LT	-399.90400	LTR	5320.9746	XADD	0.0
NMP	-3314.2704	MT	10592.210	MTR	-9704.2216	YADD	0.0
OMP	-3257.7543	NT	5014.3003	NTR	-26001.076	ZADD	0.0
XMT	-12.400400	XVT	-10.530042	ALFMTT	-3.7060076	MADD	0.0
YMT	-1.0171600	YVT	-177.07753	ALFVTT	3.9104095	LADD	0.0
ZMT	372.02590	ZVT	0.39997024	AA0B1P	5.6596437		

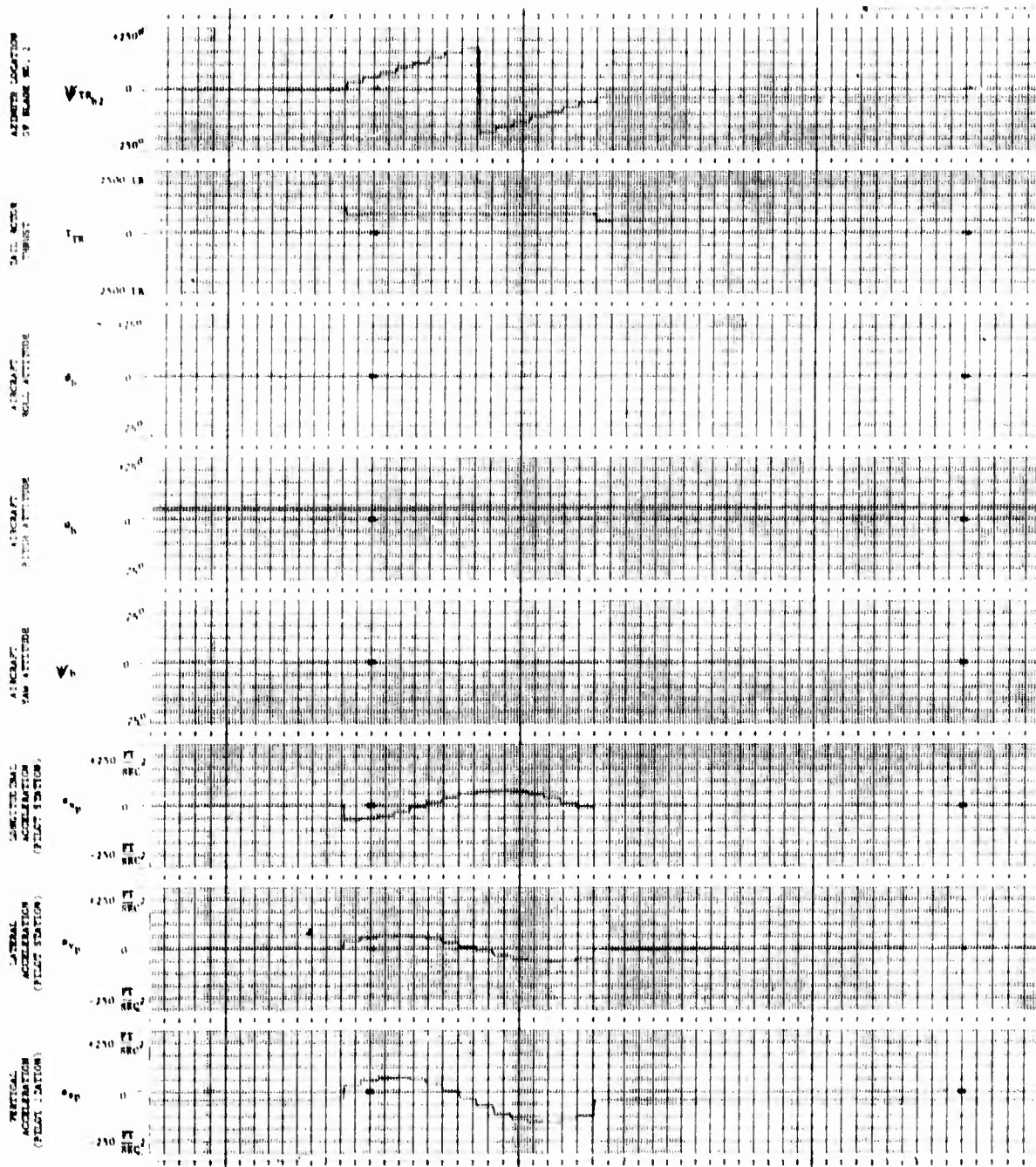
Figure D-2. (continued)





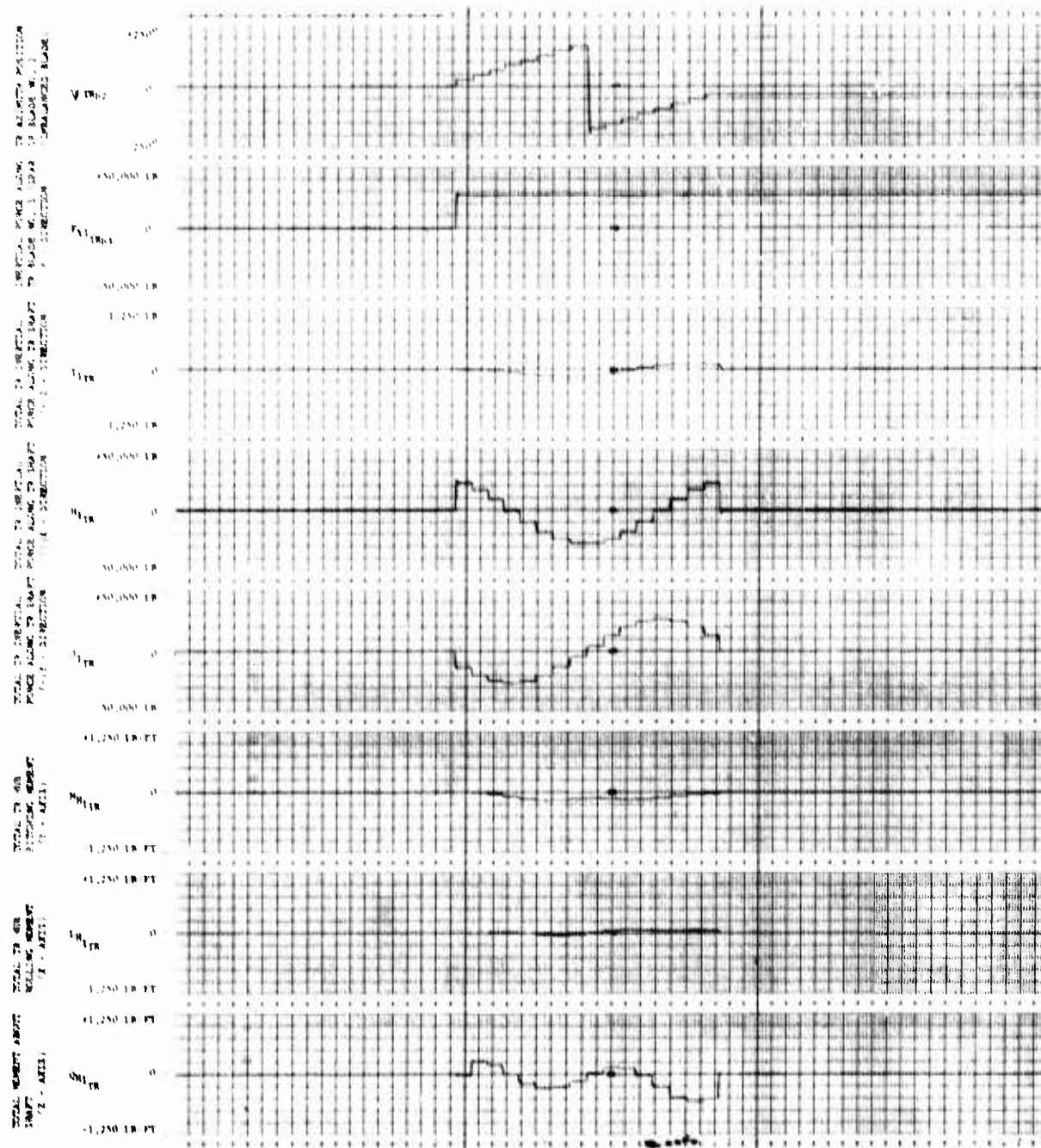
G.W.: 19,900 Lb. FSCG: 360.2 V: 100 Kts  $N_R$ : 100% SAS: OFF  $H_D$ : 10,000 Ft

Figure D-3. Stepped Transition Time History



G.W.: 19,900 Lb. FSCG: 360.2 V: 100 Kts  $N_R$ : 100% SAS: OFF  $H_p$ : 10,000 Ft

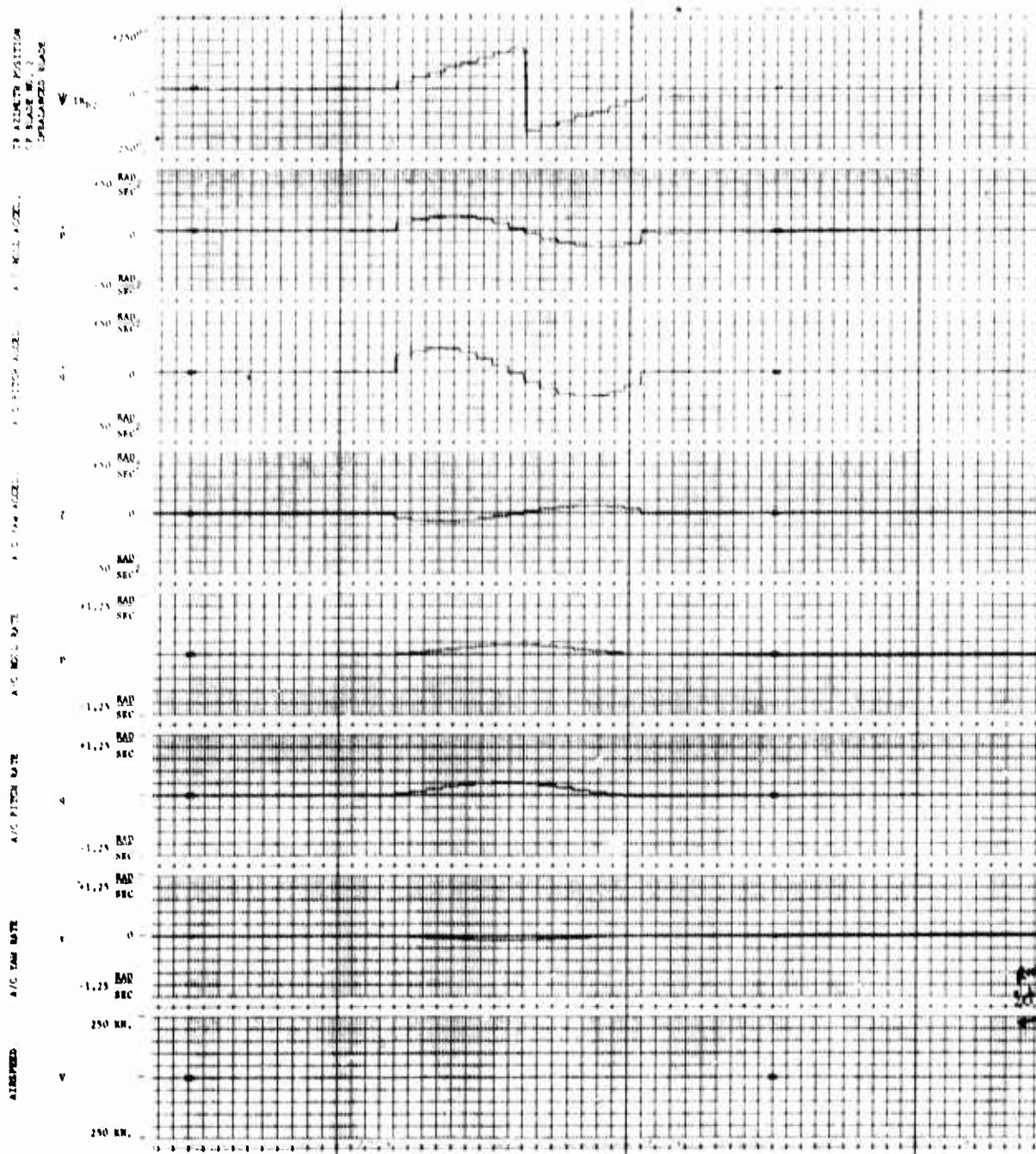
Figure D-3. (continued)



G.W.: 19,900 Lb. FSCG: 360.2 V: 100 Kts  $N_R$ : 100% SAS: OFF  $H_D$ : 10,000 Ft

Figure D-3. (continued)



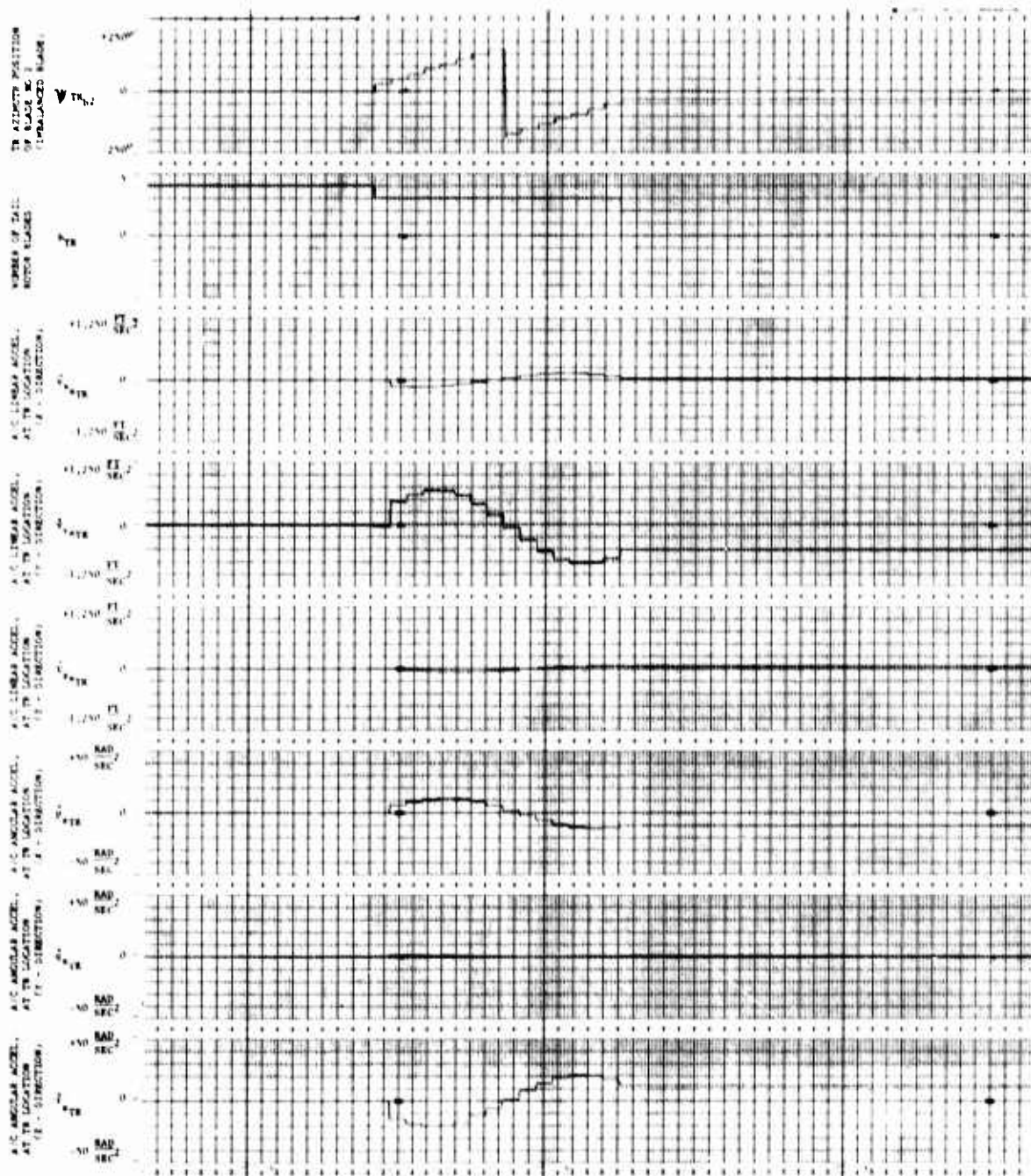


G.W.: 19,900 Lb. FSCG: 360.2 V: 100 Kts  $N_R$ : 100% SAS: OFF  $H_D$ : 10,000 Ft

Figure D-3. (continued)

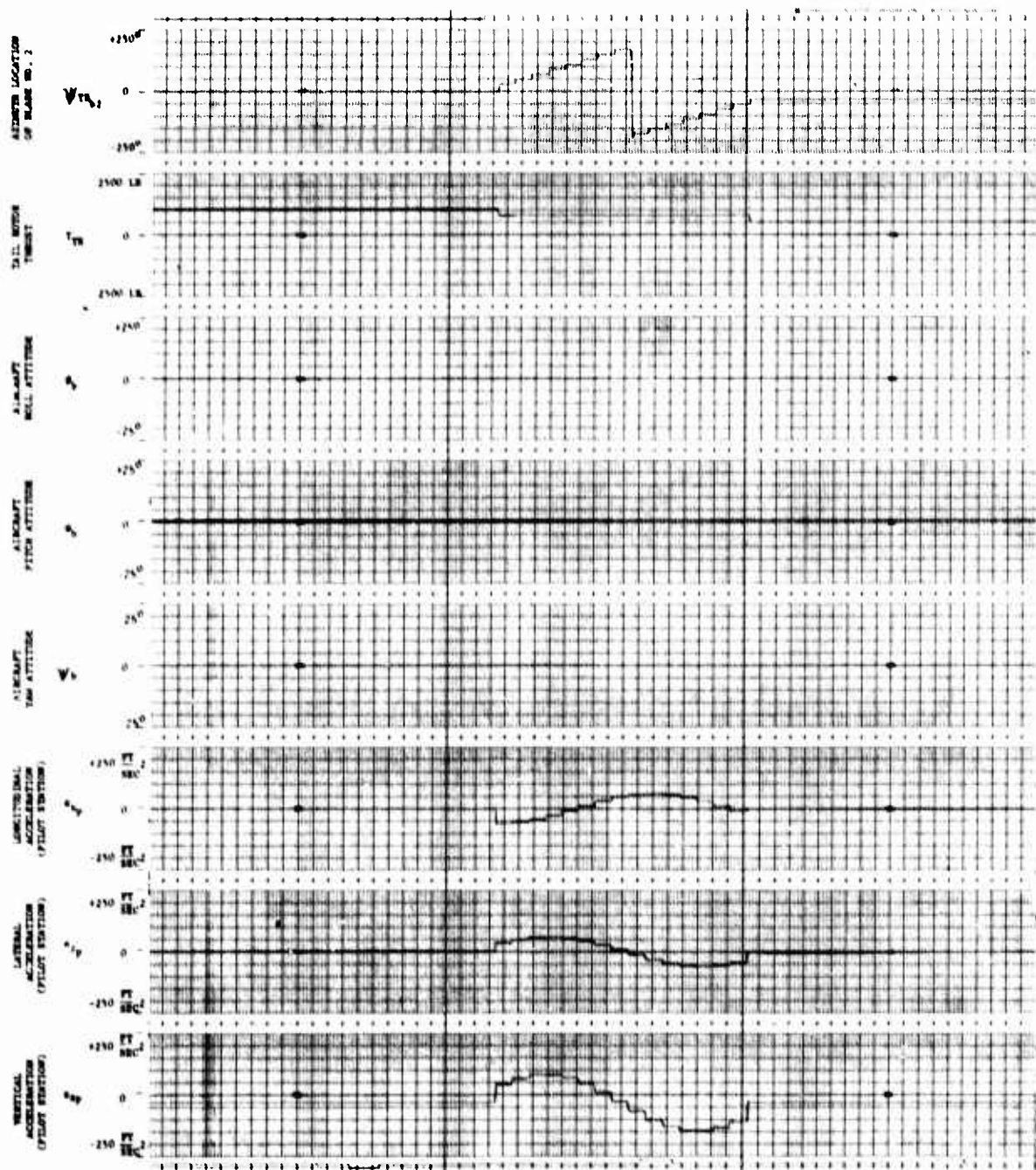
WEIGHT	19908.0	PSCG	368.20800	V	108.0	PSIIR2	0.0
IX	5460.0	WLCG	245.89999	DEL3	-5.0	VX3TR.	0.0
IY	6287.0	RMO	0.1750000E-2	V3OUNO	1077.0	VY3TR.	0.0
IZ	30224.0	TIME	0.2000000E-1	NEL3MR	0.0	VZ3TR.	0.0
OMEGMR	27.0	M883	4.0	TM3TR	-10.0	PSYR.	0.0
OMEGTR	124.55000	M888	5.0	TM3TR	-10.0	WLVT	273.0
FR	1.0	PASCHT	1521.0	WLMT	234.0	FSVT	695.0
FRMT	700.00000	SMT	45.0	SVT	32.30000	GSTR.	0.0
LATSTR	-1.1020375	A18	-2.0265006	IMT	1.9187491	XA	43.11205
LGSTR	8.5065921	Q18	9.6470191	IS	-3.0	XB	19.65000
COLSTR	19.456146	THETAB	19.456146	TH75MR	9.3761466	XC	56.100917
PEDAL	10.92249	THETTR	21.690625	TH75TR	0.1906250	XP	51.310573
XAZM	4.3112265	XBIN	1.9650684	XCIN	5.6100916	XPIN	2.7706989
XMACTP	21.710193	XBACTI	2.1710192	RSTR.	0.0	PSYR	0.0
VIB	160.59004	THETAB	4.0057607	AAOF	4.1269107	GSTR	0.0
VYB	13.600913	PHIB	0.0	AAIP	-4.0621123	RSTR	0.0
VZB	11.007422	DETAMP	4.2713551	BOIP	0.9076707E-1	TITR	0.0
P	0.0	GAMC	0.0	AAOL	-5.2033561	MITR	0.0
R	0.0	OMGRAT	1.0	AAIL	0.36240959	JITR	0.0
ALFAP	-0.92723035	PSIDOT	9.0	BOIL	0.23003240	MMTR	0.0
CHITPP	81.907202	ENTX	1.3271905	EKMF1	0.92503362	LMTR	0.0
ENTX	0.0	ENTZ	1.7010004	EKMF2	1.0000120	OMTR	0.0
QMF	29.300076	EP9MT	0.49271355	SIGMT	0.75175052	XITR	0.0
MU3B	0.2332570	QOMT	0.0717799	KQVT	0.02014002	VITR	0.0
MU3B	0.1070620E-1	CT810	0.11070312	LIOT	1.5950656	ZITR	0.0
MU3B	0.4695460E-2	CH910	-0.09353520E-2	OTOT	24.434270	LITR	0.0
LAMSAR	-0.16123065E-1	COM810	0.09085006E-0	TTR	1000.4570	MITR	0.0
D-3HMR	0.20210534E-1	NZ	0.99454092	MPMR	1377.7843	MITR	0.0
XMR	2176.0520	VC	0.7152573E-5	KTR0L4	1.0	AXP	2.5013309
YMR	-207.92724	MBAR	-1106.5571	VX90OT	0.24350972	AYP	0.66015051
ZMR	-18050.477	JBAR	207.92724	VY80OT	0.29260293	AZP	-31.920054
LPR	-4055.7333	TBAR	10900.002	VZ80OT	0.9984065E-1	VXP	108.50904
MRR	7206.5053	LBARM	-1600.0970	POOT	0.20262970	VYP	13.600913
NRR	27461.506	MBARM	-10046.266	QOOT	-0.59063979E-2	VZP	11.007422
XMP	-694.10202	OBAR	20004.340	ROOT	0.22909250E-0	QSTR.	0.0
YMP	-327.93775	YT	-3.7337091	XTR	0.0	PSIDMG	-150.0
ZMP	-35.500770	YT	-150.60654	YTR	940.19274	STR	4.0
LMP	519.01357	LT	244.23406	ZTR	-342.20203	MAOD	0.0
MMP	-3704.0117	MT	-335.21935	LTR	5774.6957	YADD	0.0
NMP	-2900.5015	NT	6930.9160	MTR	-10002.504	YADD	0.0
XMT	2.0470503	XVT	-5.7011594	ALPMTT	-3.0009157	ZADD	0.0
YMT	-1.5630101	YVT	-149.12312	ALPVT	0.6508703	LADD	0.0
ZMT	243.72009	ZVT	0.50577600	AA001F	4.0613135		

Figure D-3. (continued)



G.W.: 19,900 Lb. FSCG: 347 V: 100 Kts  $N_R$ : 100% SAS: OFF  $H_D$ : 10,000 Ft

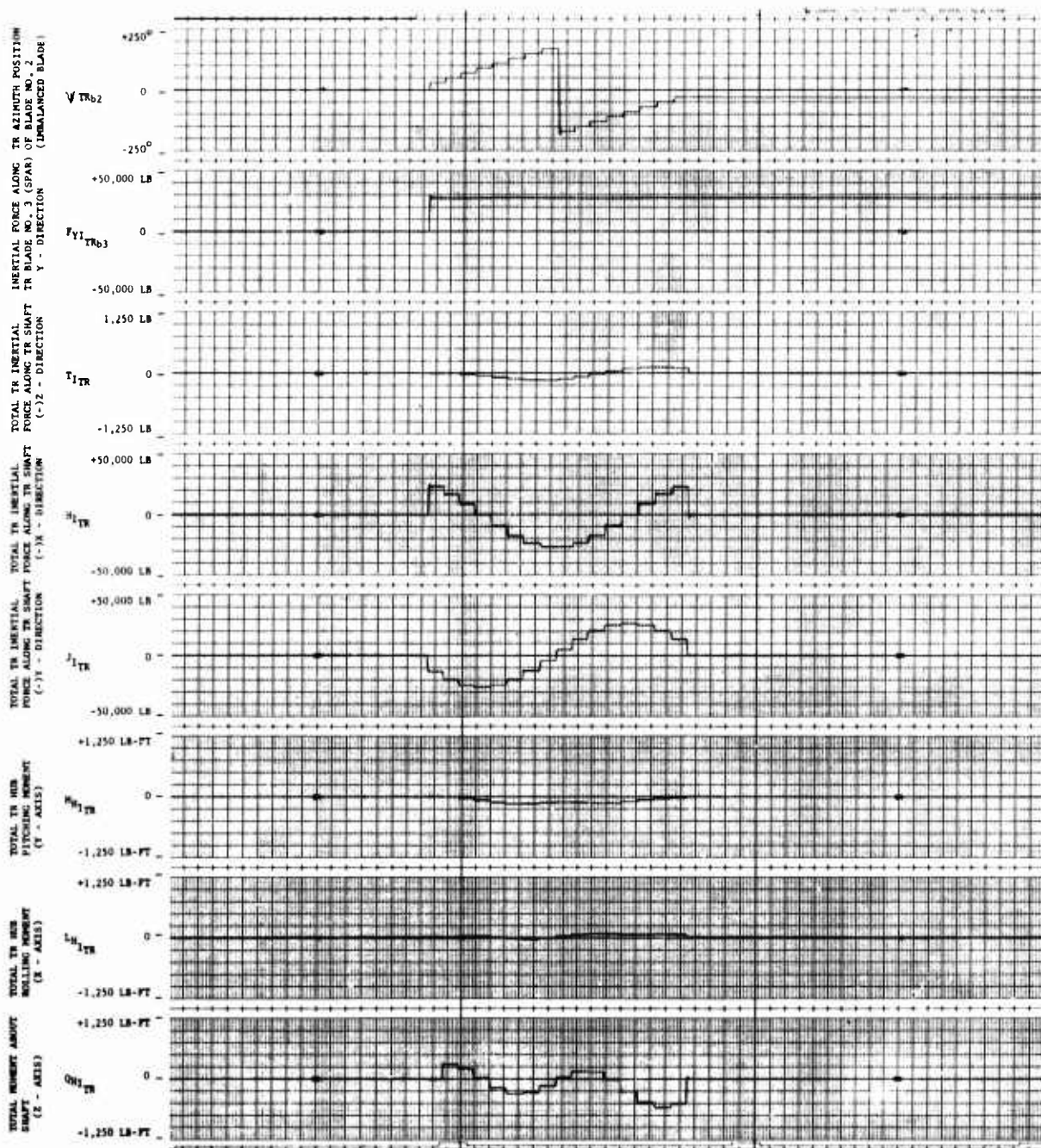
Figure D-4. Stepped Transition Time History



G.W.: 19,900 Lb. FSCG: 347 V: 100 Kts  $N_R$ : 100% SAS: OFF  $H_D$ : 10,000 Ft

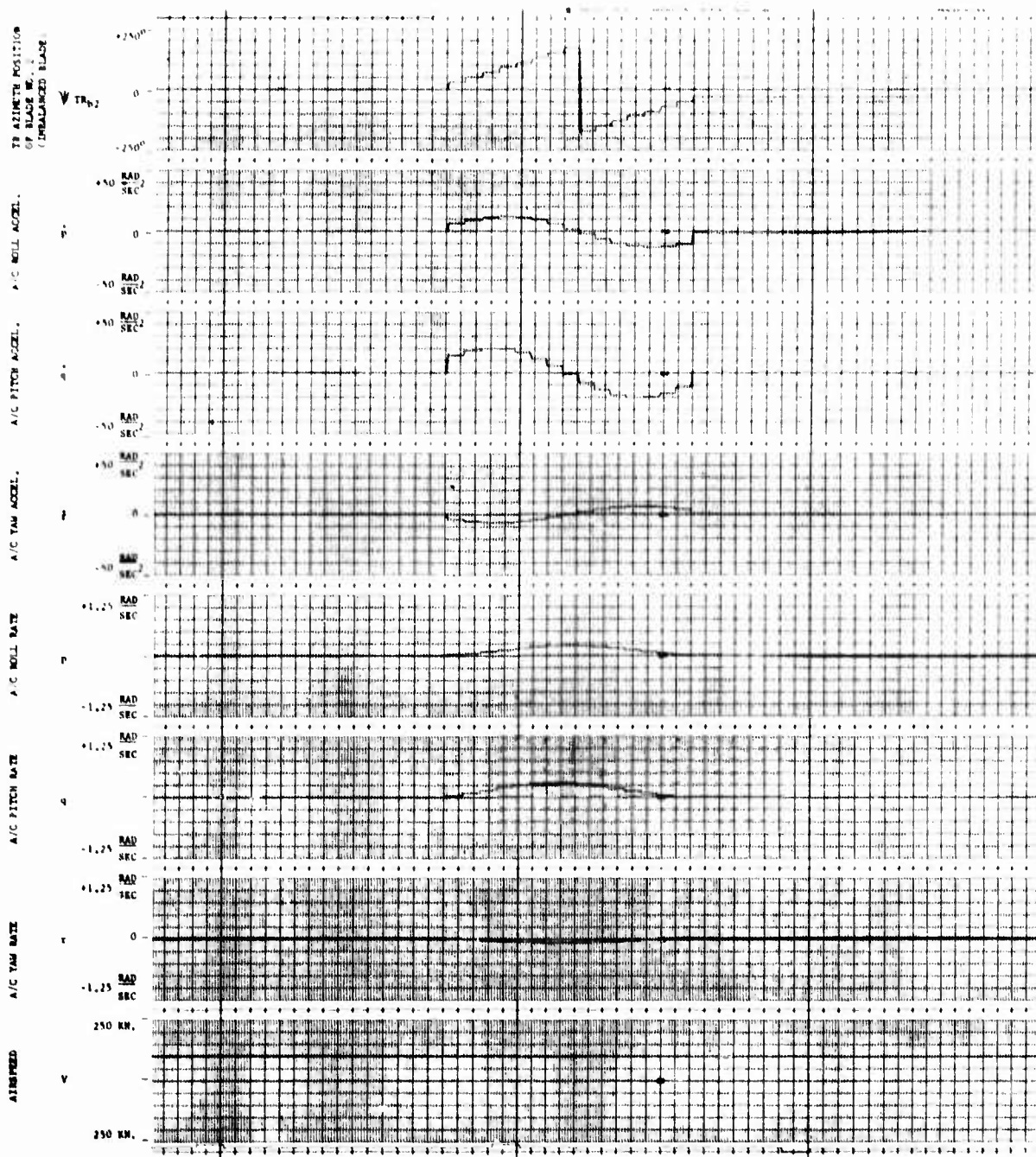
Figure D-4. (continued)





G.W.: 19,900 Lb. FSCG: 347 V: 100 Kts  $N_R$ : 100% SAS: OFF  $H_D$ : 10,000 Ft

Figure D-4. (continued)



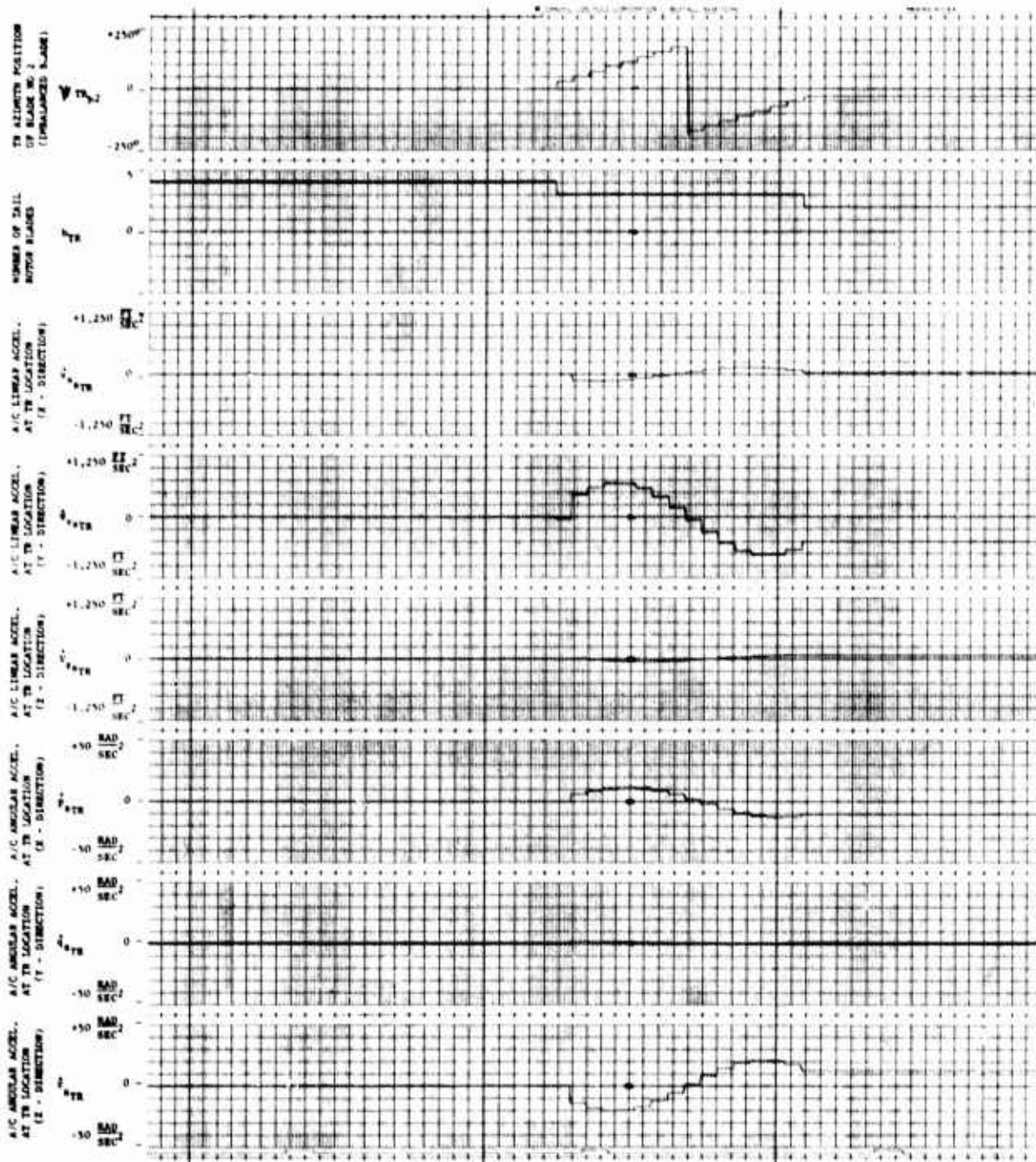
G.W.: 19,900 Lb. FSCG: 347 V: 100 Kts  $N_R$ : 100% SAS: OFF  $H_D$ : 10,000 Ft

Figure D-4. (continued)

UTTA8(S76) 1-21-77 1-DEC-77 RUN 17.

WEIGHT	1988.8	FSCB	347.8	Y	100.0	PSIR2	0.0
IX	548.0	WLCG	245.8999	DEL8	-5.0	VXSTR.	0.0
IY	48287.0	RHO	0.17560000E-2	V3OUND	1077.0	VYSTR.	0.0
IZ	38228.0	TIME	0.20000000E-2	DEL3MR	0.0	VZSTR.	0.0
ONEGMR	27.0	MBSS	4.0	TH3MR	-18.0	PSR.	0.0
ONEGTR	124.55000	MS88	5.0	TH3TTR	-18.0	WLVT	273.0
KFR	1.8	PASCNT	1223.8	WLMT	234.0	F3VT	695.0
FSMT	788.48000	SWT	45.0	SVT	32.38000	OSTR.	0.0
LAT8TK	-1.8498328	A18	-1.9940652	IHT	2.4679198	XA	43.430549
LM8TK	5.5083264	B18	6.4841892	IS	-3.0	XB	30.394883
COL8TK	19.647312	THETA8	19.647312	TH75MR	9.5673125	XC	57.295783
PEDAL	11.142235	THETTR	22.143010	TH75TR	0.6430100	XP	58.715082
XAIN	4.3438549	XBIN	3.9324683	XCIN	5.7295783	XPIN	2.7385162
X8ACTP	31.265986	X8ACTI	3.1265986	RSTR.	0.0	PSR	0.0
V18	168.95861	THETAB	0.91977100	AADF	4.2184171	OSTR	0.0
VY8	12.142984	PHIB	0.0	AAIF	-0.7403638	RSTR	0.0
VZ8	2.7126448	RETAMP	3.7894253	B8IF	0.2508135	TITR	0.0
P	0.0	GMC	0.0	AA8L	-5.3677839	MITR	0.0
Q	0.0	MGCRAT	1.0	AA1L	0.26823933	JITR	0.0
R	0.0	PSIDOT	0.0	B81L	-0.7803881E-1	MMTR	0.0
ALPFP	-3.8646721	EKTX	1.1919474	EKMFX	8.9276888	LMTR	0.0
CHITPP	82.129878	EKYZ	1.8475477	EKMZ	1.8475477	OMTR	0.0
EKTR	0.0	EPAT	0.40789425	8IGHT	0.66693007	XITR	0.0
QF	29.811737	KQMT	0.87177979	KQVT	0.83847251	YITR	0.0
MU18	0.23389438	CT8IG	0.11361789	LYOT	-2.1218364	ZITR	0.0
MU28	0.16762585E-1	CH8IG	0.79523682E-3	OTOT	24.337884	LITR	0.0
MU38	-0.84678658E-2	COH8IG	0.91898559E-6	TTR	1823.8982	MITR	0.0
LAN8MR	-0.29185843E-1	NZ	1.8834618	MPMR	1453.5976	NITR	0.0
DASHMR	0.28034779E-1	VC	0.17881393E-5	KTR8LK	1.8	AXP	0.38496639
XMR	881.85279	MBAR	136.85566	VX8DOT	-0.13622488	AYP	-0.18368821
YMR	-572.32478	JBAR	572.32478	VY8DOT	-0.72858371E-1	AZP	-32.319692
ZMR	-19417.656	TBAR	19438.683	VZ8DOT	-0.11923628	VXP	168.95861
LMR	-6461.7279	LBARM	-1478.3947	POOT	-0.68248899E-1	VYP	12.142984
MHR	2598.4241	MBARM	-1982.3948	GOOT	-0.2111815E-2	VZP	2.7126448
MHR	29281.688	QBARM	29618.322	ROOT	-0.2893114E-2	RSTR.	0.0
XMF	-695.96969	XT	81.882624	XTR	0.0	PS10MG	-158.0
YMF	-293.96351	YT	-139.15789	YTR	962.22113	BTR	4.0
ZMF	118.87737	ZT	583.73477	ZTR	-358.22833	MADD	0.0
LMF	512.44532	LT	-387.22547	LTR	5989.9948	XADD	0.0
MYF	-6337.6183	MT	14898.347	MTR	-11236.241	YADD	0.0
NMF	-2381.8253	NT	4836.5537	NTR	-38871.268	ZADD	0.0
XMT	88.195748	XVT	-7.1131234	ALPMTT	-6.4887253	NADD	0.0
YMT	-2.1859858	YVT	-136.99191	ALFVTT	4.1478971	LADD	0.0
ZMT	582.62489	ZVT	1.18988814	AA88IF	0.78984469		

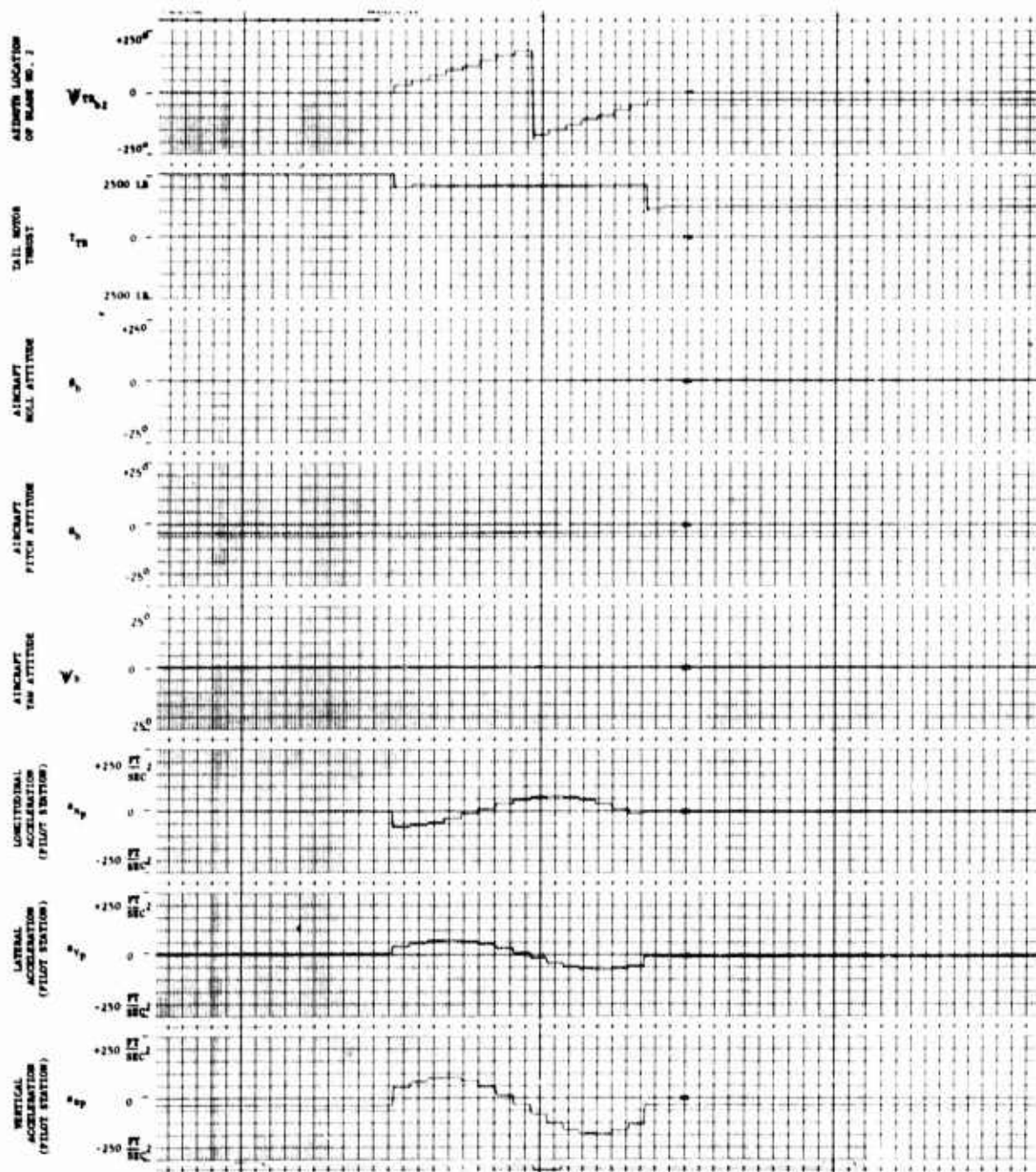
Figure D-4. (continued)



G.W.: 19,900 Lb. FSCG: 347 V: 150 Kts  $N_R$ : 100% SAS: OFF  $H_D$ : 10,000 Ft

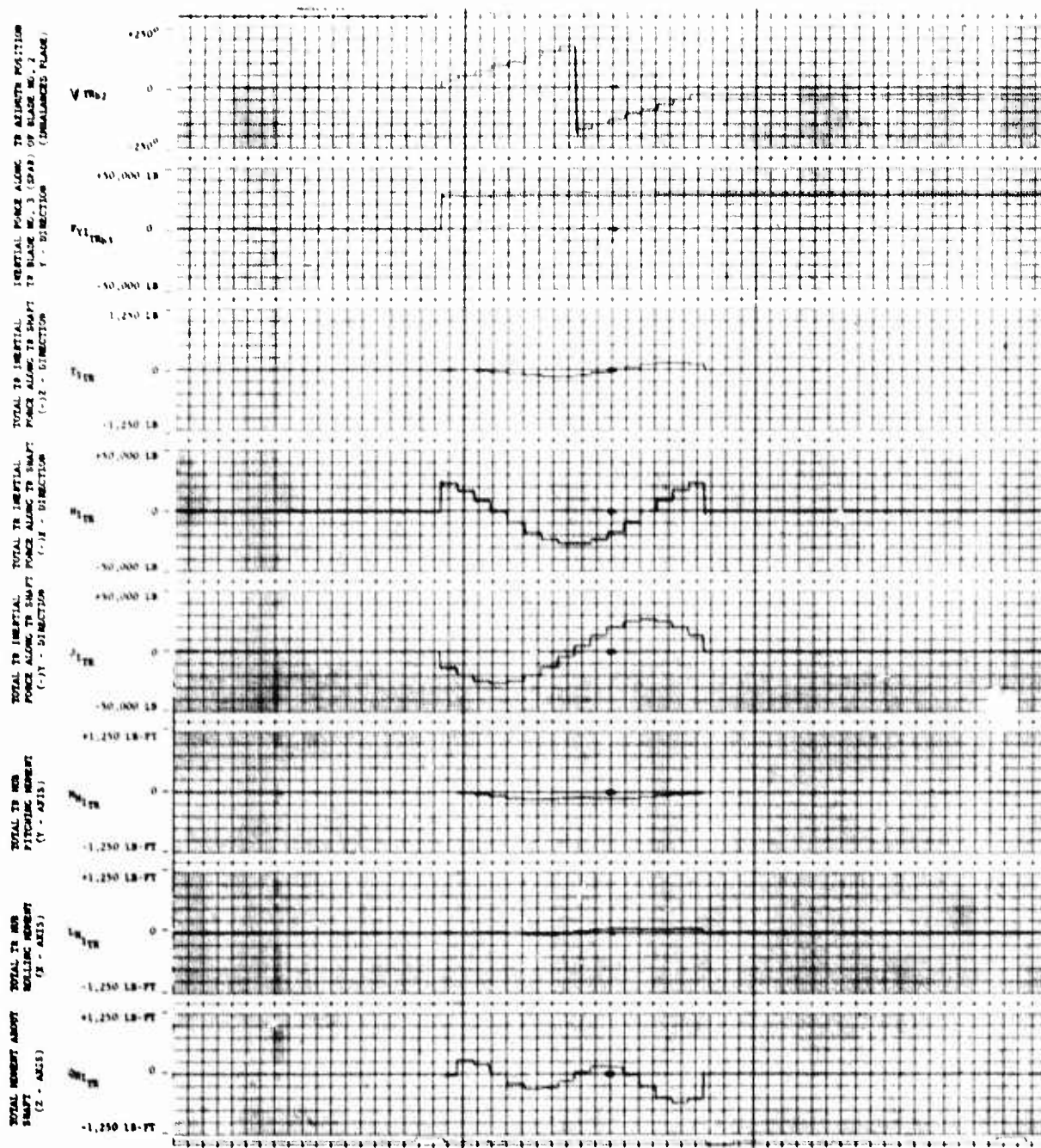
Figure D-5. Stepped Transition Time History





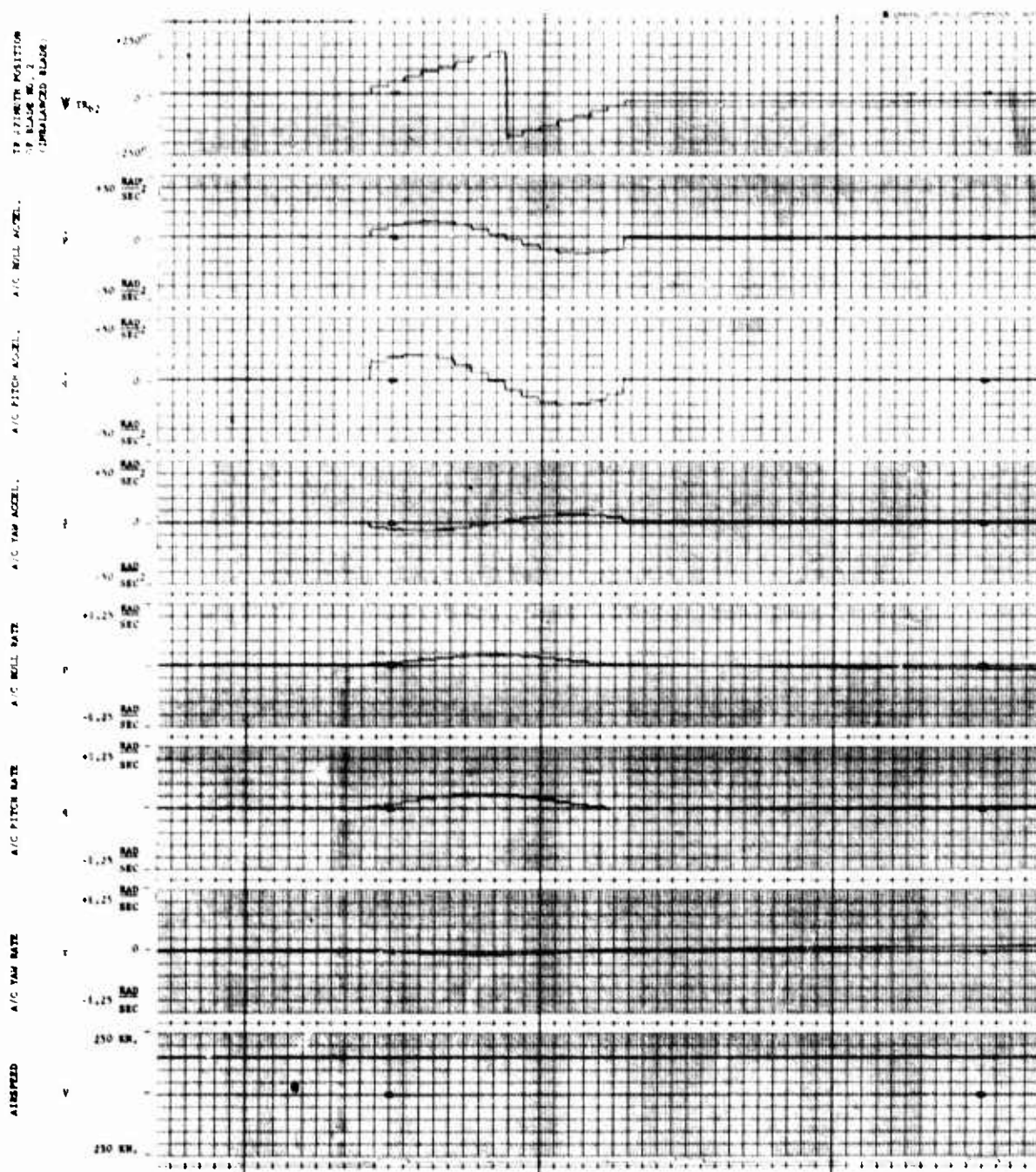
G.W.: 19,900 Lb. FSCG: 347 V: 150 Kts  $N_R$ : 100% SAS: OFF  $H_D$ : 10,000 Ft

Figure D-5. (continued)



G.W.: 19,900 Lb. FSCG: 347 V: 150 Kts  $N_R$ : 100% SAS: OFF  $H_D$ : 10,000 Ft

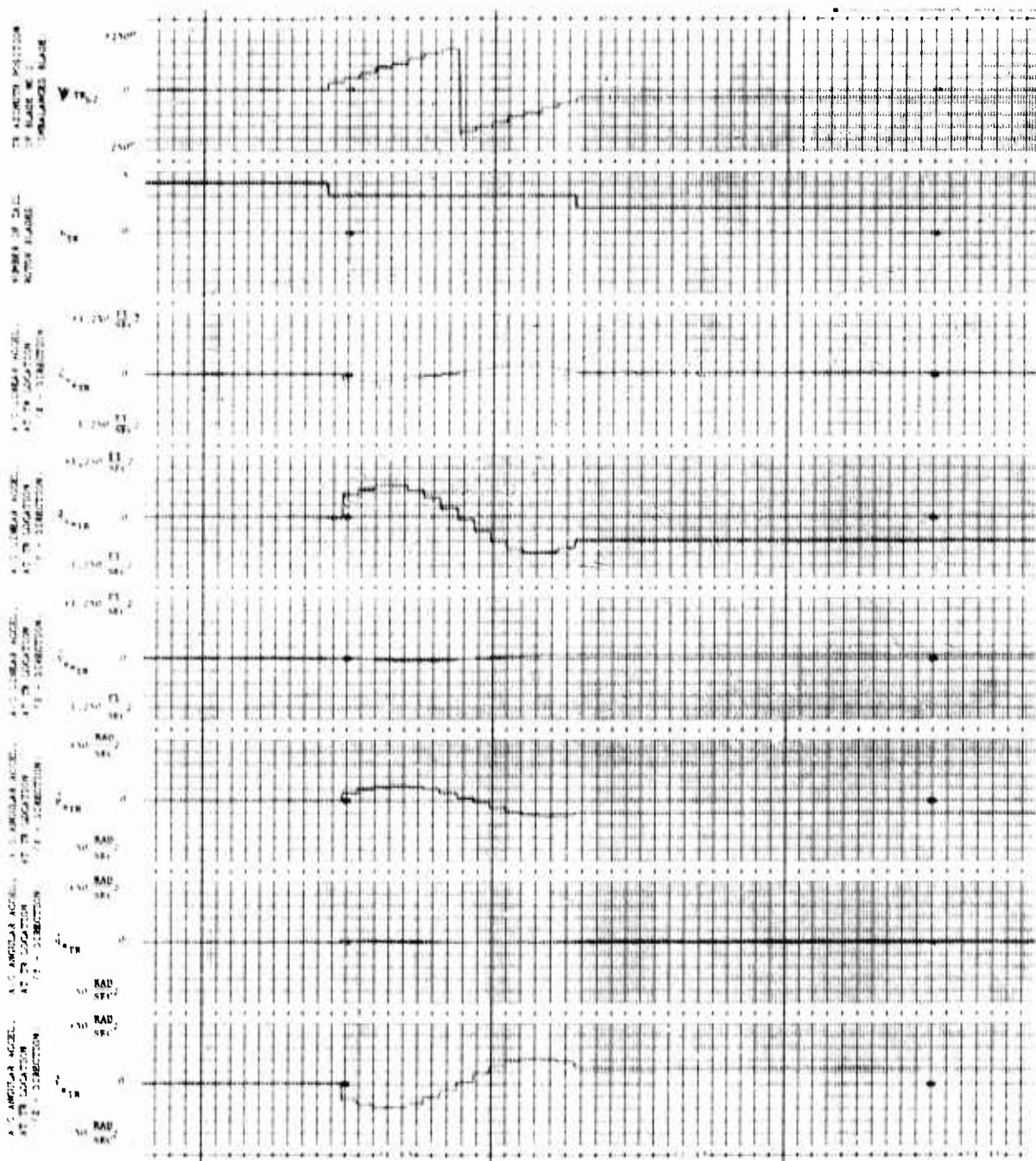
Figure D-5. (continued)



G.W.: 19,900 Lb. FSCG: 347 V: 150 Kts  $N_R$ : 100% SAS: OFF  $H_D$  10,000 Ft

Figure D-5. (continued)

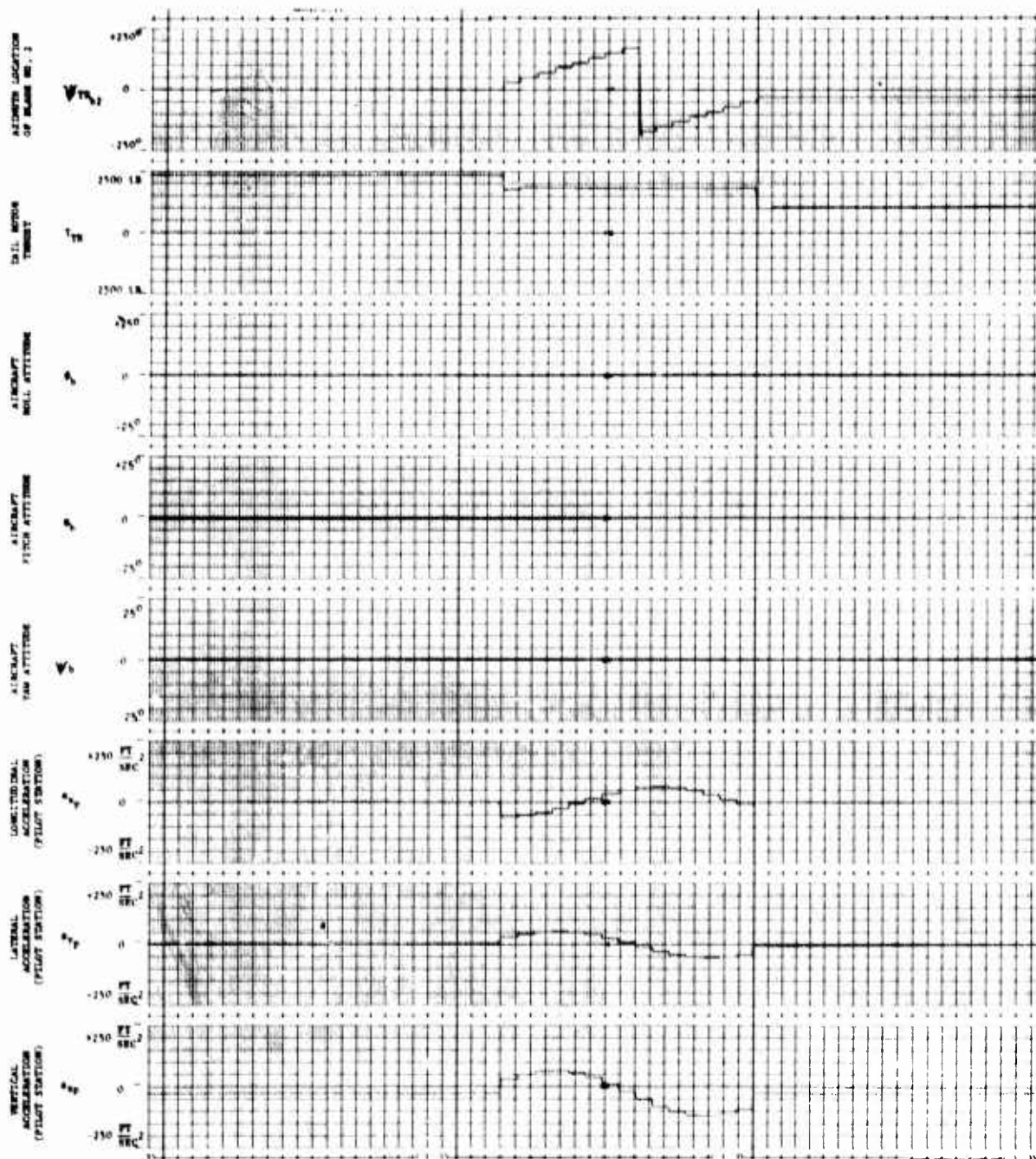




G.W.: 19,900 Lb. FSCG: 360.2 V: 150 Kts  $N_R$ : 100% SAS: ON  $H_0$ : 10,000 Ft

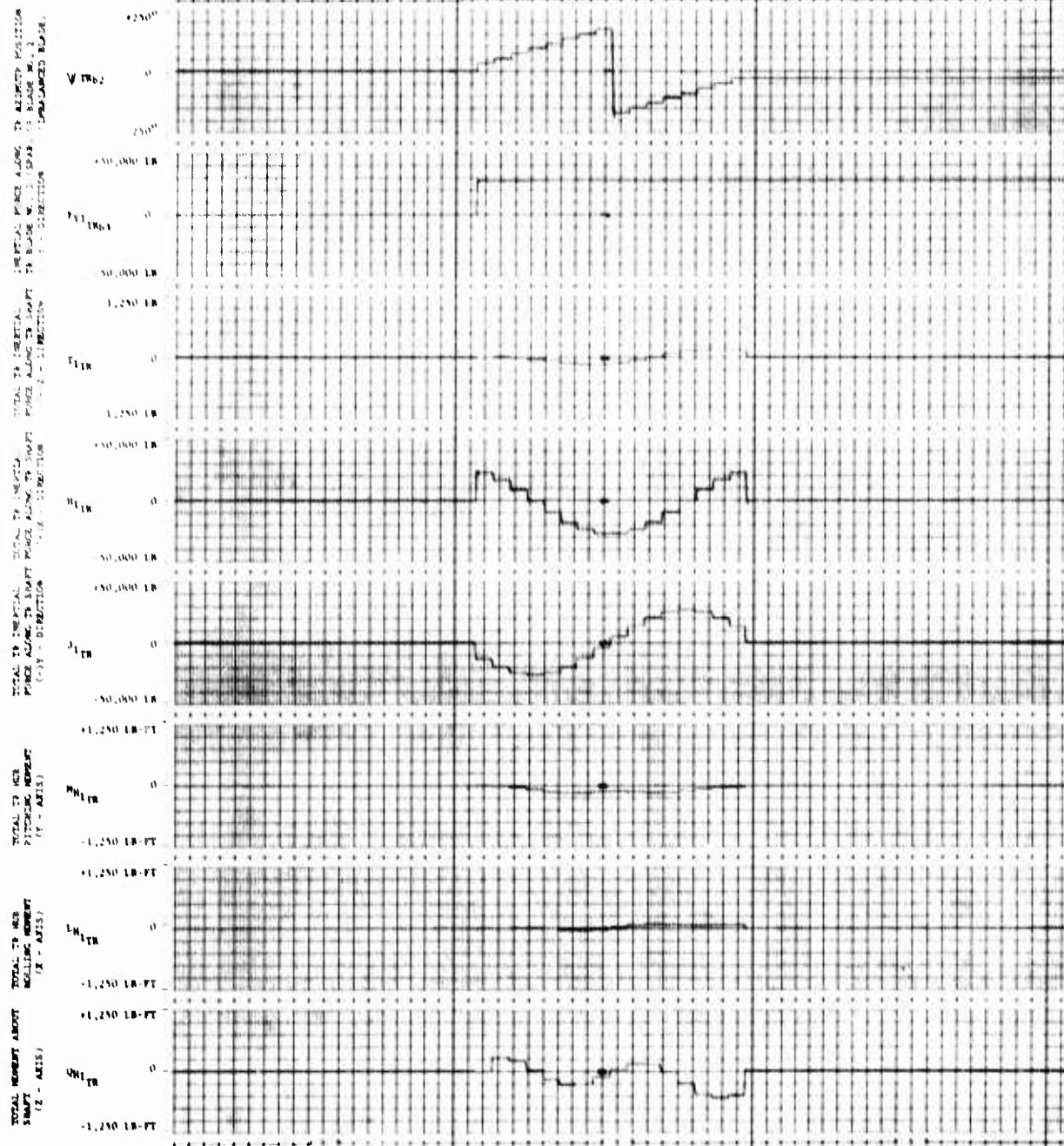
Figure D-6. Stepped Transition Time History





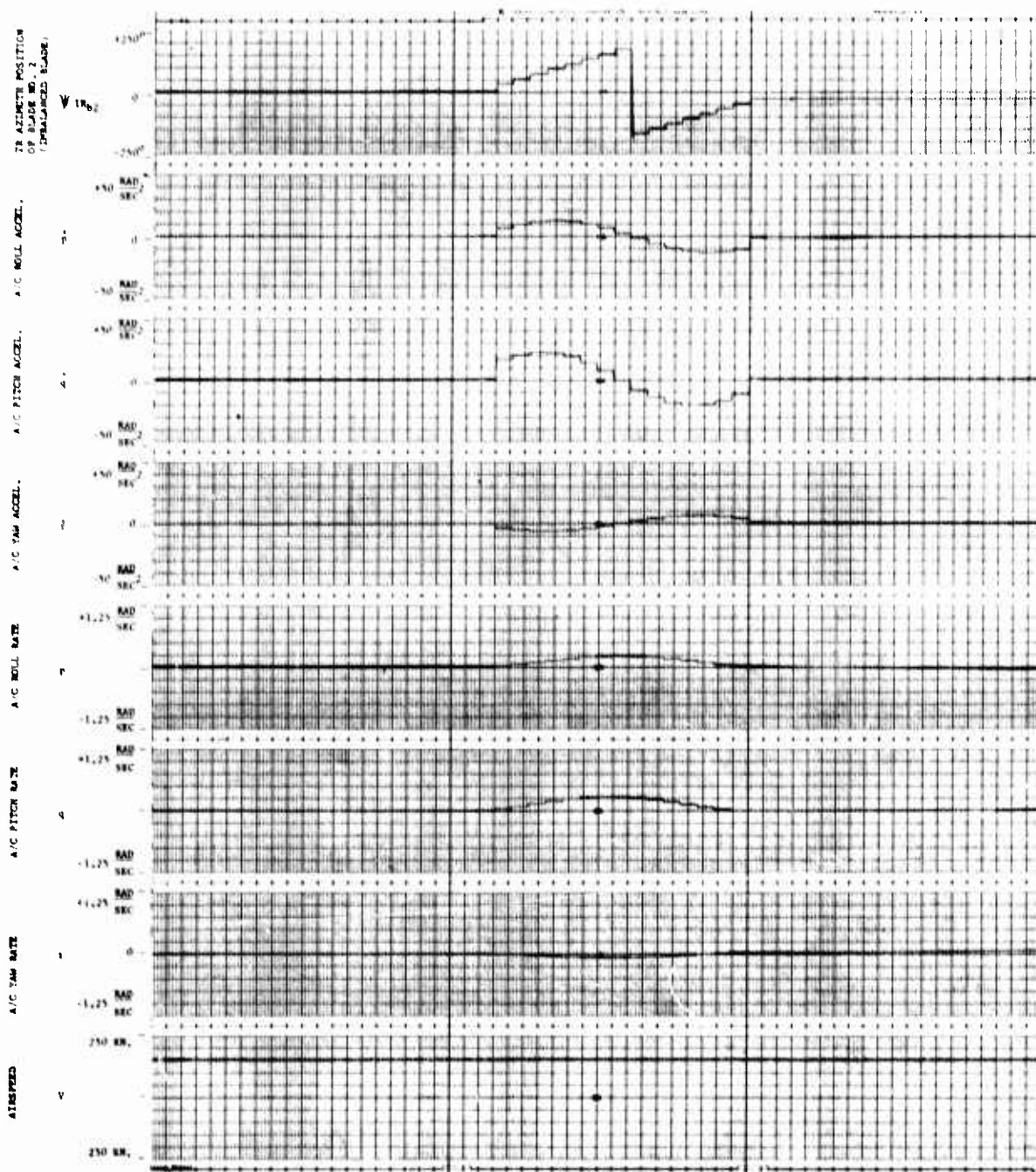
G.W.: 19,900 Lb. FSCG: 360.2 V: 150 Kts  $N_R$ : 100% SAS: ON  $H_D$ : 10,000 Ft

Figure D-6. (continued)



G.W.: 19,900 Lb. FSCG: 360.2 V: 150 Kts  $N_R$ : 100% SAS: ON  $H_D$ : 10,000 Ft

Figure D-6. (continued)



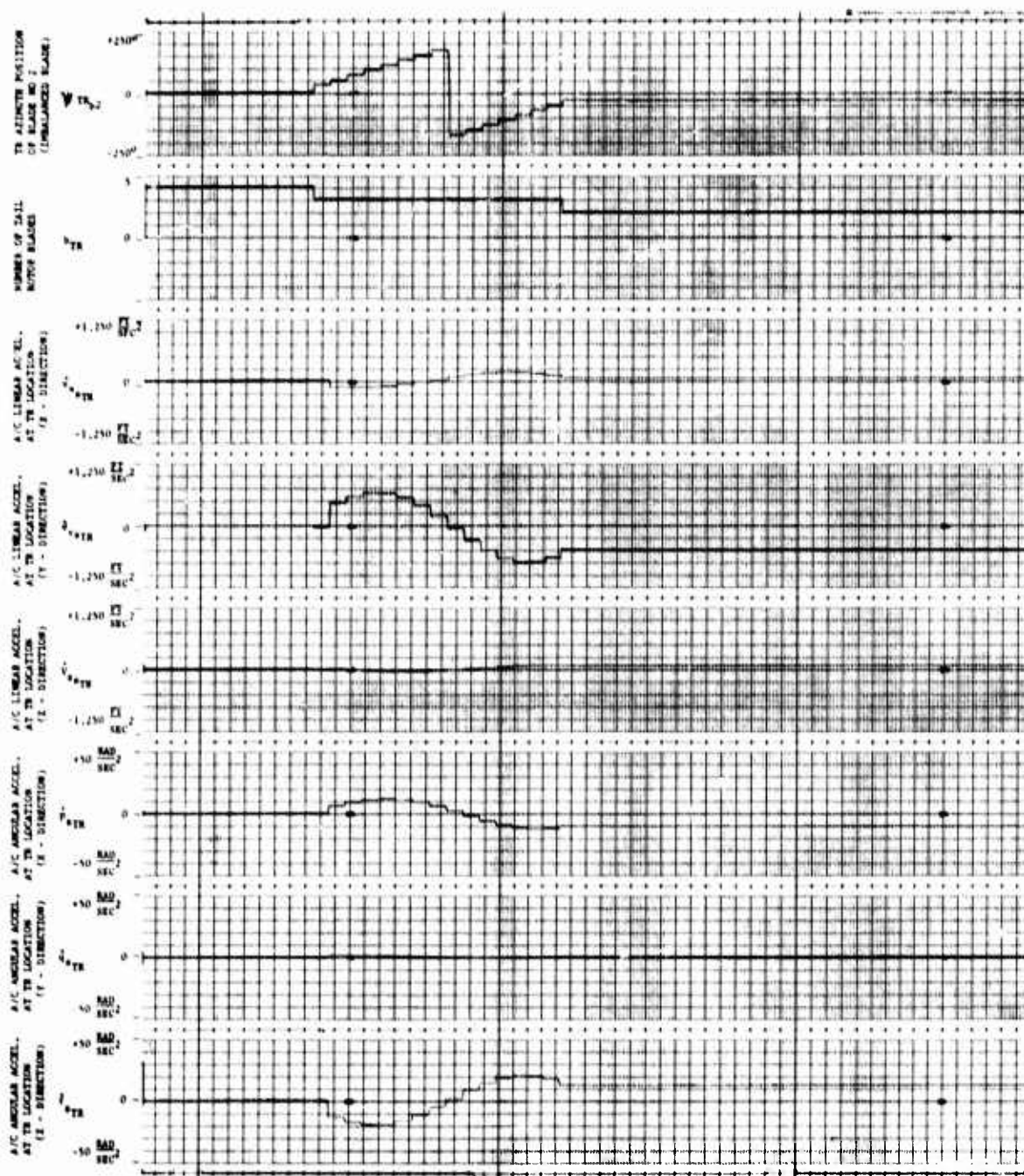
G.W.: 19,900 Lb. FSCG: 360.2 V: 150 Kts  $N_R$ : 100% SAS: ON  $H_D$ : 10,000 Ft

Figure D-6. (continued)



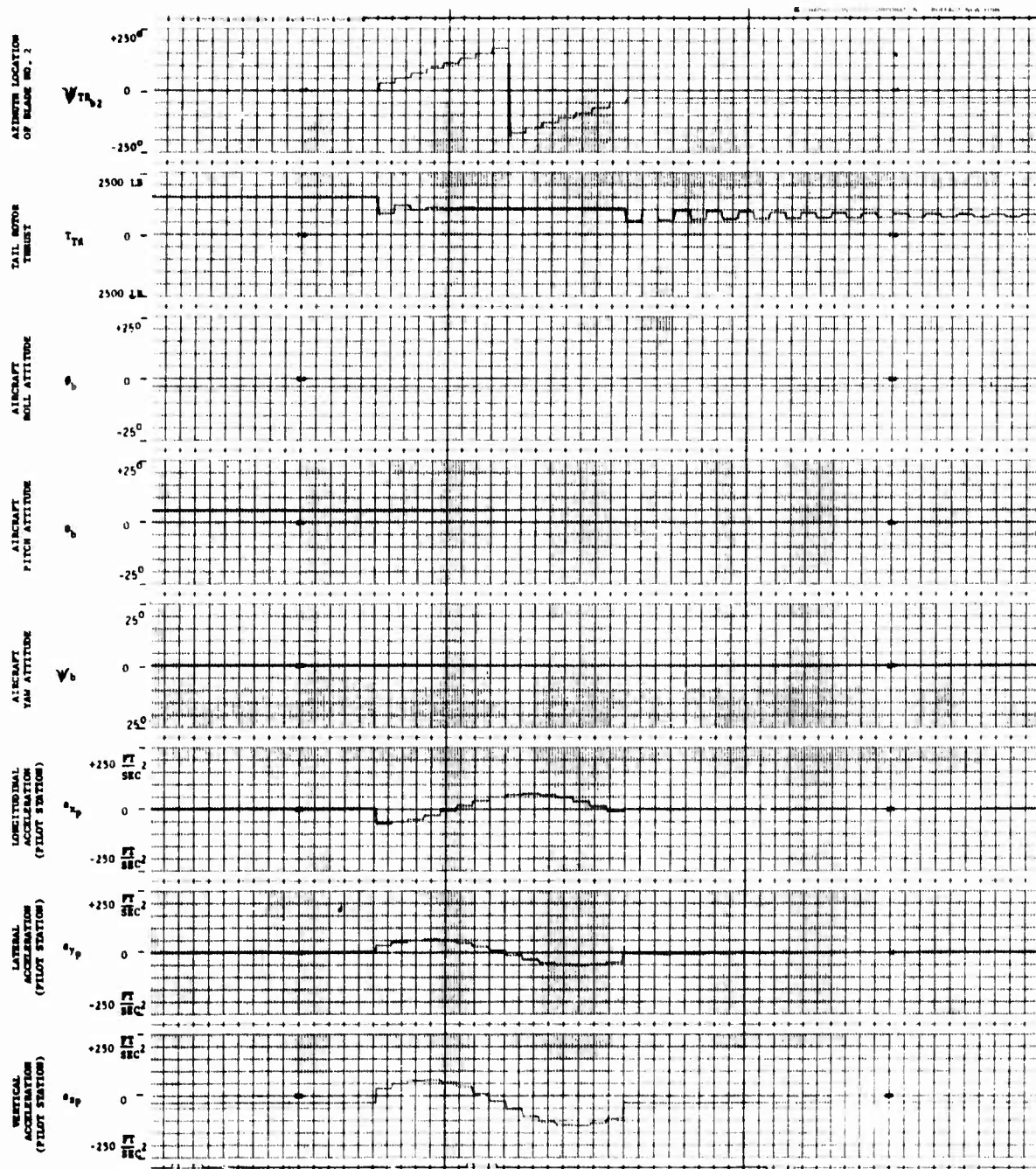
WEIGHT	19000.0	FSCG	308.20000	V	158.0	PSITR2	0.0
IX	5460.0	WLCG	245.89999	DELS	-5.0	VXSTR.	0.0
IY	40207.0	RMO	0.17560000E-2	VBOUND	1877.0	VYSTR.	0.0
IZ	30224.0	TIME	0.20000000E-1	DEL3MR	0.0	VZSTR.	0.0
ONEGMR	27.0	NBS	4.0	THSTR	-10.0	PSTR.	0.0
ONEGTR	124.55000	NBS	5.0	THSTR	-10.0	MLVT	273.0
KFR	15.0	PASCNT	2163.0	MLMT	234.0	PSVT	695.0
PSMT	781.0000	SMT	45.0	SVT	32.300000	OSTR.	0.0
LATSTR	-3.2616592	AIS	-4.6536977	INT	0.48970681	XA	29.61630
LANGTR	12.309170	RIS	14.058177	IS	-3.0	XB	6.2219004
COLSTR	23.994937	THETAB	23.994937	TH75MR	13.914937	XC	84.460359
PEDAL	13.462016	THETTR	29.600741	TH75TR	16.100741	XP	44.201391
XAIN	2.0614630	XBIN	0.62219044	XCIN	0.4460359	XPIN	2.3911329
XBACTP	3.0401503	XBACTI	0.30401503	RSTR.	0.0	PSTR	0.0
VXB	253.49214	THETAB	-0.11624517	AARF	4.0502146	OSTR	0.0
VYB	10.554529	PHIB	0.0	AAIF	-3.5159040	RSTR	0.0
VZB	-0.51425602	BTAPF	4.0384603	BBIF	-0.2060620	YSTR	0.0
P	0.0	GAMC	0.0	AABL	-11.633179	MSTR	0.0
Q	0.0	OMGRAT	1.0	AAIL	0.60304245	JSTR	0.0
ALFWF	-2.2709302	PSIDOT	0.0	BBIL	0.10593356	MMSTR	0.0
CHITPP	01.144775	EKTZ	1.7410915	EKWPX	0.91400205	LMSTR	0.0
EKTH	0.0	EPST	0.49030460	EKWPZ	1.0000552	OMSTR	0.0
OMF	60.986020	KOMT	0.07177979	SIGMT	0.71077016	YSTR	0.0
MUXS	0.34930521	CTSIG	0.11199662	KOVT	0.82927212	VSTR	0.0
MUYB	0.25613297E-1	CHSIG	-0.22562351E-2	LTOT	-0.11933051	ZSTR	0.0
MUZB	-0.19022109E-1	COMSIG	0.00400535E-6	OTOT	24.307693	LSTR	0.0
LAMBMR	-0.32642170E-1	NZ	1.0009700	YTR	2205.3241	MSTR	0.0
DASHMR	0.13619901E-1	VC	0.0946967E-6	MPMR	3100.9015	NSTR	0.0
XMP	1300.2511	MBAR	-306.01527	KTRBLK	1.0	AXP	-0.80669713E-1
YMR	-1135.7705	JBAR	1135.7705	VXBOOT	-0.29649001E-1	AYP	-0.82419063E-1
ZMR	-19113.355	TBAR	19161.305	VYBOOT	-0.35520690E-1	AZP	-32.225004
LMR	-13247.705	LBARM	-3119.5030	VZBOOT	-0.32233096E-1	VXP	253.49214
MMR	13018.403	MBARM	-9005.6962	PDOT	-0.27609234E-1	VYP	14.554529
NMR	61199.609	QBARM	63329.476	ODOT	-0.33457210E-2	VZP	-0.51425602
MMF	-1042.2283	YT	-2.3355596	ROOT	-0.16490667E-2	RSTR.	0.0
VMF	-604.44637	YT	-313.32935	XTR	0.0	PSIDMG	-50.0
ZMF	64.703925	ZT	696.36215	YTR	2072.4809	BTR	4.0
LMF	1067.7641	LT	-696.02751	ZTR	-754.32203	MADD	0.0
MMF	-10364.225	MT	19790.460	LTR	12729.248	XADD	0.0
NMF	-5729.8571	MT	8743.3000	MTR	-23371.435	YADD	0.0
XMT	13.517461	XVT	-15.053020	NTR	-64212.347	ZADD	0.0
YMT	-3.3152666	YVT	-310.01400	ALPHYT	-4.4300439	MADD	0.0
ZMT	695.01844	ZVT	1.3437000	ALPVT	4.1915000	LADD	0.0
				AABIF	3.5220196		

Figure D-6. (continued)



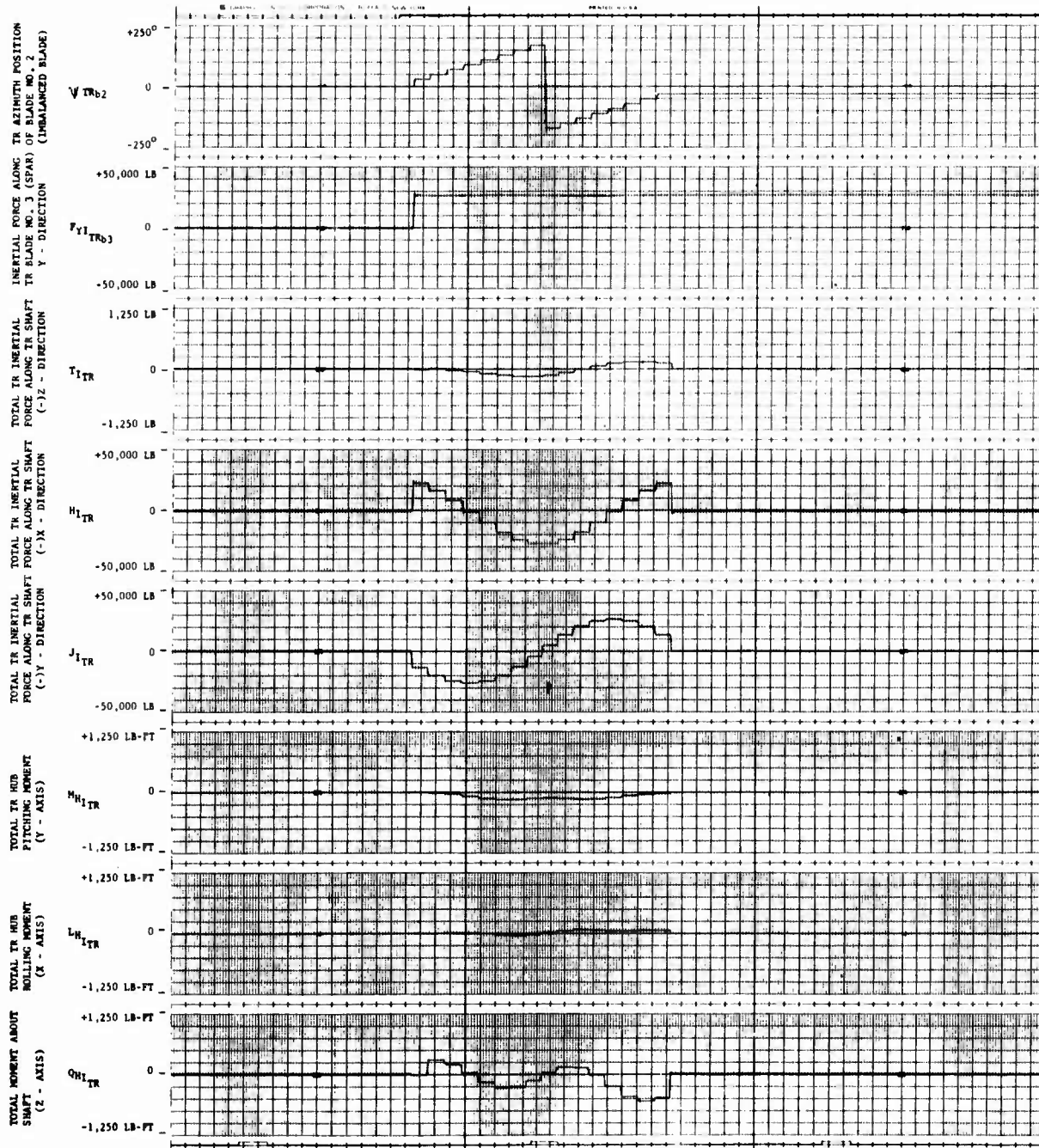
G.W.: 19,900 Lb. FSCG: 360.2 V: Hover  $N_R$ : 100% SAS: OFF  $H_D$ : 10,000 Ft

Figure D-7. Stepped Transition Time History



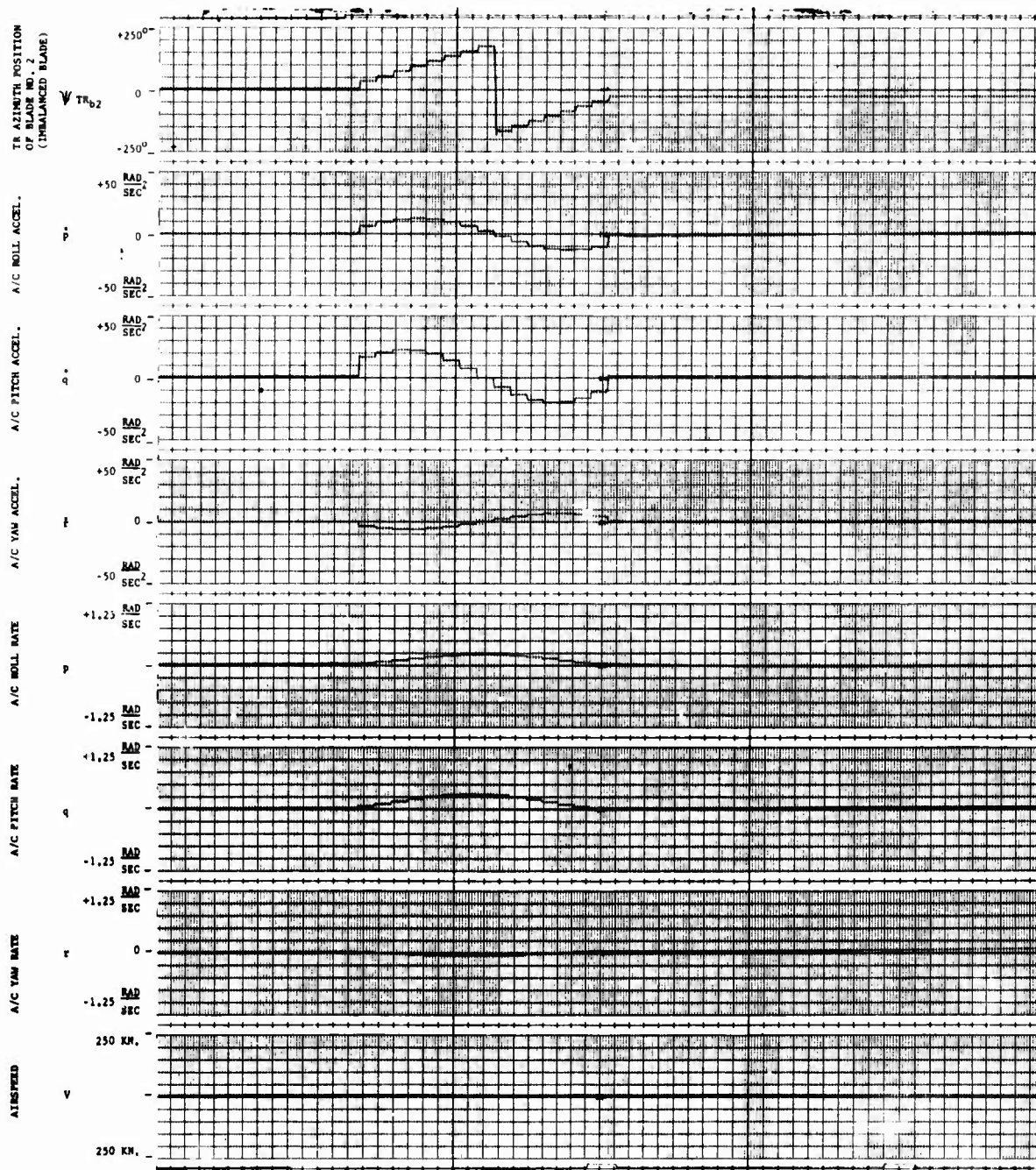
G.W.: 19,900 Lb. FSCG: 360.2 V: Hover  $N_R$ : 100% SAS: OFF  $H_D$ : 10,000 Ft

Figure D-7. (continued)



G.W.: 19,900 Lb. FSCG: 360.2 V: Hover  $N_R$ : 100% SAS: OFF  $H_D$ : 10,000 Ft

Figure D-7. (continued)



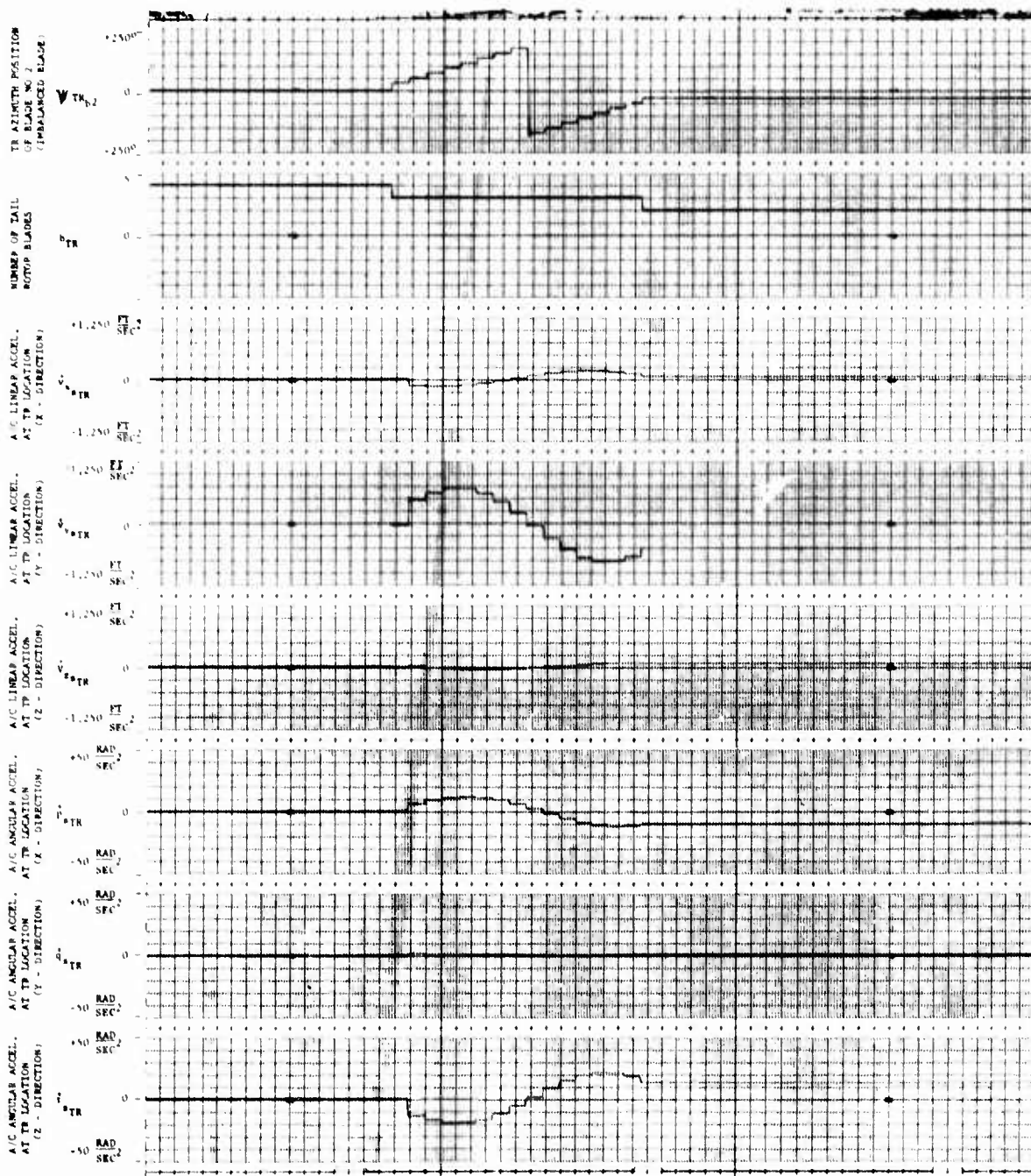
G.W.: 19,900 Lb. FSCG: 360.2 V: Hover  $N_R$ : 100% SAS: OFF  $H_D$ : 10,000 Ft

Figure D-7. (continued)



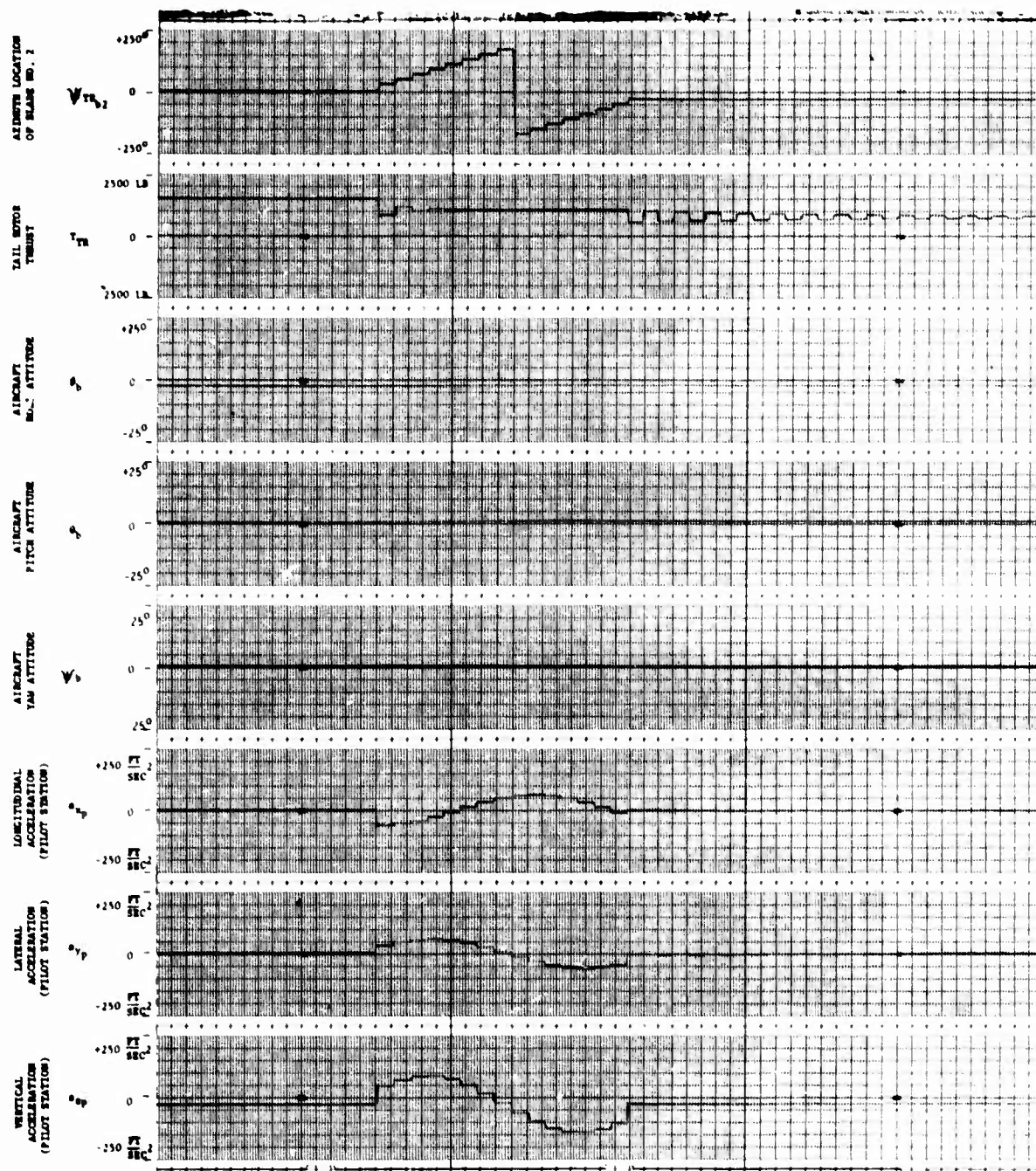
WEIGHT	1990.0	FSCG	360.20000	V	1.0E-2	PSTR2	0.0
IX	5468.0	WLCG	245.89999	DELS	-5.0	VXSTR	0.0
IY	48267.0	RHO	0.1756000E-2	VBOUND	1077.0	VYSTR	0.0
IZ	38224.0	TIME	0.2000000E-1	DEL3MR	0.0	VZSTR	0.0
OMEGR	27.0	NBS8	4.0	THSTR	-10.0	MLVT	273.0
OMEGT	124.55000	NBS8	5.0	THSTR	-10.0	PSVT	695.0
KFR	15.0	PASCHT	2552.0	WLMY	234.0	OSTR	0.0
F8MT	700.40000	SMT	45.0	SVT	32.30000	XA	48.362857
LAT8TK	-0.26194274	A18	-1.3623362	INT	33.26364	XB	39.600431
LNG8TK	2.9400136	Q18	1.5057925	IS	-3.0	XC	66.771450
CUL8TK	21.163431	THETAB	21.163431	TH5MR	11.00331	XP	22.400671
PEDAL	21.355629	THETR	34.175747	TH5TR	20.675747	XPIN	1.2896007
XAIN	4.8362857	XBIN	3.960031	XCIN	6.6771450	OSTR	0.0
XOACTP	46.394391	XOACTI	4.6394391	RSTR	0.0	OSTR	0.0
VXB	0.16035313E-1	THETAB	4.9630512	AAOF	4.326802	OSTR	0.0
VYB	0.0	PHIB	-3.0507550	AAIF	-1.7359206	OSTR	0.0
VZB	0.14620205E-2	BETAP	0.0	BBIF	-1.4543021	OSTR	0.0
P	0.0	GAMC	0.0	ABOL	-0.1493685	OSTR	0.0
O	0.0	OMGRAT	1.0	AILL	-0.31072219E-1	OSTR	0.0
R	0.0	P8100T	0.0	GBIL	0.1656303	OSTR	0.0
ALFHF	-13.121027	EXTX	-0.28429196	EKHFH	0.7995393E-5	OSTR	0.0
CHITPP	-1.7110056	EXTZ	0.24672061	EKHFZ	0.11090360E-3	OSTR	0.0
EXTR	0.0	EP8MT	0.44999999	SIGMT	0.0	OSTR	0.0
QNF	0.27402202E-6	KQMT	0.07177979	KQVT	0.04052013	OSTR	0.0
MUXS	0.23312002E-4	CTB16	0.10035051	LTOT	-20.492385	OSTR	0.0
MUXS	0.0	CH816	-0.39635926E-2	LTOT	26.570964	OSTR	0.0
MUXS	0.79904720E-6	COM816	0.94244001E-6	TTR	1500.1092	OSTR	0.0
LAMQMR	-0.60135195E-1	NZ	0.99467900	MPMR	2201.0577	OSTR	0.0
DASHMR	0.60135993E-1	VC	0.13060751E-3	KTRBLK	0.79599999	OSTR	0.0
XMR	1647.3620	MBAR	-670.12006	VX000T	0.10620064E-2	OSTR	0.0
YMR	-405.50052	JBAR	405.50052	VY000T	-0.46308191E-3	OSTR	0.0
ZMR	-10476.530	TBAR	1053A.066	VZ000T	0.1160494E-3	OSTR	0.0
LMR	-0706.5900	LBARM	-3930.1350	POOT	-0.31024201E-3	OSTR	0.0
MMR	15006.750	MBARM	-4002.0326	QOOT	-0.02030573E-4	OSTR	0.0
NMR	43912.530	QBARM	44052.059	RDOOT	0.63513940E-5	OSTR	0.0
XMF	-0.50331269E-5	XT	4.5730900	XTR	0.0	OSTR	0.0
YMF	0.0	YT	-0.35024303E-6	YTR	1417.2645	OSTR	0.0
ZMF	0.71424000E-5	ZT	5.9241120	ZTR	-515.04310	OSTR	0.0
LWF	0.0	LT	-0.79096733E-6	LTR	0704.0069	OSTR	0.0
MWF	0.0	MT	172.40356	MTR	-15982.530	OSTR	0.0
NWF	0.0	NT	0.97710030E-5	NTR	-43911.570	OSTR	0.0
XMT	4.5730999	XVT	-0.79313945E-7	ALFMTT	-7.7194499	OSTR	0.0
YMT	0.0	YVT	-0.35024303E-6	ALFVTT	0.0	OSTR	0.0
ZMT	5.9241119	ZVT	0.609085390E-7	AA00IF	2.2646514	OSTR	0.0

Figure D-7. (continued)



G.W.: 19,900 Lb. FSCG: 347 V: Hover  $N_R$ : 100% SAS: OFF  $H_D$ : 10,000 Ft

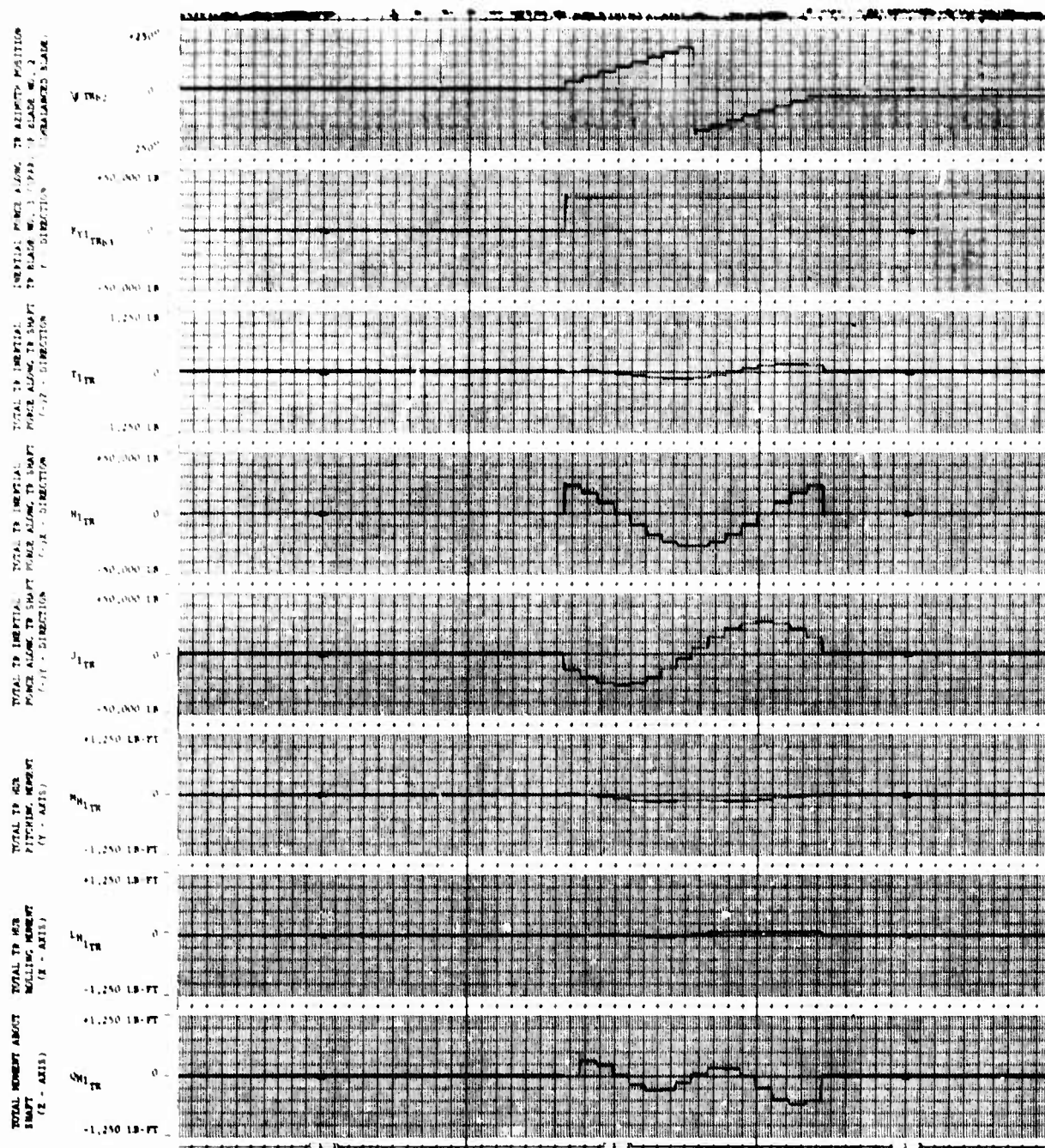
Figure D-8. Stepped Transition Time History



G.W.: 19,900 Lb. FSCG: 347 V: Hover  $N_R$ : 100% SAS: OFF  $H_D$ : 10,000 Ft

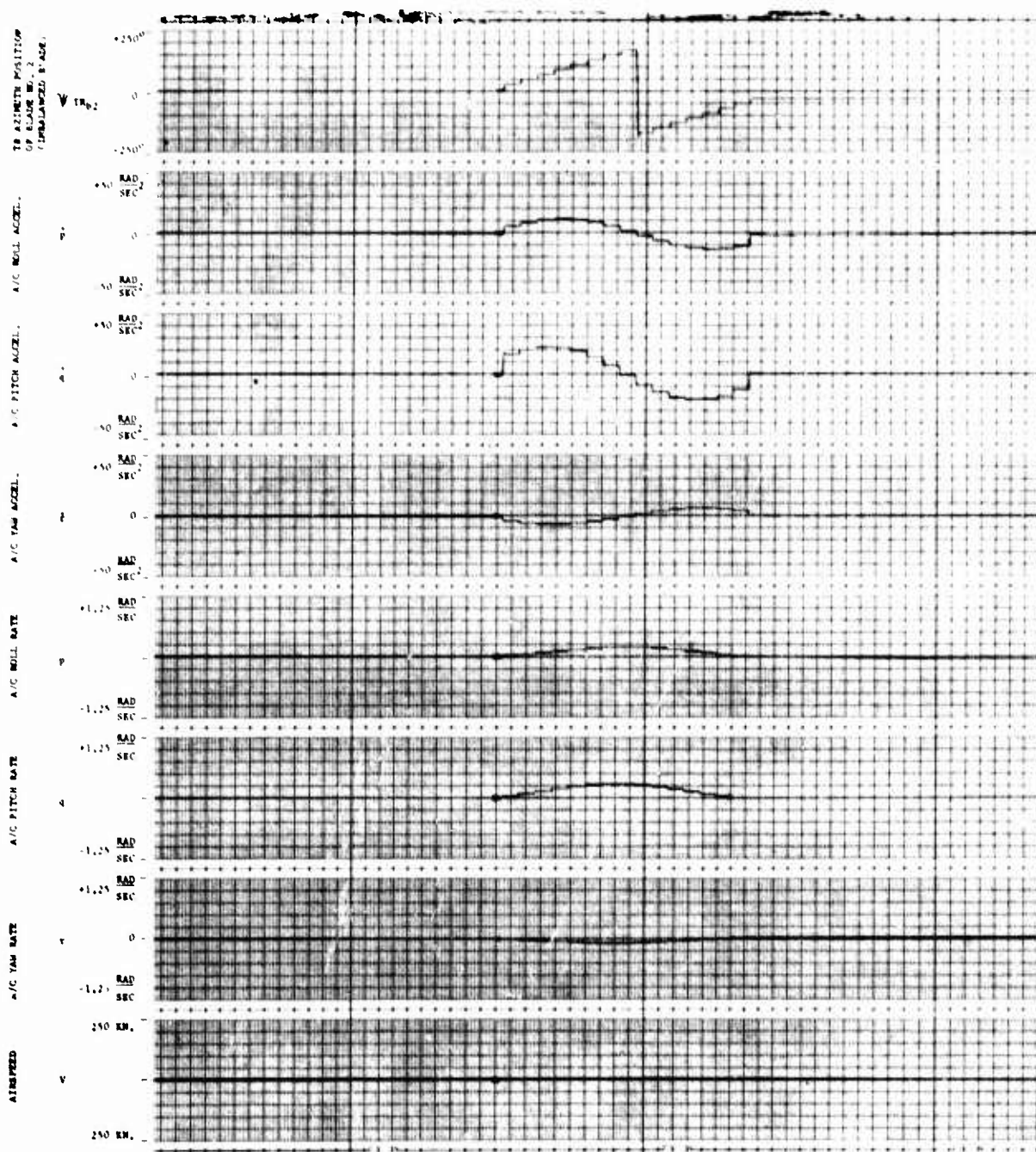
Figure D-8. (continued)





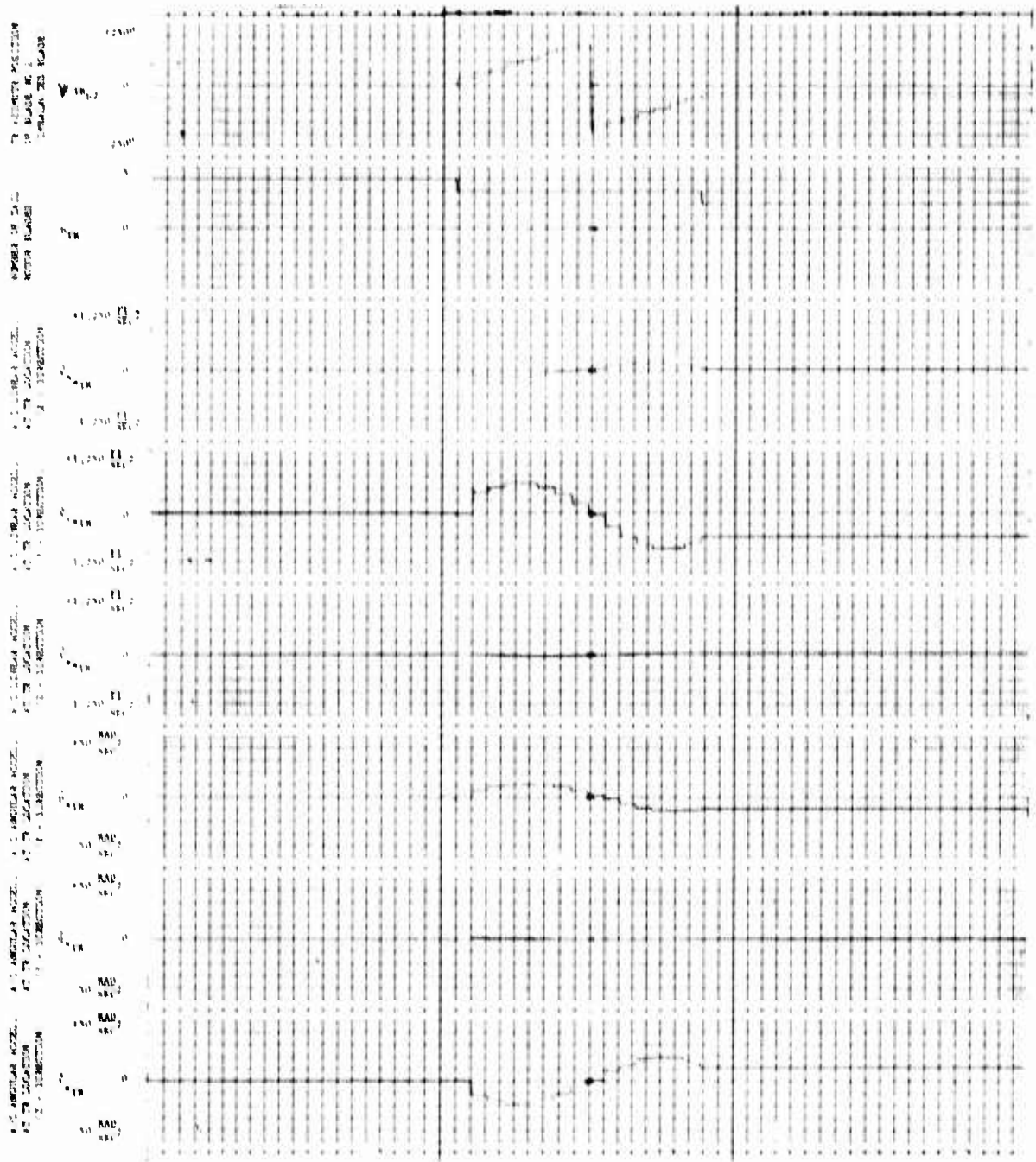
G.W.: 19,900 Lb. FSCG: 347 V: Hover  $N_R$ : 100% SAS: OFF  $H_D$ : 10,000 Ft

Figure D-8. (continued)



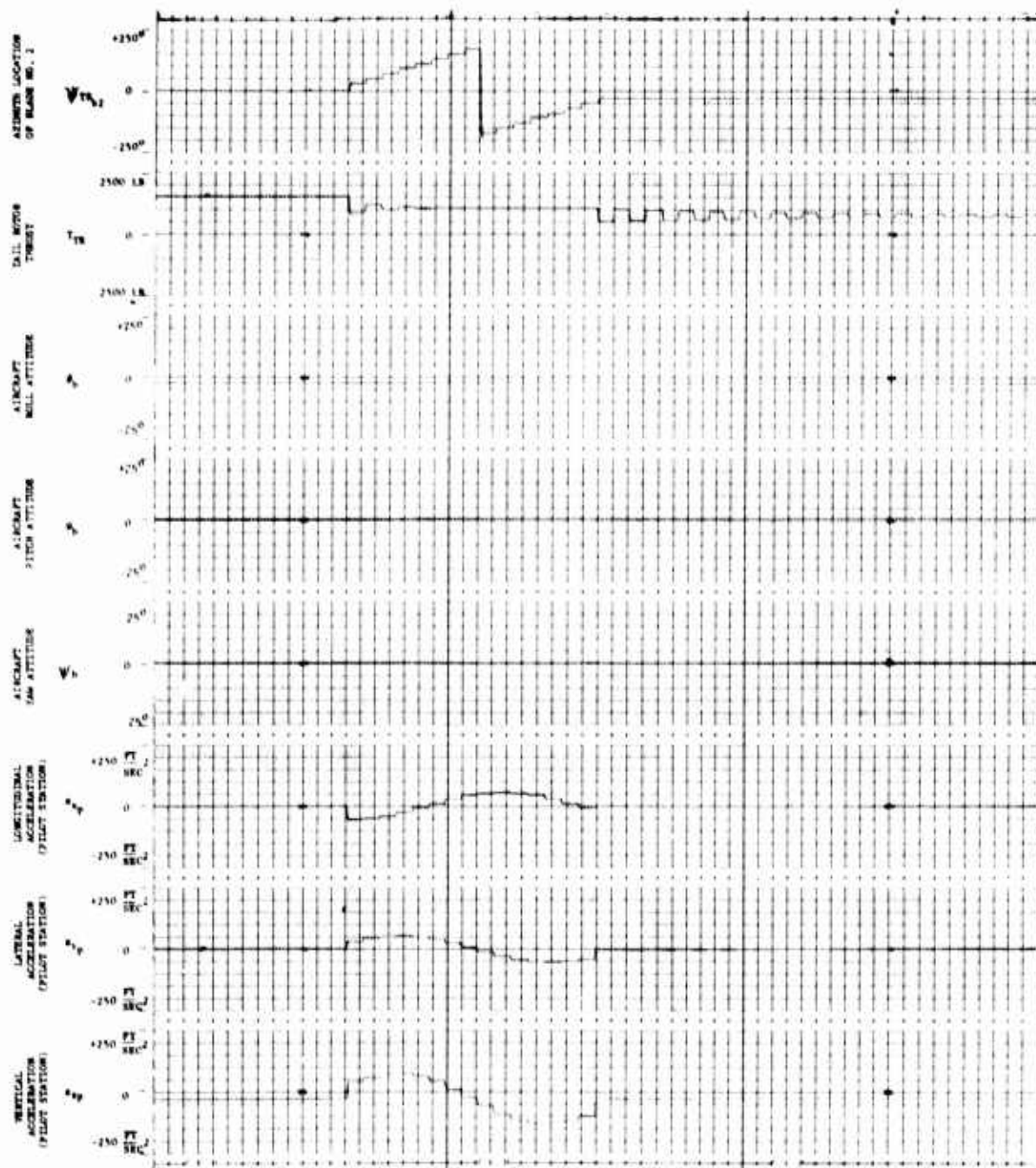
G.W.: 19,900 Lb. FSCG: 347 V: Hover  $N_R$ : 100% SAS: OFF  $H_D$ : 10,000 Ft

Figure D-8. (continued)



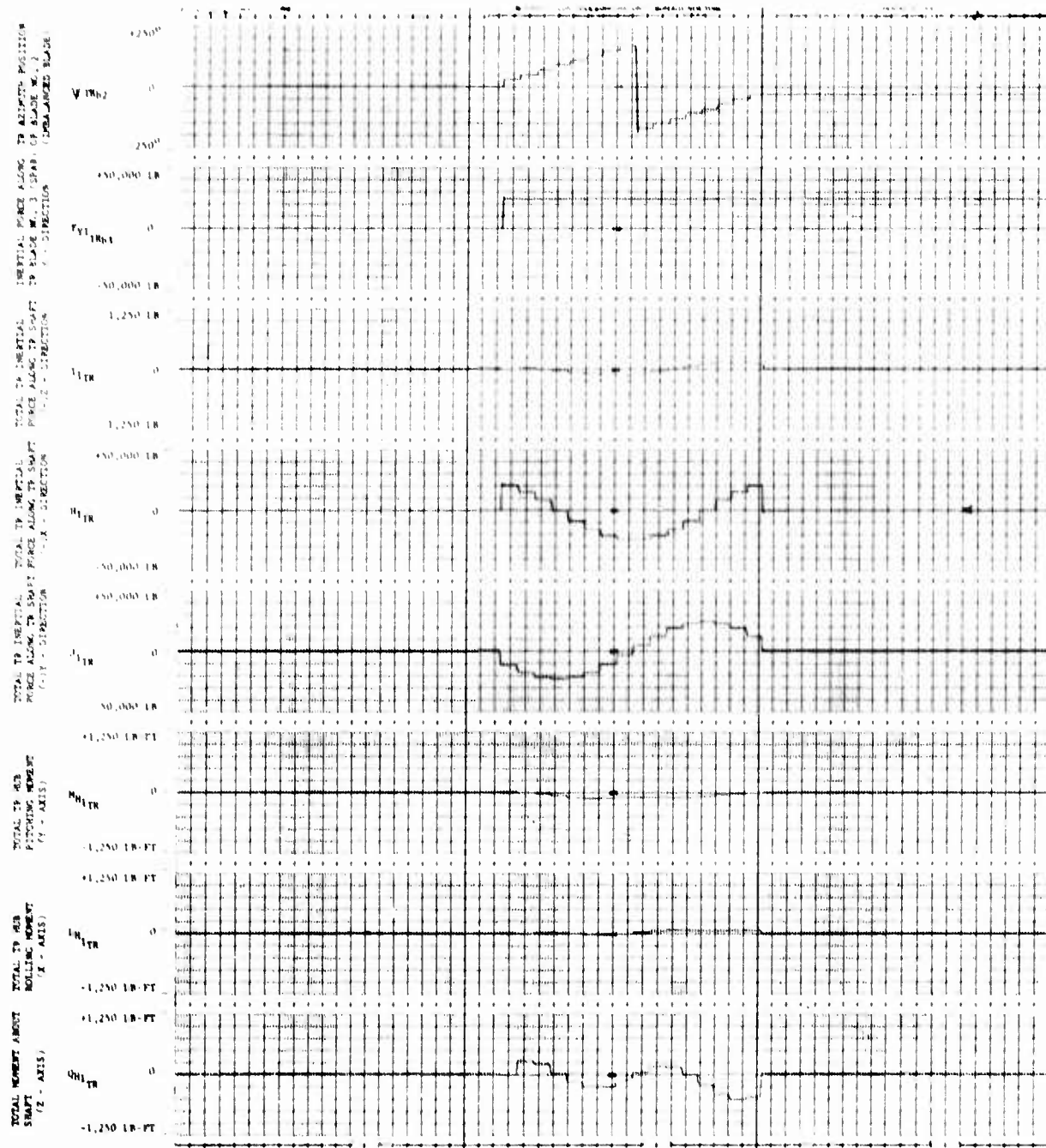
G.W.: 19,900 Lb. FSCG: 347 V: Hover  $N_R$ : 95% SAS: OFF  $H_D$ : 10,000 Ft

Figure D-9. Stepped Transition Time History



G.W.: 19,900 Lb. FSCG: 347 V: Hover  $N_R$ : 95% SAS: OFF  $H_D$ : 10,000 Ft

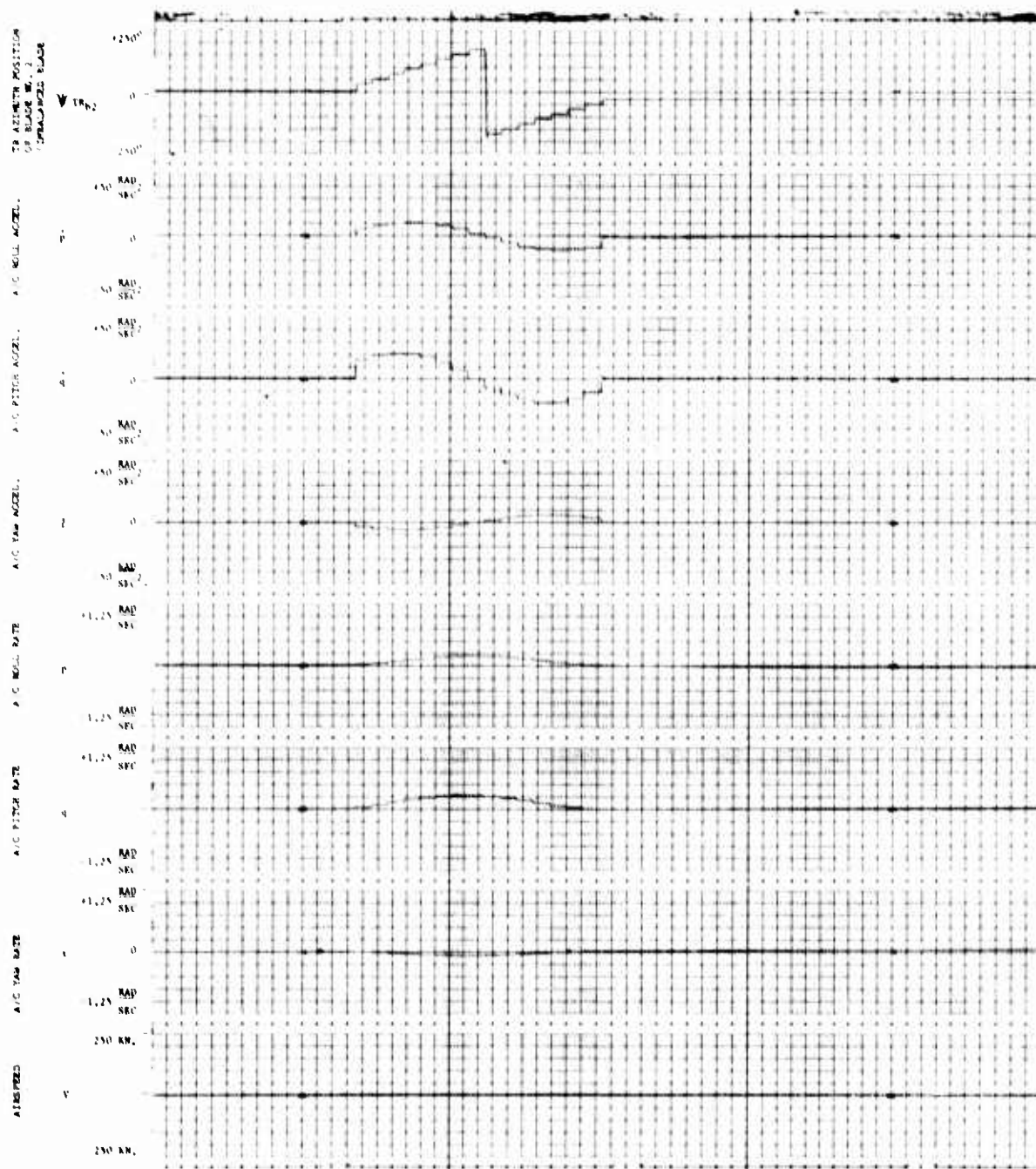
Figure D-9. (continued)



G.W.: 19,900 Lb. FSCG: 347 V: Hover  $N_R$ : 95% SAS: OFF  $H_D$ : 10,000 Ft

Figure D-9. (continued)





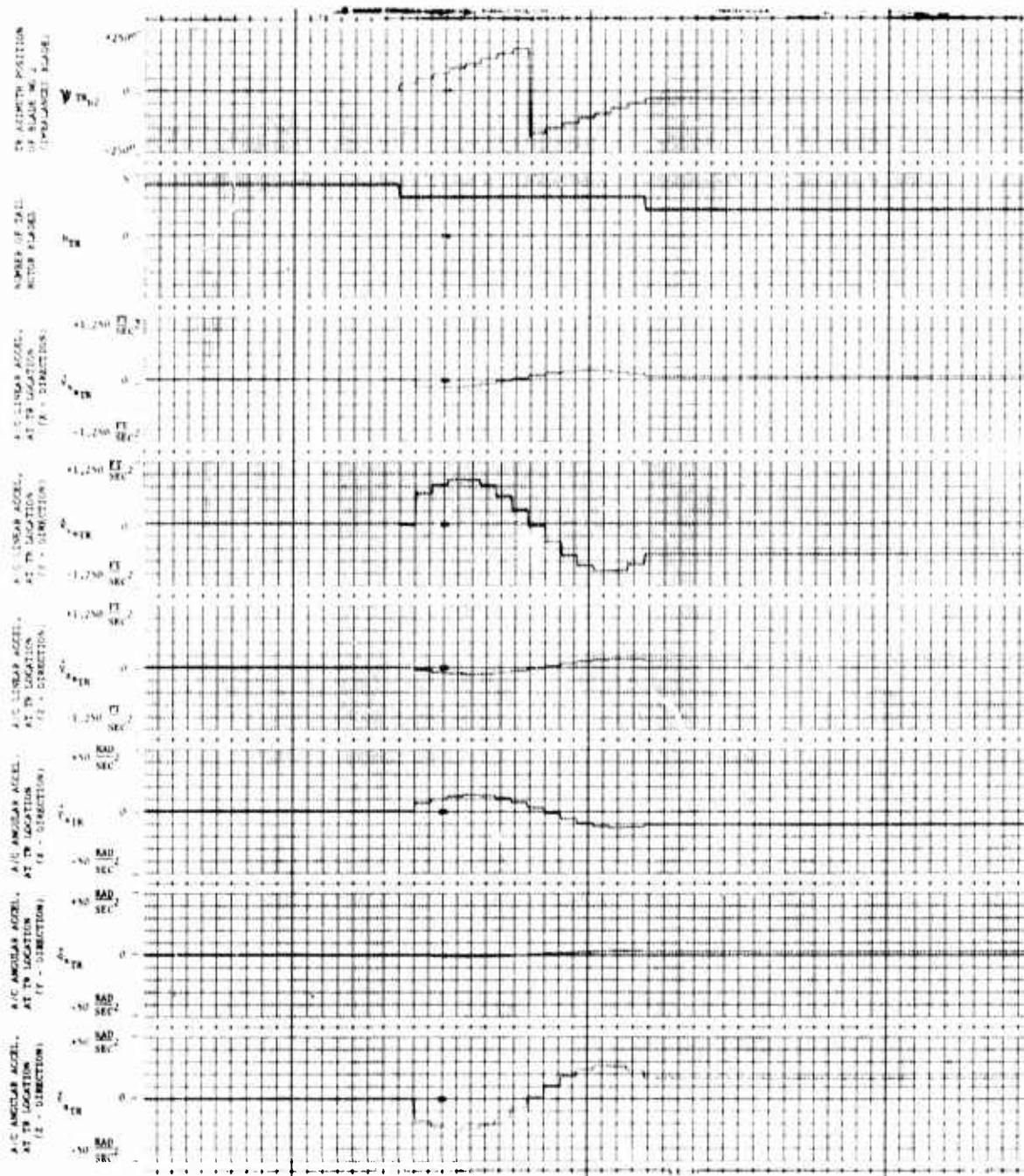
G.W.: 19,900 Lb. FSCG: 347 V: Hover  $N_R$ : 95% SAS: OFF  $H_0$ : 10,000 Ft

Figure D-9. (continued)

UTAS(376) 1-21-77 7-DEC-77 RUN 15.

HEIGHT	19000.0	PSCG	347.0	V	1.0E-2	PSIR2	0.0
IX	5400.0	WLCG	245.09999	DELS	-5.0	VXSTR.	0.0
IY	40307.0	RHO	0.1756000E-2	VROUND	1077.0	VYSTR.	0.0
IZ	38254.0	TIME	0.2000000E-1	DEL3MR	0.0	VZSTR.	0.0
OMEGMR	25.64999	NBS3	4.0	TM3MR	-18.0	PSTR.	0.0
OMEGTR	118.32250	NBS8	5.0	TM3TR	-18.0	WLVT	273.0
APR	15.0	PASCNT	1075.0	WLHT	234.0	F8VT	695.0
PSHT	700.40000	SHT	45.0	SVT	32.00000	QSTR.	0.0
LAT9TK	0.33622503	A19	-0.68756193	IMT	36.0	XA	52.101406
LANGTK	-1.3654426	B19	-2.4827410	IS	-3.0	XB	54.824885
COLSTK	22.361426	THETA0	22.361426	TH7SMR	12.281424	XC	74.250917
PEDAL	21.740664	THETTR	36.006376	TH7STR	22.506376	XP	21.311008
XAIN	5.2101406	XBIN	5.4824889	XCIN	7.4258917	XPIN	1.1507600
XBACTP	60.007016	XBACTI	6.0007016	RSTR.	0.0	PSTR	0.0
VX0	0.1609650E-1	THETAB	0.74245104	AA0F	4.0596993	QSTR	0.0
VY0	0.0	PHI0	-2.3784134	AA1F	2.6772541	RSTR	0.0
VZ0	0.21096020E-3	BETAMP	0.0	BB1F	-1.0241204	TSTR	0.0
P	0.0	GAMC	0.0	AA0L	-9.4000691	HSTR	0.0
R	0.0	OMGRAT	1.0	AA1L	-0.1635800	JSTR	0.0
ALFWF	-0.513533	PSIDOT	0.0	BB1L	-0.1606945	MSTR	0.0
CHITPP	2.7012510	EKTZ	-0.53023976	EKWFZ	0.2161007E-1	LHSTR	0.0
EATR	0.0	EPSWT	0.44999999	SGMT	0.29953885	CHSTR	0.0
QAF	0.19399675	KQHT	1.0	KQVT	0.64832013	XSTR	0.0
MUX5	0.24533431E-4	CTSIG	0.12049727	LTOT	-70.0	VSTR	0.0
MUY8	0.0	CHSIG	0.51625223E-2	DTOT	45.079999	LSTR	0.0
MUZ8	-0.96721173E-6	COMSIG	0.11730630E-5	TTR	1526.2310	HSTR	0.0
LAMBMR	-0.71046474E-1	NZ	0.99491798	HPMR	2170.2562	NSTR	0.0
DASHMR	0.71045507E-1	VC	0.11546071E-4	KTRBLK	0.79599999	AXP	0.39500075
XMR	177.73051	MBAR	797.13025	VX800T	-0.2206597E-1	AYP	1.3585305
YMR	-620.64860	JBAR	620.64860	VY800T	0.2302536E-1	AZP	-32.139716
ZMR	-18620.412	TBAR	18605.638	VZ800T	0.17653953E-3	VXP	0.16896658E-1
LMR	-8508.0047	LBARH	-2602.3943	PDOT	0.2593833E-3	VYP	0.0
MMR	14096.092	MBARM	6501.1971	QDOT	-0.17789459E-3	VZP	0.21096020E-3
NMR	40815.352	OBAR	46535.709	RDOT	-0.26210617E-4	RSTR.	0.0
XMF	12.904950	XT	43.499392	VTR	0.0	PSIDMG	-150.0
YMF	0.0	YT	-0.34978258E-6	VTR	1434.2946	BTR	4.0
ZMF	9.7135899	ZT	65.393978	ZTR	-922.04158	MADD	0.0
LMF	0.0	LT	-0.78992567E-6	LTR	8009.4865	XADD	0.0
MMF	-124.21451	MT	1960.9895	MTR	-16740.833	YADD	0.0
NMF	0.0	NT	0.1013694E-4	NTR	-46016.954	ZADD	0.0
XMT	43.499392	XVT	-0.62192185E-7	ALPHIT	-19.652797	NADD	0.0
YMT	0.0	YVT	-0.34978258E-6	ALFVTT	0.0	LADD	0.0
ZMT	65.393978	ZVT	0.64518045E-7	AAB81F	2.0664459		

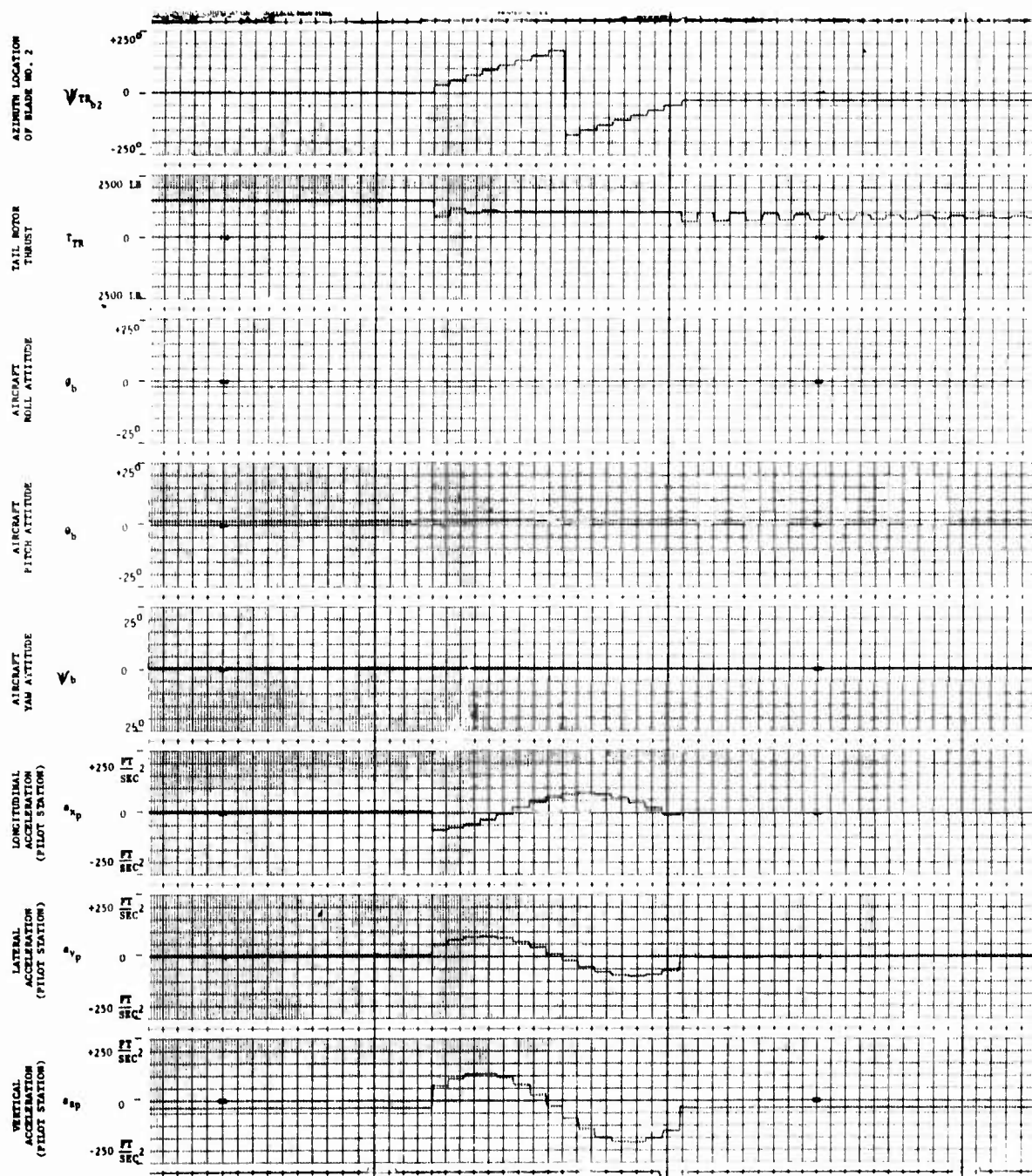
Figure D-9. (continued)



G.W.: 19,900 Lb. FSCG: 347 V: Hover  $N_R$ : 100% SAS: OFF  $H_D$ : 10,000 Ft

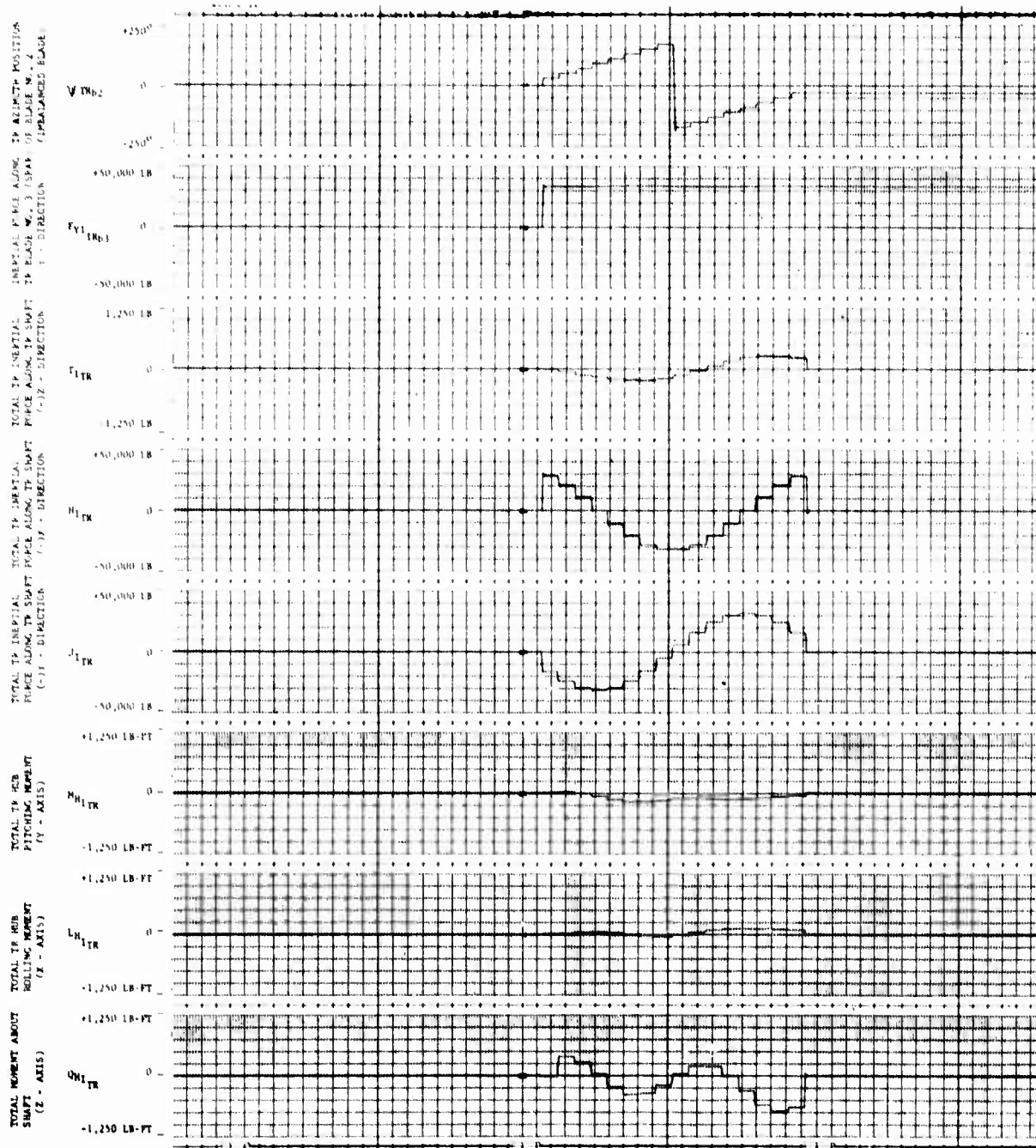
Figure D-10. Stepped Transition Time History





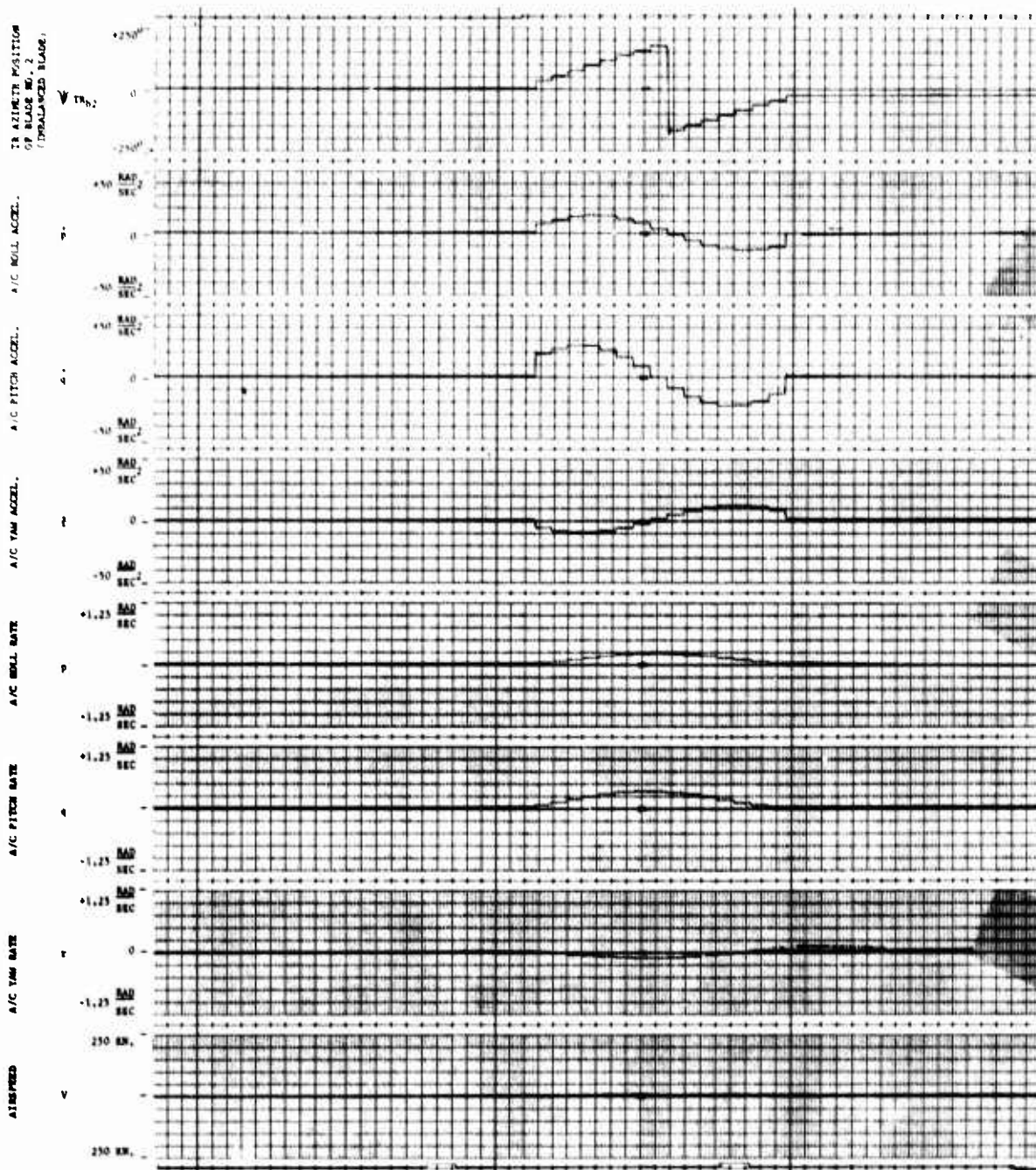
G.W.: 19,900 Lb. FSCG: 347 V: Hover  $N_R$ : 100% SAS: OFF  $H_D$ : 10,000 Ft

Figure D-10. (continued)



G.W.: 19,900 Lb. FSCG: 347 V: Hover N<sub>R</sub>: 100% SAS: OFF H<sub>D</sub>: 10,000 Ft

Figure D-10. (continued)



G.W.: 19,900 Lb. FSCG: 347 V: Hover  $N_R$ : 100% SAS: OFF  $H_D$ : 10,000 Ft

Figure D-10. (continued)

UTTAB(376) 1-21-77 9-DEC-77 RUN 12.

WEIGHT	1900.0	FSCG	347.0	V	1. RE-2	PSTR2	0.0
IX	500.0	WLCG	245.09999	DELS	-5.0	VASTR.	0.0
IV	40207.0	MHO	0.17560006E-2	VROUND	1077.0	VASTR.	0.0
IJ	20224.0	TIME	0.20000000E-1	DEL3MR	0.0	VASTR.	0.0
OMEGR	29.700000	MSS	4.0	THSTR	-10.0	PSTR.	0.0
OMEGR	137.00499	MSS	5.0	THSTR	-10.0	WLVT	273.0
KPR	15.0	PASCNT	797.0	WLMT	234.0	PST	695.0
FMT	70P.40000	SMT	45.0	SVT	32.30000	OSTR.	0.0
LATSK	0.7700578E-1	AIS	-0.04272174	INT	30.095614	XA	50.401291
LNGSK	-0.0422245	BIS	-1.048936	IS	-3.0	XB	51.569690
COLSK	19.409401	THETA0	19.409401	TH75MR	9.3294011	XC	55.000758
PEDAL	19.711142	THETTR	30.426423	TH75TR	16.926423	XP	26.959573
XAIN	5.0401291	XBIN	5.1569690	XCIN	5.5008750	XPIN	1.4557791
XACTP	56.909551	XACTI	5.6909551	RSTR.	0.0	PSTR	0.0
VXB	0.16094791E-1	THETA0	1.1575311	AAPF	3.5190006	OSTR	0.0
VYB	0.0	PHI0	-2.5714600	AAIF	1.9909193	PSTR	0.0
VZB	0.34130616E-3	BETAMP	0.0	BBIF	-0.90406475	TITR	0.0
P	0.0	GAMC	0.0	AAOL	-6.3604605	HITR	0.0
O	0.0	OMGRAT	1.0	AAIL	-0.9258007E-1	JITR	0.0
R	0.0	PSIOOT	0.0	BBIL	-0.93195509E-1	HHITR	0.0
ALFDF	-05.791369	EKTZ	-0.49606364	ERWFX	0.16119244E-1	LMITR	0.0
CHITTP	2.0149056	EKTZ	0.63757079	ERWFZ	0.22365521	OHITR	0.0
EKTR	0.0	EPBNT	0.44999999	SIGMT	0.0	XITR	0.0
QNF	0.10011099	KOMT	1.0	KQVT	0.04052013	VITR	0.0
MUXS	0.21193662E-4	CTBIO	0.90829608E-1	LTOT	-70.0	ZITR	0.0
MUYB	0.0	CHBIO	0.29592792E-2	DTOT	45.079999	LITR	0.0
MUZB	-0.60179104E-6	COMBIO	0.63356932E-6	TTR	1394.9149	MITR	0.0
LAMBDR	-0.62100330E-1	NZ	0.59563440	MPMR	2296.3993	NITR	0.0
D-SMR	0.62099656E-1	VC	0.21610908E-4	KTRBLK	0.79599999	AXP	0.67521553
XMR	363.65694	MBAR	612.62041	VXODOT	0.25050996E-1	AYP	1.4326575
YMR	-460.02712	JBAR	400.02712	VYODOT	-0.08308062E-2	AZP	-32.129302
ZMR	-10642.720	TBAR	10637.649	VZODOT	0.59669530E-4	VXP	0.16094791E-1
LMR	-0051.7150	LBARM	-3060.9140	PDOT	0.18407133E-3	VYP	0.0
MMR	13000.949	MBARM	6590.1334	DDOT	0.19199304E-3	VZP	0.34130616E-3
MKR	42071.915	OBAR	62325.914	RODT	0.51938199E-3	RSTR.	0.0
XMF	7.1901497	XT	30.079456	XTR	0.0	PSIDMG	-150.0
YMF	0.0	YT	-0.34976672E-6	YTR	1310.0007	BTR	4.0
ZMF	5.4163090	ZT	52.494390	ZTR	-477.12501	MADD	0.0
LMF	0.0	LT	-0.70900906E-6	LTR	0051.5233	XADD	0.0
MMF	-69.230111	MT	1575.7000	MITR	-15307.773	YADD	0.0
NMF	0.0	NT	0.10143233E-4	NTR	-42057.601	ZADD	0.0
XMT	30.079456	XVT	-0.04416423E-7	ALFMTT	-22.034167	MAOD	0.0
YMT	0.0	YVT	-0.34976672E-6	ALFVTT	0.0	LADD	0.0
ZMT	52.494390	ZVT	0.02035500E-7	AABGIF	2.1069010		

Figure D-10. (continued)

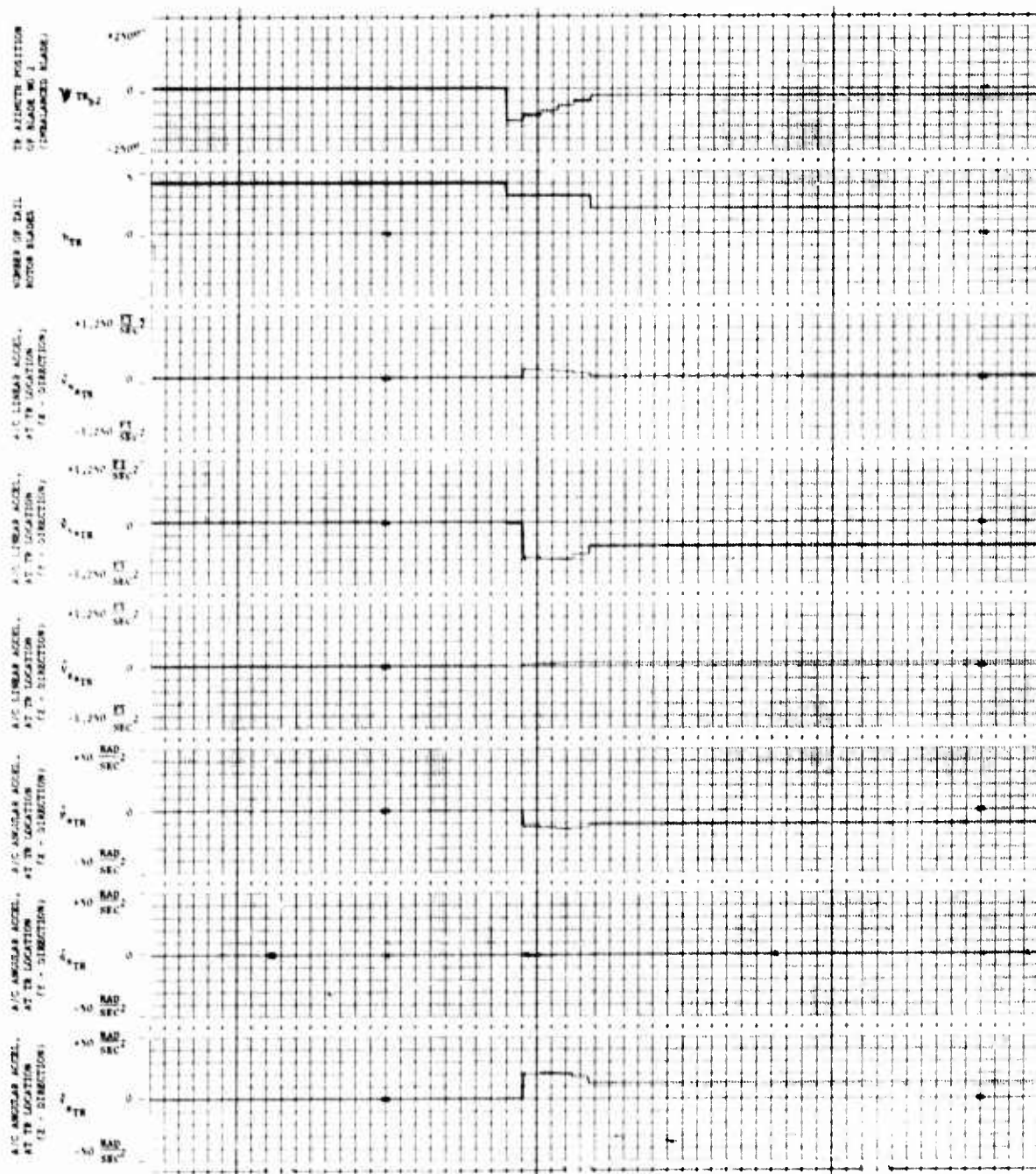


Figure D-11. Stepped Transition Time History, Damage = 50<sup>0</sup>



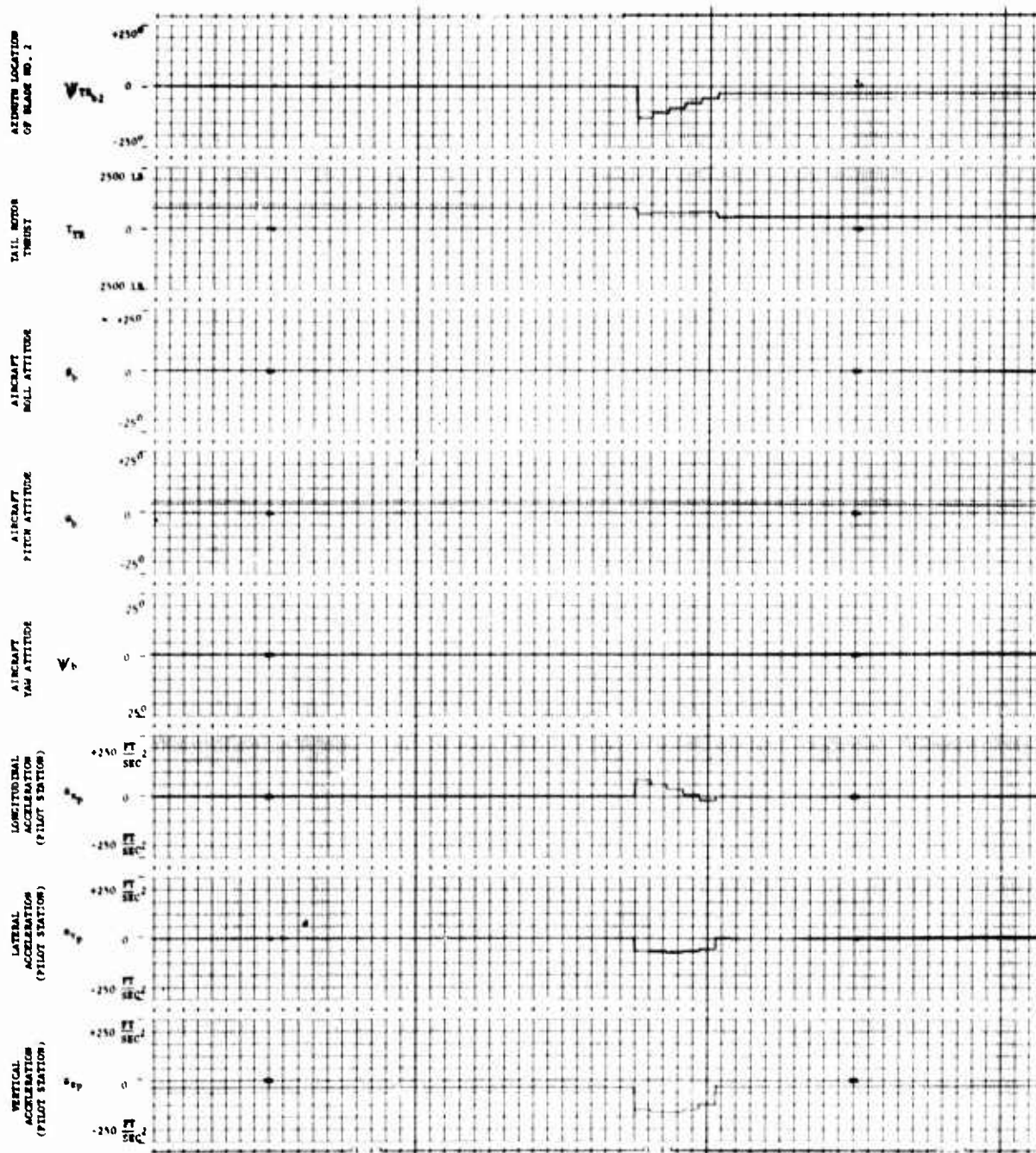


Figure D-11. (continued)

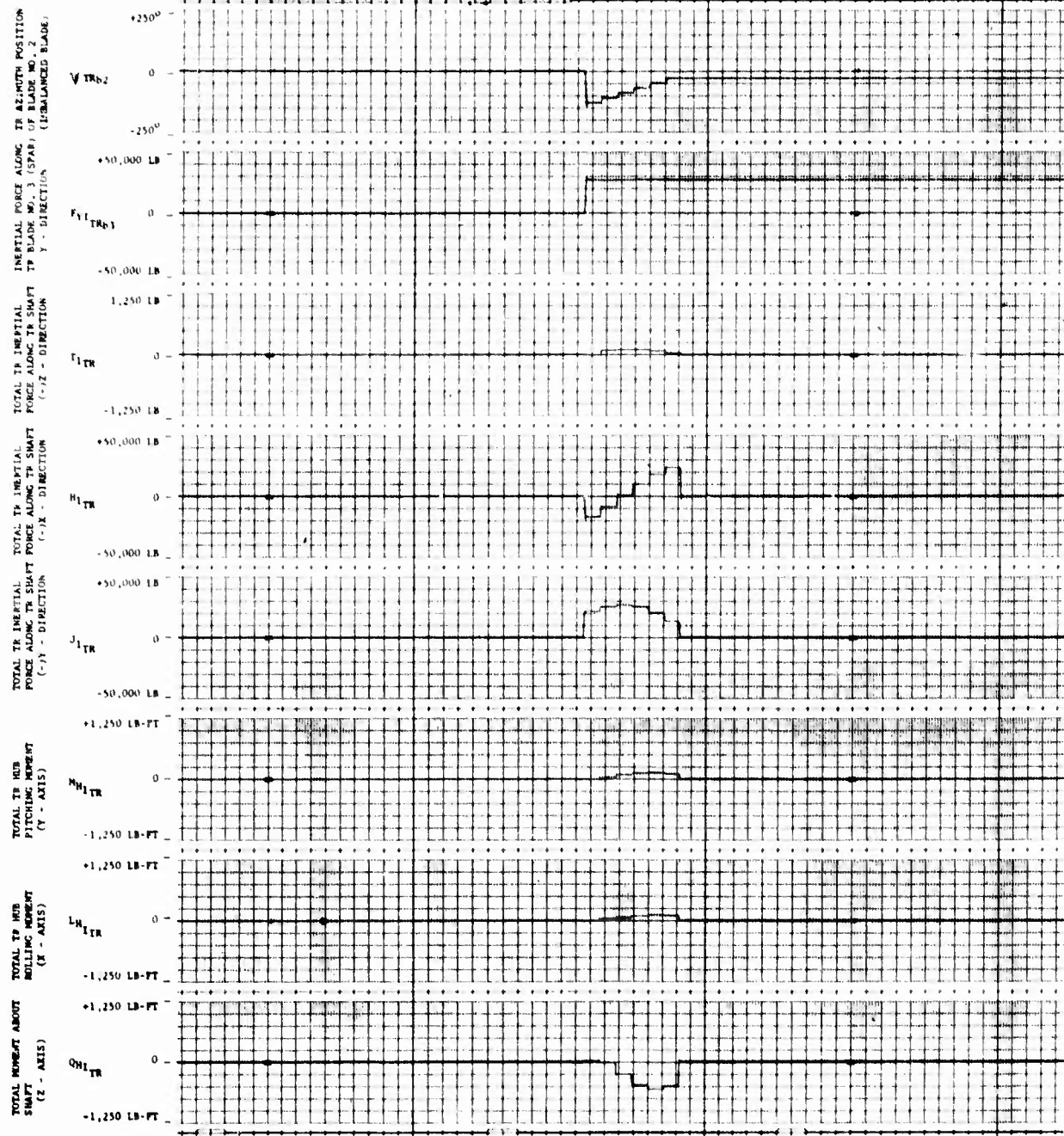


Figure D-11. (continued)

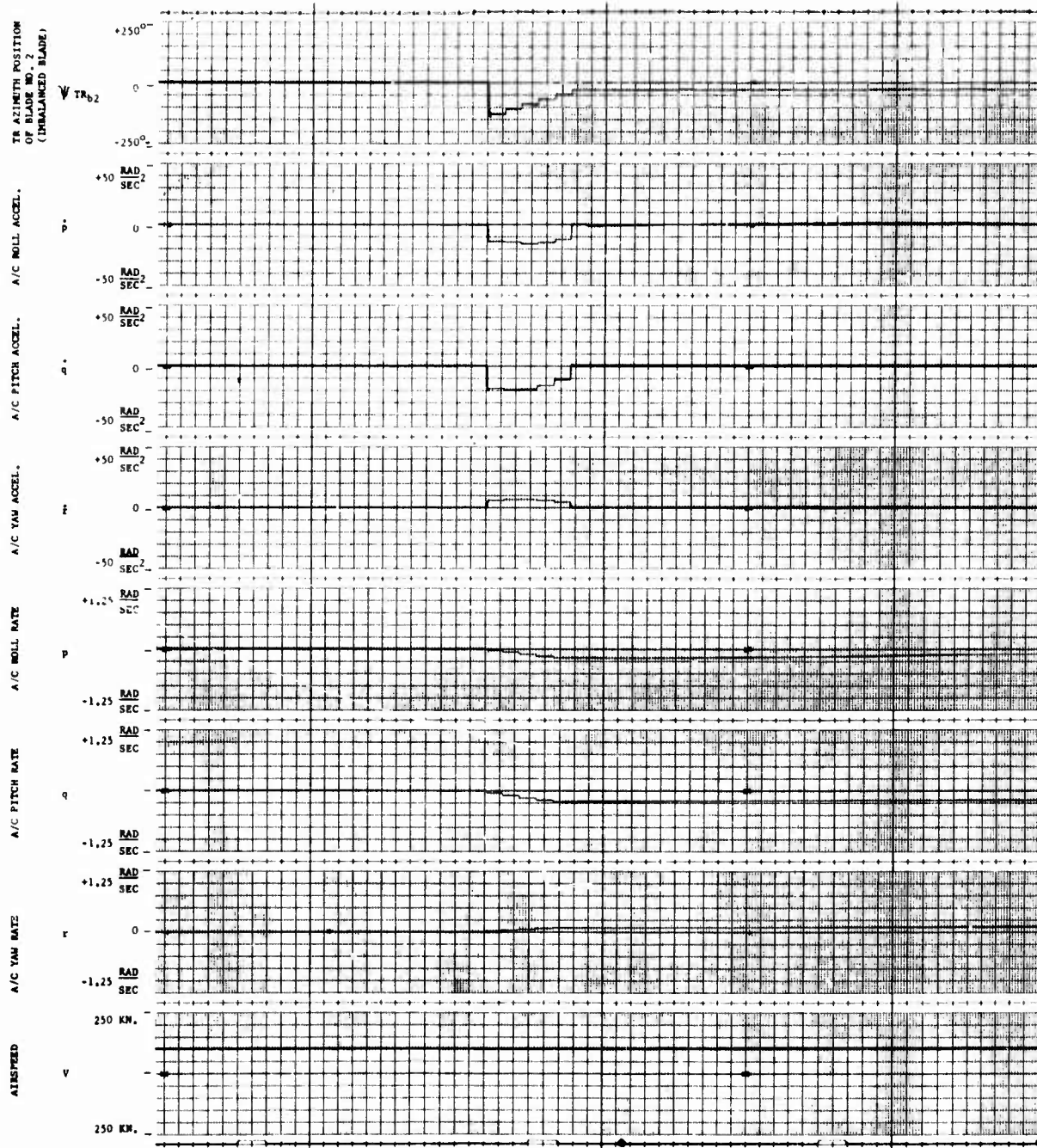


Figure D-11. (continued)



UTIAS (376) 1-21-77 15 NOV-77 RUN 10.

WEIGHT	16450.0	FSCG	360.23000	V	100.0	PSITR2	0.0
IX	4330.0	WLCG	245.09999	DELS	-5.0	VXSTR.	0.0
IY	38515.0	RMO	0.2370000E-2	V SOUND	1116.0	VYSTR.	0.0
IZ	37363.0	TIME	0.2000000E-1	DEL3MR	0.0	VZSTR.	0.0
OMEGMA	27.0	MDS	4.0	TH3THR	-18.0	ASTR.	0.0
OMEGTA	124.55000	MDS	5.0	TH3THR	-18.0	MLVT	273.0
KFR	15.0	PASCHT	1217.0	MLMT	234.0	PSVT	695.0
F8MT	700.40000	3MT	45.0	SVT	32.30000	OSTR.	0.0
LAT8TK	-0.59340201	A18	-1.2161207	IMT	-2.7695562	XA	46.290737
LG8TK	0.7472700	B18	0.0051600	IS	-3.0	XB	19.090009
COL8TK	16.525114	THETAB	16.525114	TH7SHR	6.4451140	XC	37.701963
PEDAL	11.107153	THETTR	16.441292	TH7STR	4.9412920	XP	50.590054
XAIN	4.6290737	XBIN	1.9090009	XCIN	3.7701963	XPIN	2.7317919
XOACTP	21.024000	XOACTI	2.1024000	ASTR.	0.0	ASTR	0.0
VXB	160.65003	THETAB	3.6000032	AABF	3.1014497	OSTR	0.0
VYB	11.391420	PHIB	0.0	AAIF	-5.6001062	RSTR	0.0
VZB	10.047795	REYAMP	3.6790093	BBIF	0.00609945201	YSTR	0.0
P	0.0	GAMC	0.0	AABL	-4.1900659	MSTR	0.0
R	0.0	OMGRAT	1.0	AAIL	0.24107694	JSTR	0.0
ALFMP	0.55000906	PSIDOT	0.0	BBIL	0.36200003	MHSTR	0.0
CHITPP	02.003040	EXTX	1.6498261	ERMPX	0.92600990	LMSTR	0.0
EKTR	0.0	EXTZ	1.0079961	EKWFZ	1.0079961	OMSTR	0.0
QMP	37.429361	EPSTY	0.40679009	SIGMT	0.64751973	XSTR	0.0
MUXS	0.23325674	KOHT	0.07177970	KOVT	0.03100377	YSTR	0.0
MUYB	0.15725112E-1	CTBIC	0.67070520E-1	LTOT	3.4630934	ZSTR	0.0
MUZB	0.27699011E-2	CHBIC	-0.47506990E-2	DTOT	24.481060	LSTR	0.0
LAMBMR	-0.97539490E-8	COMBIC	0.40092032E-6	TTR	0.37.00001	MSTR	0.0
DM8MR	0.12522950E-1	NZ	0.99705491	MPMR	1133.2135	NSTR	0.0
XMR	1922.0494	VC	0.71525533E-3	MTBRLK	1.0	AXP	2.0042153
YMR	-254.36015	MBAR	-1100.6090	VX00OT	0.15104240E-2	AYP	-0.24406269E-1
ZMR	-15044.553	JBAR	254.36015	VY00OT	-0.14300017E-1	AZP	-32.103912
LMP	-5026.5936	TBAR	15724.929	VZ00OT	0.2390519E-2	VXP	160.65003
MMR	-042.14135	LBARM	-2201.0103	PDOT	-0.95050965E-2	VYP	11.391420
NMR	22507.512	MBARM	-15256.306	QDOT	0.20201096E-2	VZP	10.047795
XMP	-093.60400	OBAR	23003.970	RDOT	-0.29749000E-2	RSTR.	0.0
YMP	-361.12760	XT	-23.053153	XTR	0.0	PSIDMO	50.0
ZMP	-130.22601	YT	-170.11212	YTR	706.62007	BTR	4.0
LMP	556.64727	ZT	464.63322	ZTR	-206.30030	MADO	0.0
MMP	-3392.2619	LT	-395.01927	LTR	0031.0717	YADD	0.0
NMP	-3194.7102	MT	13103.227	MTR	-0070.7055	XADD	0.0
XMT	-13.177201	NT	4970.2169	NTR	-24372.235	ZADD	0.0
YMT	-1.9745510	XVT	-10.675071	ALPMTT	-4.7500403	MADD	0.0
ZMT	404.26319	YVT	-176.13757	ALPVT	3.0617702	LADD	0.0
		ZVT	0.37005121	A001F	5.6000070		

Figure D-11. (continued)

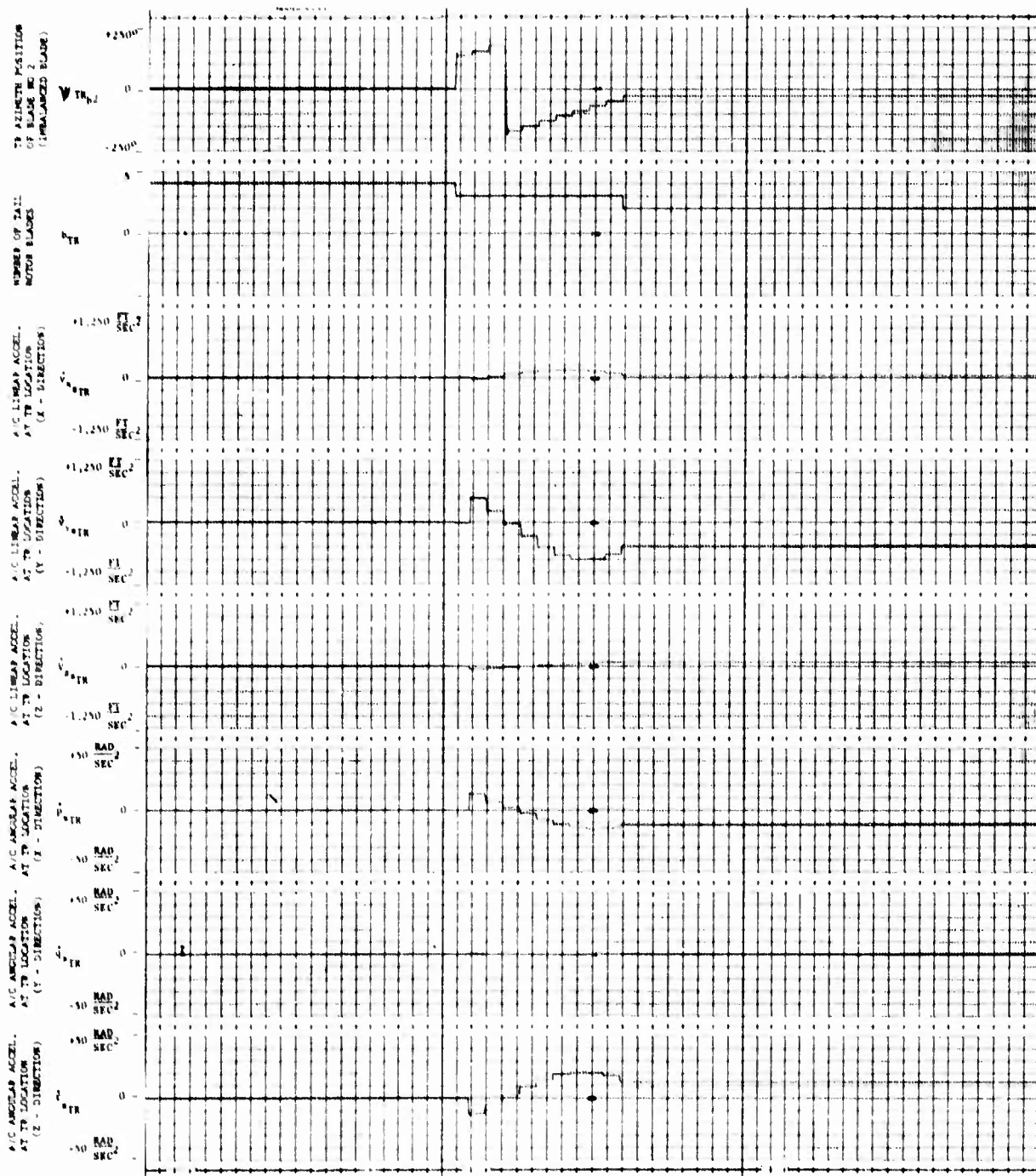


Figure D-12. Stepped Transition Time History,

Damage =  $-50^{\circ}$

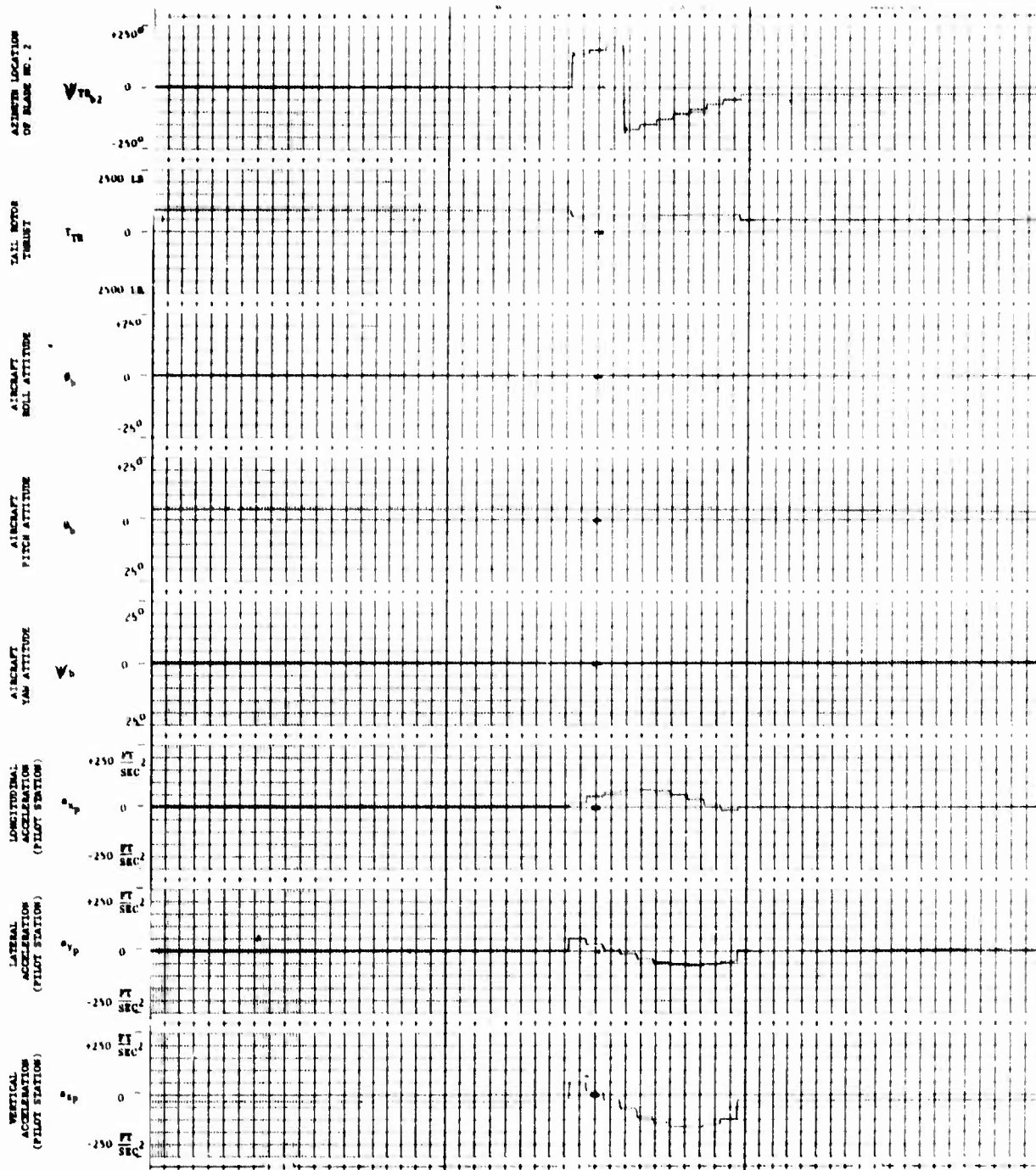


Figure D-12. (continued)



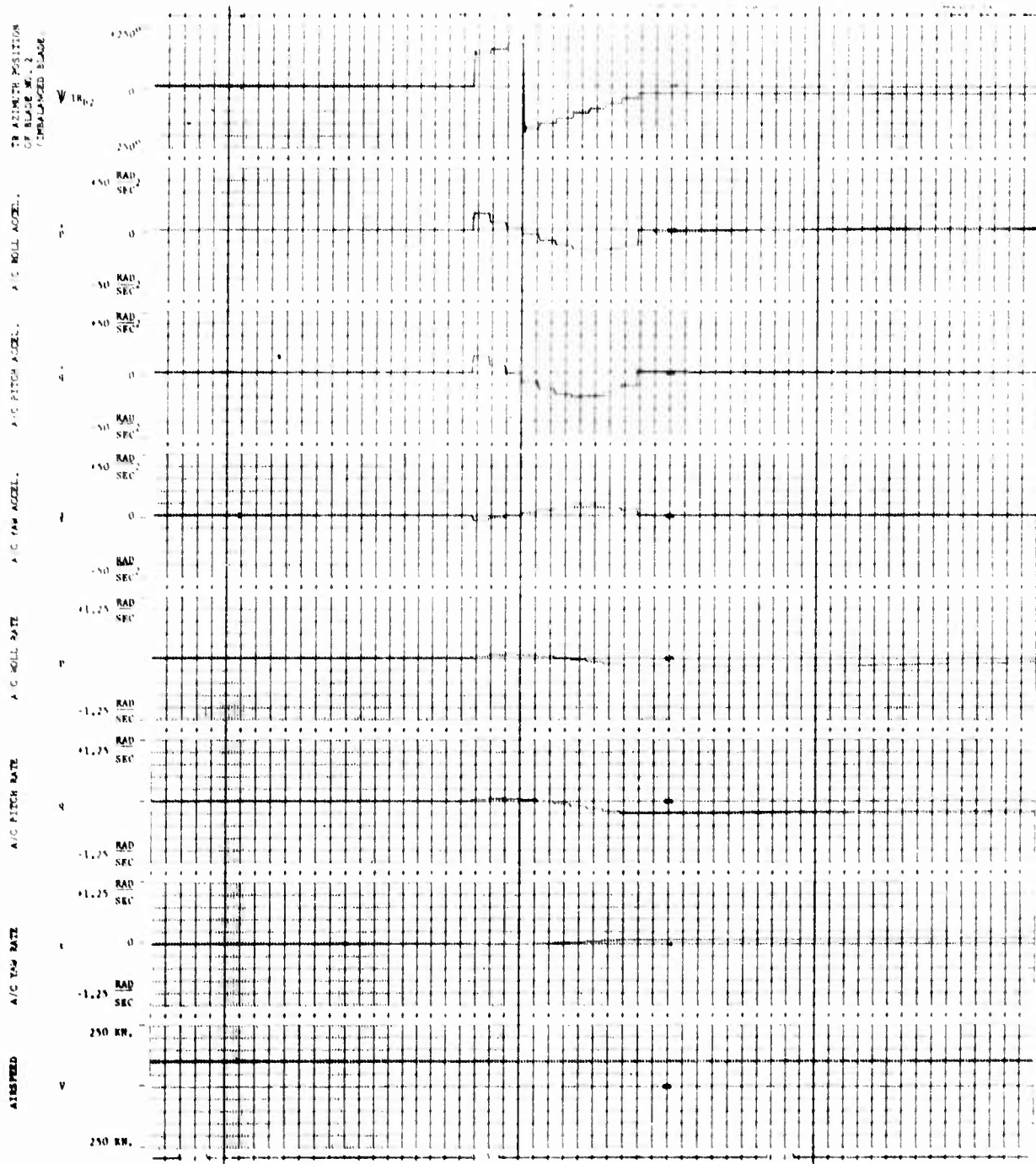


Figure D-12. (continued)

UTIAS(S76) 1-21-77 18 47-NOV-77 RUN 11.

WEIGHT	1045R.0	PSCG	369.20000	V	10R.0	PSITR2	0.0
IX	4330.0	WLCG	245.09999	DELS	-5.0	VXSTR.	0.0
IY	30513.0	RHO	0.2370000E-2	V SOUND	1116.0	VYSTR.	0.0
IZ	37363.0	TIME	0.2000000E-1	DELMR	0.0	VZSTR.	0.0
OMEGMR	27.0	NBS9	4.0	TMSTR	-10.0	PSTR.	0.0
OMEGTR	124.55000	NBS9	5.0	TMSTR	-10.0	MLVT	273.0
KFR	15.0	PASCNT	1217.0	WLT	234.0	PSVT	695.0
F8MT	700.40000	8MT	45.0	SVT	32.30000	QSTR.	0.0
LAT8TK	-0.59340201	ALS	-1.2161207	IMT	-2.7695562	XA	46.290737
LNG8TK	0.7472700	OLS	0.0051600	IS	-3.0	XB	19.090009
COL8TK	16.525114	THETAB	16.525114	TH5MR	6.4451140	XC	37.701963
PEDAL	11.107155	THETTR	10.441292	TH5STR	4.9412920	XP	50.590054
XAIN	4.6200737	XBIN	1.9090009	XCIN	3.7701963	XPIN	2.7317919
XBACTP	21.024000	XBACTI	2.1024000	RSTR.	0.0	PSTR	0.0
V80	160.65003	THETAB	3.6000052	AABF	3.1014497	OSTR	0.0
VYB	11.391420	PHIB	0.0	AAIF	-5.0061062	RSTR	0.0
VZ0	10.007795	RETAMP	3.6790005	BBIF	0.00649945E-1	TITR	0.0
P	0.0	GAMC	0.0	AAOL	-4.1900659	MITR	0.0
R	0.0	OMGRAT	1.0	AAIL	0.24107694	JITR	0.0
ALFMP	0.55000906	PHIDOT	0.0	BBIL	0.36200045	MMITR	0.0
CHITPP	02.003040	EKTZ	1.6490261	EMFX	0.92004908	LMITR	0.0
EKTR	0.0	EPSTMT	0.00679009	EMFZ	1.2079961	OMITR	0.0
OMF	37.429361	KGMT	0.07177979	SICMT	0.64751975	XITR	0.0
MUXS	0.23325674	CTSIG	0.6707030E-1	KQVT	0.03100377	YITR	0.0
MUYS	0.15725112E-1	CM8IG	-0.47500950E-2	LTOT	3.4630934	ZITR	0.0
MUZS	0.27690011E-2	COM8IG	0.49092052E-0	DTOT	24.401060	LITR	0.0
LAMBMR	-0.97539494E-2	NZ	0.99705491	TTR	0.3704561	MITR	0.0
DMSMR	0.12522950E-1	VC	0.71525373E-9	MPHR	1133.2135	NITR	0.0
XMR	1922.0494	M8AR	-1100.6090	KTBLK	1.0	AXP	2.0602155
YMR	-250.36815	J8AR	254.36815	V8DOT	0.15100240E-2	AYP	-0.24006269E-1
ZMR	-13640.553	T8AR	15724.929	V9DOT	-0.10360017E-1	AZP	-32.103912
LMR	-5026.5936	LBARM	-2201.0103	V2DOT	0.23009519E-2	VXP	160.65003
MMR	-002.14135	MBARM	-15256.306	PDOT	-0.95050965E-2	VYP	11.391420
NMR	22507.512	QBARM	23003.979	QDOT	0.20201096E-2	VZP	10.047795
YMF	-093.60400	XT	-23.053153	ROOT	-0.2974900E-2	RSTR.	0.0
ZMF	-301.12760	YT	-170.11212	XTR	0.0	PSIDMG	-50.0
LMP	536.64727	LT	-395.01927	YTR	706.62407	BTR	0.0
NMP	-3392.2619	MT	13103.227	ZTR	-206.30030	MADD	0.0
XMT	-3194.7102	NT	4970.2169	LTR	4031.4717	XADD	0.0
YMT	-13.17201	XVT	-10.675071	MTR	-0070.7055	YADD	0.0
YMT	-1.9745510	VVT	-176.13757	ALFMTT	-2432.235	ZADD	0.0
ZMT	460.26319	ZVT	0.37003121	ALFYTT	3.0617702	NADD	0.0
				A4901F	5.6000070	LADD	0.0

Figure D-12. (continued)